Alaska
Department of
Transportation
and
Public Facilities

Alaska Test Methods Manual

Effective April 15, 2007

Preface

This manual provides a compilation of approved Test Methods, Forms and Standard Practices to be used to test materials on Alaska Department of Transportation & Public Facilities (DOT&PF) projects.

Most of these testing procedures follow two nationally recognized standards; American Society for Testing and Materials (ASTM), and the American Association of State Highway and Transportation Official (AASHTO). Modifications to these standards are in recognition of the necessity of adjusting test requirements to meet local demands and/or naturally occurring materials.

This manual also includes Field Operating Procedures (FOPs) for existing AASHTO test methods. These procedures are developed and maintained by the Western Alliance for Quality in Transportation Construction (WAQTC). The FOPs select options and provide concise directions in the use of the AASHTO methods.

In addition, this manual includes WAQTC test methods that are not covered by AASHTO or ASTM. These methods have been submitted to AASHTO for adoption. Other procedures were developed by the Alaska DOT&PF to address specific needs in the State of Alaska that are not adequately covered in AASHTO, ASTM or WAQTC.

This manual's footers include the test method acceptance or revision date. These dates identify when the ASTM, WAQTC, or AASHTO method was approved or revised. The effective date, also included in the footer, represents when this manual as a whole was adopted by this department.

The Appendix contains standardized practices to be used by all DOT&PF regional and/or field laboratories including consultant fixed and field laboratories.

This Alaska Test Methods Manual supercedes all previously issued and is effective April 15, 2007

Acknowledgement

Design and Engineering Services, Statewide Materials is indebted to the following organizations for use of, or reference to, portions of their publications.

The American Association of State Highway and Transportation Officials
The American Society for Testing and Materials

Appreciation is also extended to Laboratory and Construction personnel from each Region for their dedication and patience in seeing this task to completion.

Third Edition Printing, April 15, 2007

List of Revisions for this edition:

1. TOC Corrected errors, added addendum reference to T224 and added Section 413
2. 207—added a statement to the addendum making the use of an extruder optional. Allows the use of estimated specific gravities for creating the ZAV line.
3. 212—corrected the numbered references that are now letters, removed references to CBR Mold. Corrected the Mold Factor rounding to 0.01 instead of a whole number.
4. 213—defined visual description for reporting in the addendum.
5. 214 – T 224, added addendum for TCTT
6. 301 – T 2, deleted," When Sampling without the use of a sampling tube, the sample should be obtained in three increments minimum."
7. 303- added an addendum to T 248 requiring the number of chutes to be maximized, using the greatest number possible over the minimum width requirement.
8. 306—removed the phrase, "flat (thin) particles, elongated particles or…" from the scope.
9. 312 – added requirement for Flat and Elongated at 8%, deleted the Precision statement and corrected the Flat and Elongated ratio to 1:5.
10. 313 – Added the T 210 vessel to apparatus.
11. 402 – Added coring reference to the addendum.
12. 405 – Changed JMF to JMD (Job Mix Design), added AASHTO T329 and deleted TM 6; added 10 to 15 spadings instead of undetermined number; requires the printer tape be attached to the report. Added the phrase, "approximately equal to or up to 5 grams above" to step 3 of the procedure. Added a note 1 to step 8 of the procedure, "When taking the moisture from the gauge pan sample, remove it immediately after completing the oil content test."
13. 406 – T 308, Changed Calibration to Correction Factors; added requirement to determine oil content using external balances; added calculating and reporting requirements; record final weight prior to 3 hours after removal from the oven.
14. 407 – T329, added addendum clarifying the initial 90 minutes is a minimum.
15. 409 – T209, remove guideline number 2 from the addendum as it is now covered by the WAQTC FOP.
16. 410 – T 166/T 275, changed the variable designators to match the procedure and corrected the method to read method C/A.
17. 411- Deleted the language in the addendum that restricted this method to quality control only.

18. 412 – Made scope only for HMA and added note in the Scope allowing this procedure to be used for other than HMA; removed the compaction requirement, removed the references to WAQTC TM 8 from procedure steps 4 and 9..
19. 413 – Added new section to accommodate new WAQTC method for coring. Added addendum allowing different methods of separating layers of a core, specifying joint cores to be centered on the longitudinal joint and required length to be determined and recorded.
20. 417 – Made changes to the viscosity determination methods table.
21. 504 – T 121, deleted density and yield reporting requirements from the addendum as the procedure now specifies this.
22. 505 – T 152, requires aggregate correction factors for new sources and when a source has a history of correction factors in excess of 0.4%.
23. 506 – T 23, added requirement to addendum that all curb and gutter concrete shall be rodded regardless of slump.
24. 520 – removed the intended use for APL qualification from scope. Require the cubes to be made in accordance with ATM 507.
25. SP3 – Removed and referenced AASHTO T 88.
26. SP8 – removed references to the White Meter which is no longer allowed.
27. Forms – updated and added calculating forms and examples.
28. Changed WAQTC methods that have been updated since last review.
    - 28.1 T 2 – Editorial and clarification only.
    - 28.2 T 27/ T 11 – Now allows the use of a mechanical washer for the removal of minus No. 200's. Consolidated the calculation section. While each method shows the calculations that are unique, the common portions have been consolidated under method A.
    - 28.3 T 176 – Editorial and clarification only.
    - 28.4 T 248 – Editorial and clarification only.
    - 28.5 TP 61 – The language for washing the sample has been removed. Other editorial changes for clarification only.
    - 28.6 T 30 – Language has been added to allow the use of the T 308 sample. The instructions now require that the weighed determination of the original sample mass agree with the calculated mass from T 308 within 0.1%. The calculation section was rewritten to clarify. All other changes are editorial and clarification only.
    - 28.7 T 40 – Editorial and clarification only.
    - 28.8 T 166/ T 275 – The towel drying for SSD weight must be completed in 5 seconds or less. All other changes are editorial and clarification only.
    - 28.9 T 168 – Editorial and clarification only.
    - 28.10 T 209 – Editorial and clarification only.
    - 28.11 T 308 – The method now allows the calculation of the percent asphalt binder to be calculated using masses from external balances with using procedure A – Internal Balance. Set the reporting to .01% for both oil content and moisture content. All other changes are editorial and clarification only, added aggregate correction factor need only be determined when it meets the conditions set.
    - 28.12 T 329 – AASHTO has adopted WAQTC TM 6. This now takes the place of TM 6 in our manual. All other changes are editorial and clarification only.
    - 28.13 TM 5 – Editorial and clarification only. A new name has been added for the loaf method. It is now called the loaf/incremental method.
    - 28.14 T 23 – Changes were editorial and to standardize the screen used to wet sieve oversized aggregate. The standard was set for 1 ½" for all methods.
    - 28.15 T 119 – Editorial and clarification only.

28.16 T 121 – Added reporting requirements.
28.17 T 152 – Changes were editorial and to standardize the screen used to wet sieve oversized aggregate. The standard was set for 1 ½" for all methods.
28.18 T 309 – Changed "thermometer" to "Temperature measuring devices."
28.19 T 85 – Editorial and clarification only.
28.20 T 255/ T 265 – Editorial and clarification only.
28.21 T 310 – Editorial and clarification only.

Contents

Section 200 Earthwork

Section 300 Bases and Aggregates

*This Test Method has an Addendum attached which has specific instructions for the use of the noted test method by the State of Alaska DOT&PF.

Section 400 Asphalt

Section 500 Concrete

Appendix 1 Standard Practice

Sticks & Roots Content of Aggregate and Soil, ATM 201

1. Scope

This method describes the procedure for determining the percent of sticks & roots by wet mass of the total aggregate or soil sample.

2. Significance

This test would be used to quantify the organic content of soils for particles that are too large to test in accordance with ATM 203, Organic Content of Soils by Ignition.

3. Apparatus

- Balance or scale: Capacity sufficient for the field sample mass, readable to 0.1 percent or 0.1 g and meeting the requirements of AASHTO M 231.
- 2.00 mm (No. 10) sieve conforming to AASHTO M 92.
- Miscellaneous equipment including pans, gloves, etc.

4. Sampling and Sample Preparation

Obtain the sample in accordance with WAQTC FOP for AASHTO T 2. The test will be performed on the complete as-received sample before drying.

5. Procedure

5.1. Determine the mass of the as-received sample to 0.1 percent or 0.1 g. Record this as the Total Sample Mass.

5.2. Separate the sample on a 2.00 mm (No. 10) sieve to ease identification of sticks & roots.

5.3. Separate the sticks & roots from the plus 2.00 mm (No. 10) material and place in a separate pan.

5.4. Determine the mass of the sticks & roots to 0.1 percent or 0.1 g. Record this as the Sticks & Roots Mass.

6. Calculations

Calculate the percentage of Sticks & Roots by:
Sticks & Roots, percent =

$$\left(\frac{\text{Sticks \& Roots Wet Mass}}{\text{Total Wet Sample Mass}}\right) \text{x}\, 100$$

7. Report

Report the Stick and Root Content on Department forms to the nearest 1 percent.

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TOTAL EVAPORABLE MOISTURE CONTENT OF AGGREGATE BY DRYING
FOP FOR AASHTO T 255
LABORATORY DETERMINATION OF MOISTURE CONTENT OF SOILS
FOP FOR AASHTO T 265

Scope

This procedure covers the determination of moisture content of aggregate and soil in accordance with AASHTO T 255 and AASHTO T 265. It may also be used for other construction materials.

Apparatus

- Balance or scale: capacity sufficient for the principle sample mass, accurate to 0.1 percent of sample mass or readable to 0.1 g. Meeting the requirements of AASHTO M 231.
- Containers, capable of being sealed
- Suitable drying containers
- Microwave safe containers
- Thermometer reading to 205 ±6°C (400 ±10°F)
- Heat source , controlled
  - Forced draft oven
  - Ventilated / convection oven
- Heat source, uncontrolled
  - Microwave oven (600 watts minimum)
  - Infrared heater, hot plate, fry pan, or any other device/method that will dry the sample without altering the material being dried
- Utensils such as spoons
- Hot pads or gloves

Sample Preparation

For aggregate, select the proper sample size based on Table 1 or other information that may be specified by the agency. Obtain the sample in accordance with the FOP for AASHTO T 2.

Immediately seal or cover samples to prevent any change in moisture content.

Table 1
Sample Sizes for Moisture Content of Aggregate

Nominal Maximum Size* mm (in.)	Minimum Sample Mass g (lb)
4.75 (No. 4)	500 (1.1)
9.5 (3/8)	1500 (3.3)
12.5 (1/2)	2000 (4)
19.0 (3/4)	3000 (7)
25.0 (1)	4000 (9)
37.5 (1 1/2)	6000 (13)
50 (2)	8000 (18)
63 (2 1/2)	10,000 (22)
75 (3)	13,000 (29)
90 (3 1/2)	16,000 (35)
100 (4)	25,000 (55)
150 (6)	50,000 (110)

* One sieve larger than the first sieve to retain more than 10 percent of the material using an agency specified set of sieves based on cumulative percent retained. Where large gaps in specification sieves exist, intermediate sieve(s) may be inserted to determine nominal maximum.

For soil, select the proper sample size based on Table 2 or other information that may be supplied by the agency.

Table 2
Sample Sizes for Moisture Content of Soil

Maximum Particle Size mm (in)	Minimum Sample Mass g
0.425 (No. 40)	10
4.75 (No. 4)	100
12.5 (1/2)	300
25.0 (1)	500
50 (2)	1000

Procedure

For aggregate, determine and record all masses to the nearest 0.1 percent of the sample mass or to the nearest 0.1 g. For soil, determine and record all masses to the nearest 0.1 g. When determining mass, allow the sample and container to cool sufficiently so as not to damage or interfere with the operation of the balance or scale.

1. Determine and record the mass of the container.

2. Place the wet sample in the container, and record the total mass of the container and wet sample.
3. Determine the wet mass of the sample by subtracting the mass in Step 1 from the mass in Step 2.
4. Dry the sample to a constant mass in accordance with the directions given under Directions for Drying below. Measures will be taken to protect the scale from excessive heat while determining constant mass.
5. Allow the sample to cool and record the total mass of the container and dry sample.
6. Determine the dry mass of the sample by subtracting the mass in Step 1 from the mass in Step 5.

Directions for Drying Aggregate

- Controlled (Forced Draft, Ventilated or Convection Oven)

  1. Spread sample in the container.

  2. Dry to constant mass at 110 ±5°C (230 ±9°F). Constant mass has been reached when there is less than a 0.10 percent change after an additional 30 minutes of drying.

- Uncontrolled

Where close control of temperature is not required (such as with aggregate not altered by higher temperatures, or with aggregate that will not be used in further tests, or where precise information is not required), higher temperatures or other suitable heat sources, may be used. Other heat sources may include microwaves, hot plates, or heat lamps.

  – Microwave Oven
    1. Heap sample in pile in the center of the container and cover. This cover must allow moisture to escape.
    2. Dry to constant mass. Constant mass has been reached when there is less than a 0.10 percent change after at least an additional 10 minutes of drying.

       Caution: Some minerals in the sample may cause the aggregate to overheat altering the aggregate gradation.
  – Hot plates, heat lamps, etc.
    1. Spread sample in container.
    2. Stir the sample frequently to avoid localized overheating and aggregate fracturing.
    3. Dry to a constant mass. Constant mass has been reached when there is less than a 0.10 percent change after at least an additional 20 minutes of drying.

Directions for Drying Soil

- Oven (Preferably Forced Draft/Air)
  1. Place sample in container.

2. Dry to constant mass at 110 ±5°C (230 ±9°F). Constant mass has been reached when there is no change after an additional 1 hour of drying. A sample dried overnight (15 to 16 hours) is sufficient in most cases.

Note 1: Soils containing gypsum or significant amounts of organic material require special drying. For reliable moisture contents dry these soils at 60°C (140°F). For more information see AASHTO T 265, Note 2.

Calculation

Constant Mass for Aggregates:

Calculate constant mass using the following formula:

$$\%Change = \frac{Mp - Mn}{Mp} x100$$

Where: M_p = previous mass measurement
M_n = new mass measurement

Example:

Mass of container: 1232.1 g

Mass of container& sample after first drying cycle: 2637.2 g

Mass, M_p, of possibly dry sample: 2637.2 g - 1232.1 g = 1405.1 g

Mass of container and dry sample after second drying cycle: 2634.1 g

Mass, M_n, of dry sample: 2634.1 g - 1232.1 g = 1402.0 g

$$0.22\% = \frac{1405.1 - 1402.0}{1405.1} x100$$

0.22% is not less than 0.10% so continue to dry it

Mass of container and dry sample after third drying cycle: 2633.0 g

Mass, M_n, of dry sample: 2633.0 g - 1232.1 g = 1400.9 g

$$0.08\% = \frac{1402.0 - 1400.9}{1402.0} x100$$

0.08% is less than 0.10% constant mass has been reached for an aggregate, but continue drying for soil.

Moisture Content Aggregate and Soils:

Calculate the moisture content, as a percent, using the following formula:

$$w = \frac{M_W - M_D}{M_D} \times 100$$

Where:

w = moisture content, percent
M_W = wet mass
M_D = dry mass

Example:

Mass of container: 1232.1 g
Mass of container and wet sample: 2764.7 g
Mass, M_W, of wet sample: 2764.7 g - 1232.1 g = 1532.6 g
Mass of container and dry sample (**COOLED**): 2633.1 g
Mass, M_D, of dry sample: 2633.1 g - 1232.1 g = 1401.0 g

$$w = \frac{1532.6\,\text{g} - 1401.0\,\text{g}}{1401.0\,\text{g}} \times 100 = \frac{131.6\,\text{g}}{1401.0\,\text{g}} \times 100 = 9.39\% \text{ rounded to } 9.4\%$$

Report

Results shall be reported on standard forms approved for use by the agency. Include:

- M_W, wet mass
- M_D, dry mass
- w, moisture content to nearest 0.1 percent

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Organic Content of Soils ATM 203

1. Scope

This method describes the procedure for determining organic content of soils by loss on ignition as adopted from AASHTO T 267.

This standard involves hazardous materials, operations and equipment. This standard does not purport to address all of the safety problems associated with its use. It is the responsibility of the agency to establish appropriate safety and health practices and to train the user of this standard prior to use. It is the responsibility of the user to consult the appropriate agency authority for and to practice and maintain the appropriate safety and health practices.

2. Apparatus

- 2.00 mm (No. 10) sieve and pan, plus whatever additional larger size sieves are necessary to prevent overloading the No. 10 sieve. Sieves will conform to AASHTO M 92
- Pulverizing apparatus suitable for breaking up aggregations of soil particles without reducing the size of individual grains
- Balance or scale: Capacity sufficient for the principle sample mass, readable to 0.1%, or better, of the total sample mass and meeting the requirements of AASHTO M 231

  For this test, this would require a scale with a capacity of at least 100 g and readable to 0.01 g
- Muffle Furnace, thermostatically controlled, capable of maintaining a temperature of 445 ± 10°C (830 ±15°F). The combustion chamber will be capable of accommodating the designated container(s) and sample(s). The furnace shall be equipped with a pyrometer recorder that will indicate chamber temperature while in use.
- Crucible, with covers, having a minimum volume of 100 ml and capable of withstanding repeated exposure to temperatures of 500ºC (950°F)
- Non-asbestos, heat-resistant, gauntlet-type gloves capable of withstanding temperatures of 500ºC (950°F)
- Desiccator of sufficient size containing an effective desiccant
- Miscellaneous equipment including tongs, spatulas, wire brushes, etc.

3. Sampling and Sample Preparation

1. Obtain the sample in accordance with WAQTC FOP for AASHTO T 2.
2. Dry the sample to constant mass in accordance with the soil procedure of WAQTC FOP for AASHTO T 255/T 265.
3. Sieve the dry sample through the 2.00 mm (No. 10) sieve.

   If the material contains lumps of organics or aggregations of soil, they will be broken up by such means that will not reduce the size of the plus 2.00 mm (No. 10) aggregate particles.

   For Topsoil samples: Any large particles of organics that cannot be broken up will be removed and discarded.

   Note 1: Organic content for topsoil is the organics that are readily available for use by the root system of the plantings (grass, trees, etc.).

   For other types of samples: Any large particles of organics that cannot be broken up will be removed by hand and reported as Sticks and Roots (see ATM 201).

4. Reduce the sample to a mass of approximately 100 g in accordance with WAQTC FOP for AASHTO T 248.

4. Procedure

1. Determine the mass of a crucible to the nearest 0.01 g and record as Tare.
2. Select a sample with a mass between 10-40 g, place into the crucible, determine the mass to the nearest 0.01 g and record as Mass Before Ignition + Tare.

   Note 2: Sample masses for lightweight materials such as peat may be less than 10 g but should be of sufficient amount to fill the crucible to at least 3/4 depth. A cover may initially be required over the crucible during the initial phase of ignition to decrease the possibility of the sample being "blown out" from container.

3. Place the crucible into a pre-heated muffle furnace at a temperature of 445ºC (835°F) for a minimum of six hours until all organic matter is combusted. If a cover has been used, it shall be removed after approximately 2 hours of combustion.
4. Remove the test sample from the muffle furnace and cool it to room temperature in a desiccator.
5. Determine the mass to the nearest 0.01 grams and record as Mass After Ignition + Tare.

5. Calculations

1. Calculate the percent organic content by the following formula:

$$\text{Organic Content} = \left(\frac{A - B}{A - C}\right) x\, 100$$

Where: A = Mass Before Ignition + Tare,
B = Mass After Ignition + Tare,
C = Tare.

6. Report

Report the organic content on Department forms to the nearest 0.1 percent.

DETERMINING THE LIQUID LIMIT OF SOILS
WAQTC FOP FOR AASHTO T 89

Scope

This procedure covers the determination of the liquid limit of a soil in accordance with AASHTO T 89. It is used in conjunction with WAQTC FOP AASHTO T 90, Determining the Plastic Limit and Plasticity Index of Soils. The three values are used for soil classification and other purposes.

Apparatus

- Dish: preferably unglazed porcelain or similar mixing dish, about 115 mm (4.5 in.) in diameter.
- Spatula: having a blade 75 to 100 mm (3 to 4 in.) long and about 20 mm (3/4 in.) wide.
- Liquid Limit Device: manually or mechanically operated, consisting of a brass cup, carriage, and base plate.
- Grooving Tool: used to cut the soil in the liquid limit device cup.
- Gauge: part of the grooving tool or a separate metal bar, 10.0 ±0.2 mm (0.394 ±0.008 in.) thick and approximately 50 mm (2 in.) long.
- Containers: corrosion resistant, suitable for repeated heating and cooling, having close fitting lids to prevent the loss of moisture. One container is needed for each moisture content determination.
- Balance: conforming to AASHTO M 231, class G1, sensitive to 0.01 g with a 1200 g capacity.
- Oven: thermostatically controlled, capable of maintaining temperatures of 110 ±5°C (230 ±9°F).
- Graduated cylinders for measuring distilled or demineralized water.

Adjustment of Liquid Limit Device

The liquid limit device shall be inspected to determine that the device is in good working order; that the pin connecting the cup is not worn to permit side play; that the screws connecting the cup to the hanger are tight; that the points of contact on the cup and base are not excessively worn; that the lip of the cup is not excessively worn; and that a groove has not been worn in the cup. The grooving tool shall be inspected to determine that the critical dimensions are correct.

> ***Note 1:*** Wear is considered excessive when the point of contact on the cup or base exceeds approximately 13 mm (0.5 in.) in diameter, or when any point on the rim of the cup is worn to approximately 1/2 the original thickness. A slight groove in the center of the cup is not objectionable. If the groove becomes pronounced, the cup shall be replaced. A base that is excessively worn may be refinished as long as it is maintained within the tolerances specified.

Adjust the height of drop of the cup so that the point on the cup that comes in contact with the base rises to a height of 10.0 ± 0.2 mm (0.394 ± 0.008 in.).

> ***Note 2:*** Check the height of the drop, before each use, by turning the crank at two revolutions per second while holding the gauge in position against the cup. If a ringing or clicking sound is heard without the cup rising from the gauge, the adjustment is correct. If no ringing is heard or if the cup rises from gauge, readjust the height of the drop. If the cup rocks on the gauge during this checking operation, the cam follower pivot is excessively worn and should be replaced.

Sample

Samples must be prepared per AASHTO T 87 or T 146. Obtain a sample with a mass of about 100 g taken from the portion of the material passing the 0.425 mm (No. 40) sieve.

The mass required depends upon the method chosen. Method A (multi-point method) requires approximately 100 g. Method B (single point method) requires approximately 50 g.

Procedure – Method A (Multi-Point)

1. Place the sample in the dish and thoroughly mix with 15 to 20 mL of distilled or demineralized water by alternately and repeatedly stirring, kneading, and chopping with a spatula. Further additions of water shall be in increments of 1 to 3 mL. Each increment shall be thoroughly mixed with the soil before another increment is added. Once testing has begun, no additional dry soil should be added to the moistened soil. The cup of the Liquid Limit device shall not be used for mixing soil and water. If too much water is added, the sample shall either be discarded or mixed and kneaded until natural evaporation lowers the moisture content.

   > ***Note 3:*** Some soils are slow to absorb water. It is possible to add water so fast that a false LL value is obtained. This can be avoided by allowing more mixing and/or time. Also, tap water may be used for routine testing if comparative tests indicate no differences in results between using tap water and distilled or demineralized water.

2. Add sufficient water to form a uniform mass of a stiff consistency.

3. Place enough material in the cup so that, when squeezed and spread with the spatula, the soil will rest in the cup above the spot where the cup rests on the base and will be 10 mm thick at the point of maximum thickness. Use as few strokes of the spatula as possible, taking care to prevent the entrapment of air bubbles in the sample.

4. Divide the soil in the cup with a firm stroke of the grooving tool. Avoid tearing of the sides of the groove or slipping of the soil cake on the cup. Up to six strokes are permitted. The depth of the groove should be increased with each stroke, and only the last stroke should scrape the bottom of the cup.

5. Lift and drop the cup by turning the crank at a rate of approximately two revolutions per second until the two halves of the soil pat come together along a distance of about 13 mm (0.5 in.). Do not hold the base while the crank is turned. Record the number of shocks required to close the groove.

   > ***Note 4:*** Some soils tend to slide on the cup instead of flowing. If this occurs, water should be added, the sample remixed, and the procedure repeated. If the soil continues to slide on the cup, the test is not applicable and a note should be made that the liquid limit could not be determined.

6. Obtain a moisture content sample by slicing through the soil pat perpendicularly with the spatula and through the center of the groove. Place it into a suitable container for subsequent moisture determination.

7. Determine the moisture content of the moisture content sample in accordance with the FOP for AASHTO T 255/T 265. Determine and record all masses to 0.01g.

8. Place the soil remaining in the cup back in the mixing dish and add 1 to 3 mL of water, or use previously prepared portions to which sufficient water has been added to result in a more fluid condition.

9. Repeat Steps 3 through 8, a minimum of two times. The object is to have a determination in all three shock ranges 25-35, 20-30, & 15-25.

Flow Curve – Method A

Prepare a flow curve on a semi-logarithmic graph with moisture content on the arithmetic vertical axis and the number of shocks on the logarithmic horizontal axis. The flow curve is a straight line drawn as closely as possible through three or more plotted points.

Liquid Limit – Method A

Determine the liquid limit. The moisture content at the intersection of the flow curve and the 25 shock line is the liquid limit.

Procedure – Method B (Single-Point)

1. Place the sample in the dish and thoroughly mix with 8 to 10 mL of distilled or demineralized water, and following the mixing procedure in Method A, Step 1.

2. Follow the procedure in Method A except that the soil pat should be prepared with water to produce a consistency that will close the two halves of the soil pat at least 13 mm (0.5 in.) within 22 to 28 shocks of the cup.

   Note: Groove closures occurring between 15 and 40 blows may be accepted if variations of ±5 percent of the true liquid limit are tolerable.

3. Return the soil remaining in the cup to the mixing dish and, without adding any additional water, repeat Step 2. If the closure again occurs within the acceptable range, obtain a moisture content specimen.

4. Determine the moisture content of the moisture content sample in accordance with the FOP for AASHTO T 255/T 265.

Liquid Limit – Method B

Calculate the liquid limit as follows:

$$LL = (w_N)(N/25)^{0.121}$$

N	$(N/25)^{0.121}$	N	$(N/25)^{0.121}$
22	0.985	26	1.005
23	0.990	27	1.009
24	0.995	28	1.014
25	1.000		

$$LL = (w_N)(N/25)^{0.121}$$

where

LL = liquid limit
w_N = moisture content of sample at N blows
N = number of blows

Example:

w_N = 16.0 % and N = 23
LL = $(16.0)(23/25)^{0.121}$ = 15.8, say 16%

Report

Results shall be reported on standard forms approved by the agency. Report LL to the nearest whole percent.

DETERMINING THE PLASTIC LIMIT AND PLASTICITY INDEX OF SOILS WAQTC FOP FOR AASHTO T 90

Scope

This procedure covers the determination of the plastic limit and plasticity index of soil in accordance with AASHTO T 90. It is used in conjunction with AASHTO T 89, Determining the Liquid Limit of Soils. The three values are used for soil classification and other purposes. This FOP will cover the hand rolling method only. If the plastic limit device method is approved by the agency see AASHTO T 90 for that procedure.

Apparatus

- Dish: preferably unglazed porcelain or similar mixing dish, about 115 mm (4.5 in.) in diameter.
- Spatula: having a blade 75 to 100 mm (3 to 4 in.) long and about 20 mm (3/4 in.) wide.
- Rolling Surface: a ground glass plate or piece of smooth, unglazed paper.
- Containers: corrosion resistant, suitable for repeated heating and cooling, having close fitting lids to prevent the loss of moisture. One container is needed for each moisture content determination.
- Balance: conforming to AASHTO M 231, class G1, sensitive to 0.01 g with a 1200 g capacity.
- Oven: thermostatically controlled, capable of maintaining temperatures of 110 ±5°C (230 ±9°F)

Sample

The plastic limit procedure is often run in conjunction with the liquid limit procedure. If this is the case, the plastic limit sample should be obtained from the soil prepared for the liquid limit test at any point in the process at which the soil is plastic enough to be easily shaped into a ball without sticking to the fingers excessively when squeezed. Obtain approximately 8 g of soil to run the plastic limit test.

If the plastic limit only is to be determined, the sample must be prepared per AASHTO T 87 or T 146. Obtain about 20 g of material passing the 0.425 mm (No. 40) sieve. Mix the soil with distilled or demineralized water until the mass becomes plastic enough to be easily shaped into a ball. Obtain approximately 8 g of soil to run the plastic limit test.

> ***Note 1:*** Tap water may be used for routine testing if comparative tests indicate no differences in results between using tap water and distilled or demineralized water.

Procedure (Hand Rolling Method)

1. From the sample pull a 1.5 to 2 g mass.
2. Squeeze and form the test sample into an ellipsoidal-shape mass.
3. Roll this mass between the fingers or palm and the rolling surface with just sufficient pressure to roll the mass into a thread of uniform diameter along its length. Roll out between 80 and 90 strokes per minute, counting a stroke as one back and forth motion. The sample must be rolled into the 3 mm (1/8 in.) thread in no longer than 2 minutes.

4. Break the thread into six or eight pieces when the diameter of the thread reaches 3 mm (1/8 in.).

5. Squeeze the pieces together between the thumbs and fingers of both hands into an ellipsoidal-shape mass and reroll.

6. Continue this process of alternately rolling to a thread 3 mm (1/8 in.) in diameter, cutting into pieces, gathering together, kneading and rerolling until the thread crumbles under the pressure required for rolling and the soil can no longer be rolled into a thread.

   Note 2: Crumbling may occur when the thread has a diameter greater than 3 mm (1/8 in.). This shall be considered a satisfactory end point, provided the soil has been previously rolled into a thread 3 mm (1/8 in.) in diameter. The crumbling will manifest itself differently with various types of soil. Some soils fall apart in many pieces; others form an outside tubular layer that splits at both ends; splitting progresses toward the middle, and the thread falls apart in small platy particles. Heavy clay requires much pressure to deform the thread, particularly as it approaches the plastic limit, and the thread breaks into a series of barrel-shaped segments each 6 to 9 mm (1/4 to 3/8 in.) long. At no time shall the tester attempt to produce failure at exactly 3 mm (1/8 in.) diameter. It is permissible, however, to reduce the total amount of deformation for feebly plastic soils by making the initial diameter of the ellipsoidal-shaped mass nearer to the required 3 mm (1/8 in.) final diameter.

7. Gather the portions of the crumbled soil together and place in a suitable, tared container & cover.

8. Repeat steps one through seven until 8 g of sample have been tested and placed in the covered container.

9. Determine the moisture content of the sample in accordance with the FOP for T 255/T 265. Determine and record all masses to 0.01g.

Plastic Limit

The moisture content, as determined in Step 9 above, is the Plastic Limit. It is advisable to run several trials on the same material to ensure a proper determination of the Plastic Limit of the soil.

Plasticity Index

The Plasticity Index (PI) of the soil is equal to the difference between the Liquid Limit (LL) and the Plastic Limit (PL).

PI = LL – PL

Examples: **#1** **#2**

#1

LL = 34 and PL = 17

PI = 34 – 17 = 17

#2

LL = 16 and PL = 10

PI = 16 – 10 = 6

Example Calculation

Container	Container Mass, g	Container and Wet Soil Mass, g	Wet Soil Mass, g	Container and Dry Soil Mass, g	Dry Soil Mass, g
1	14.44	22.65	8.21	21.45	7.01
2	14.18	23.69	9.51	22.81	8.63

Water Mass, g	Moisture Content	Plastic Limit
1.20	17.1	17
0.88	10.2	10

Report

Results shall be reported on standard forms approved by the agency. Report the PL and PI to the nearest whole number.

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pH of Topsoil ATM 206

1. Scope

This method describes the procedure for determining the pH of topsoil.

2. Apparatus

- A soil test kit capable of determining the pH of soils. These are available from commercial greenhouses. Verify Reagent expiration dates and replace as needed.
- pH Meter—Calibrate according to manufacturers recommendations.
- 2.00 mm (No. 10) sieve conforming to AASHTO M 92.

3. Sampling and Sample Preparation

3.1. Obtain the sample in accordance with WAQTC FOP for AASHTO T 2.

3.2. Prepare the soil sample in accordance with the manufacturer's instructions for the soils kit.

4. Procedure

4.1. Separate sample on a 2.00 mm (No. 10) sieve. Discard the plus 2.00 mm (No. 10) material unless required for other testing.

4.2. Determine the pH of the minus 2.00 mm (No. 10) material in accordance with the manufacturer's instructions.

5. Report

Report the pH value to the nearest 0.5.

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MOISTURE-DENSITY RELATIONS OF SOILS:

USING A 2.5-kg (5.5-lb) RAMMER AND A 305 mm (12-in.) DROP

FOP FOR AASHTO T 99 (See Addendum for DOT&PF Guidelines)

USING A 4.54-kg (10-lb) RAMMER AND A 457 mm (18-in.) DROP

FOP FOR AASHTO T 180 (See Addendum for DOT&PF Guidelines)

Scope

This procedure covers the determination of the moisture-density relations of soils and soil-aggregate mixtures in accordance with two similar test methods:

- AASHTO T 99 methods A, B, C & D
- AASHTO T 180 methods A, B, C & D

This test method applies to soil mixtures having 40% or less retained on the 4.75 mm (No 4) sieve for methods A or B, or, 30 % or less retained on the 19mm (¾") with methods C or D. The retained material is defined as oversize (coarse) material. If no minimum percentage is specified, 5% will be used. Samples that contain oversize (coarse) that meet percent retained criteria should be corrected by using the FOP for AASHTO T 224. Samples of soil or soil-aggregate mixture are prepared at several moisture contents and compacted into molds of specified size using manual or mechanical rammers delivering a specified quantity of compactive energy. The moist masses of the compacted samples are divided by the volume of the mold to determine moist density values. Moisture contents of the compacted samples are determined and used to obtain the dry density values of the same samples. Maximum dry density and optimum moisture content for the soil or soil-aggregate mixture is determined by plotting the relationship between dry density and moisture content.

Apparatus

- Mold – Cylindrical, made of metal and having the dimensions shown in Table 1 or Table 2. It shall include a detachable collar and a base plate to which the mold can be fastened. If permitted by the agency, the mold may be of the "split" type, consisting of two half-round sections, which can be securely locked in place to form a cylinder.
- Rammer –Manually or mechanically operated rammers as detailed in Table 1 or Table 2. A manually operated rammer shall be equipped with a guide-sleeve to control the path and height of drop. The guide-sleeve shall have at least four vent holes no smaller then 9.5 mm (3/8 in.) diameter, spaced approximately 90 degrees apart and approximately 19 mm (3/4 in.) from each end. A mechanically operated rammer will uniformly distribute blows over the sample and will be calibrated with several soil types, and be adjusted, if necessary, to give the same moisture-density results as with the manually operated rammer. For additional information concerning calibration, see AASHTO T 99 and T 180.
- Sample Extruder – A jack, lever frame, or other device for extruding compacted specimens from the mold quickly and with little disturbance.

- Balance(s) or scale(s) of the capacity and sensitivity required for the procedure used by the agency.

  A balance or scale with a capacity of 20 kg (45 lb) and a sensitivity of 5 g (0.01 lb) for obtaining the sample. Meeting the requirements of AASHTO M 231.

  A balance or scale with a capacity of 2 kg and a sensitivity of 0.1 g is used for moisture content determinations done under both procedures. Meeting the requirements of AASHTO M 231
- Drying Apparatus – A thermostatically controlled drying oven capable of maintaining a temperature of 110 ±5°C (230 ±9°F) for drying moisture content samples in accordance with the FOP for AASHTO T 255/T 265.
- Straightedge – A steel straightedge at least 250 mm (10 in.) long, having one beveled edge and at least one surface, used for final trimming, plane within 0.1 percent of its length.
- Sieve(s) – 4.75 mm (No. 4) and/or 19.0 mm (3/4 in.) conforming to AASHTO M 92.
- Mixing Tools – Miscellaneous tools such as a mixing pan, spoon, trowel, spatula, etc., or a suitable mechanical device, for mixing the sample with water.
- Containers with close-fitting lids to prevent gain or loss of moisture in the sample.

Table 1
Comparison of Apparatus, Sample, and Procedure – Metric

	T 99	T 180
Mold Volume, m^3	Methods A, C: 0.000943	Methods A, C: 0.000943
	Methods B, D: 0.002124	Methods B, D: 0.002124
Mold Diameter, mm	Methods A, C: 101.6	Methods A, C: 101.6
	Methods B, D: 152.4	Methods B, D: 152.4
Mold Height, mm	116.43	116.43
Detachable Collar Height, mm	51	51
Rammer Diameter, mm	50.80	50.80
Rammer Mass, kg	2.495	4.536
Rammer Drop, mm	305	457
Layers	3	5
Blows per Layer	Methods A, C: 25	Methods A, C: 25
	Methods B, D: 56	Methods B, D: 56
Material Size, mm	Methods A, B: 4.75 minus	Methods A, B: 4.75 minus
	Methods C, D: 19.0 minus	Methods C, D: 19.0 minus
Test Sample Size, kg	Method A: 3	Method B: 7
	Method C: 5 (1)	Method D: 11(1)
Energy, kN-m/m^3	592	2,693

(1)This may not be a large enough sample depending on your nominal maximum size for moisture content samples.

Table 2
Comparison of Apparatus, Sample, and Procedure – English

	T 99	T 180
Mold Volume, ft^3	Methods A, C: 1/30	Methods A, C: 1/30
	Methods B, D: 1/13.33	Methods B, D: 1/13.33
Mold Diameter, in.	Methods A, C: 4.000	Methods A, C: 4.000
	Methods B, D: 6.000	Methods B, D: 6.000
Mold Height, in.	4.584	4.584
Detachable Collar Height, in.	2	2
Rammer Diameter, in.	2.000	2.000
Rammer Mass, lb	5.5	10
Rammer Drop, in.	12	18
Layers	3	5
Blows per Layer	Methods A, C: 25	Methods A, C: 25
	Methods B, D: 56	Methods B, D: 56
Material Size, in.	Methods A, B: No. 4 minus	Methods A, B: No.4 minus
	Methods C, D: 3/4 minus	Methods C, D: 3/4 minus
Test Sample Size, lb	Method A: 7 Method C: $12_{(1)}$	Method B: 16 Method D: $25_{(1)}$
Energy, lb-ft/ ft^3	12,375	56,250

(1)This may not be a large enough sample depending on your nominal maximum size for moisture content samples.

Sample

If the sample is damp, dry it until it becomes friable under a trowel. Drying may be in air or by use of a drying apparatus maintained at a temperature not exceeding 60°C (140°F). Thoroughly break up aggregations in a manner that avoids reducing the natural size of individual particles.

Obtain a representative test sample of the mass required by the agency by passing the material through the sieve required by the agency. See Table 1 or Table 2 for test sample mass and material size requirements.

Note 1: Both T 99 & T 180 have four methods (A, B, C, D) that require different masses and employ different sieves

Note 2: If the sample is plastic (clay types), it should stand for a minimum of 12 hours after the addition of water to allow the moisture to be absorbed. In this case, several samples at different moisture contents should be prepared, put in sealed containers and tested the next day. Instances where the material is prone to degradation i.e. granular material a compaction sample with differing moisture contents should be prepared for each point.

Procedure

1. Determine the mass of the clean, dry mold. Include the base plate, but exclude the extension collar. Record the mass to the nearest 0.005 kg (0.01 lb).

2. Thoroughly mix the selected representative sample with sufficient water to dampen it to approximately 4 to 6 percentage points below optimum moisture content. See note 2.

3. Form a specimen by compacting the prepared soil in the mold (with collar attached) in approximately equal layers. For each layer, spread the loose material uniformly in the mold. Lightly tamp the fluffy material with the manual rammer or other similar device. This establishes a firm surface on which to hold the rammer sleeve. Compact each layer with uniformly distributed blows from the rammer. See Table 1 for mold size, number of layers, number of blows, and rammer specification for the various test methods. Use the method specified by the agency. If material that has not been compacted remains adjacent to the walls of the mold and extends above the compacted surface, trim it down.

   Note 3: During compaction, the mold shall rest firmly on a dense, uniform, rigid, and stable foundation or base. This base shall remain stationary during the compaction process.

4. Remove the extension collar. Avoid shearing off the sample below the top of the mold. A rule of thumb is that the material compacted in the mold should not be over 6 mm (¼ in) above the top of the mold once the collar has been removed.

5. Trim the compacted soil even with the top of the mold with the beveled edge of the straightedge.

6. Determine the mass of the mold and wet soil in kg to the nearest 0.005 kg (0.01 lb) or better.

7. Determine the wet mass of the sample by subtracting the mass in Step 1 from the mass in Step 6.
8. Calculate the wet density as indicated below under "Calculations."

9. Extrude the material from the mold. For soils and soil aggregate mixtures slice vertically through the center and take a representative moisture content sample from one of the cut faces insuring that all layers are represented. For granular materials a vertical face will not exist. Take a representative sample. This sample must meet the sample size requirements of the test method to be used to determine moisture content.

   Note 4: When developing a curve for free-draining soils, such as uniform sands and gravels, where seepage occurs at the bottom of the mold and base plate, taking a representative moisture content from the mixing bowl may be preferred in order to determine the amount of moisture available for compaction.

10. Determine the moisture content of the sample in accordance with the FOP for AASHTO T 255/T 265.

11. Thoroughly break up the remaining portion of the molded specimen until it will again pass through the sieve, as judged by eye, and add to the remaining portion of the sample being tested. See note 2.

12. Add sufficient water to increase the moisture content of the remaining soil by approximately 1 to 2 percentage points and repeat the above procedure.

13. Continue determinations until there is either a decrease or no change in the wet density. A minimum of five determinations is usually necessary.

Calculations

1. Calculate the wet density, in kg/m^3 (lb/ft^3), by multiplying the wet mass from Step 7 by the appropriate factor chosen from the two below.

   Method A & C molds: 1060 (30)

Method B & D molds: 471 (13.33)

Note 5: The moist mass is in kg (lb). The factors are the inverses of the mold volumes in m^3 (ft^3) shown in Table 1. If the moist mass is in grams use 1.060 or 0.471 for factors when computing kg/m^3.

1/0.000943 = 1060 [1/(1/30) = 30]
1/0.002124 = 471 [1/(1/13.33) = 13.33]

Example – Method A or C mold: 30

Wet mass = 1.916 kg (4.22 lb)

(1.916)(1060) = 2031 kg/m^3 Wet Density [(4.22)(30) = 126.6 lb/ft^3 Wet Density]

2. Calculate the dry density as follows.

$$\rho_d = \left(\frac{\rho_w}{w + 100}\right) \times 100 \quad \text{or} \quad \rho_d = \left(\frac{\rho_w}{\frac{w}{100} + 1}\right)$$

where

ρ_d = Dry density, kg/m^3 (lb/ft^3)
ρ_w = Wet density, kg/m^3 (lb/ft^3)
w = Moisture content, as a percentage

Example: 32

ρ_w = 2030 kg/m^3 (126.6 lb/ft^3) and w = 14.7%

$$\rho_d = \left(\frac{2030\,kg/m^3}{14.7 + 100}\right) \times 100 = 1770\ kg/m^3$$

$$\rho_d = \left(\frac{126.6\,lb/ft^3}{14.7 + 100}\right) \times 100 = 110.4\ lb/ft^3$$

or

$$\rho_d = \left(\frac{2030\,kg/m^3}{(14.7/100) + 1}\right) = 1770\ kg/m^3$$

$$\rho_d = \left(\frac{126.6\,lb/ft^3}{(14.7/100) + 1}\right) = 110.4\ lb/ft^3$$

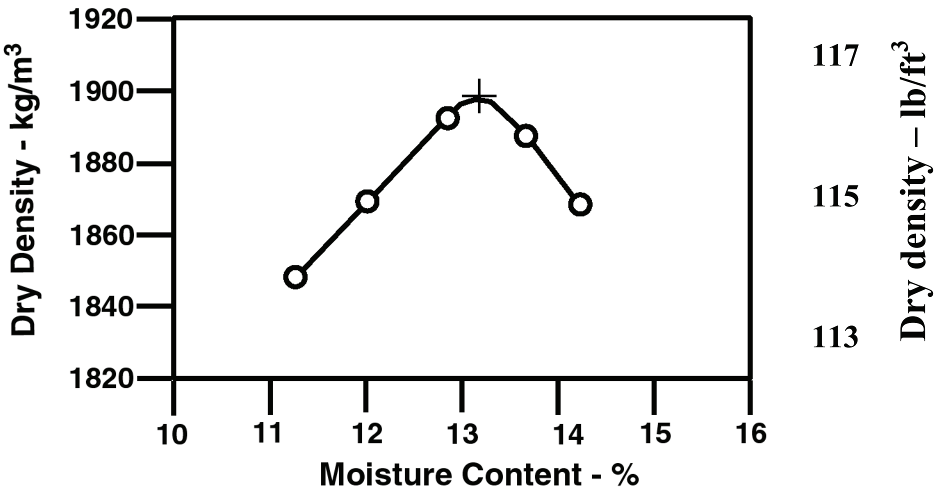
Moisture-Density Curve Development

When dry density is plotted on the vertical axis versus moisture content on the horizontal axis, and the points are connected, a moisture-density curve is developed. The peak of the curve has, as coordinates, the maximum dry density, or just "maximum density," and the "optimum moisture content" of the soil.

Example:

Given the following dry density and corresponding moisture content values, develop a moisture-density relations curve and determine maximum dry density and optimum moisture content.

Dry Density, kg/m³	Dry Density, lb/ft³	Moisture Content, %
1846	114.3	11.3
1868	115.7	12.1
1887	116.9	12.8
1884	116.7	13.6
1871	115.9	14.2



Ideally, there will be three points on the dry side of the curve and two points on the wet side. In this case, the curve has its peak at:

Maximum dry density = 1890 kg/m^3 (117.0 lb/ft^3)
Optimum water content = 13.2%

Note that both values are approximate, being based on sketching the curve to fit the points.

Report

Results shall be reported on standard forms approved by the agency. Report maximum dry density to the closest 1 kg/m^3 (0.1 lb/ft^3) and optimum moisture content to the closest 0.1 percent.

Addendum WAQTC FOP for AASHTO T 99/ T 180

Following are guidelines for the use of WAQTC FOP for AASHTO T 99/T 180 by the State of Alaska DOT&PF.

1. Moisture content shall be determined using the mass requirements listed in table 2 of WAQTC FOP for AASHTO T 255/T 265.
2. In order to properly draw the moisture-density curve, it may be helpful to plot a Zero Air Voids curve. To plot the curve, you will need to establish the specific gravity of the soil. Specific gravity of the soil can be estimated at 2.700 or it can be determined in accordance with AASHTO T 100.

1. The points for plotting the ZAV shall be calculated by selecting dry unit masses and calculating a corresponding moisture content value as follows:

$$W_s = \frac{(\gamma_w)G_s - \gamma d}{(\gamma d)(G_s)} \times 100$$

Where:
W_s = Water content for complete saturation, %
γ_w = Unit Mass of water 9.789 kN/m^3 (62.4 lbf/ft^2)
γd = Dry unit mass of soil, kN/m^3 (lbf/ft^2)
G_s = specific Gravity of soil

2. When the material includes plus 4.75 mm (No. 4) materials, the plus 4.75 mm (No. 4) specific gravity may be estimated at 2.700 or it can be tested in accordance with WAQTC FOP for AASHTO T 85. If a weighted average is used, it shall be calculated as follows:

$$G_{avg} = \frac{1}{\frac{R_1}{100G_1} + \frac{P_1}{100G_2}}$$

Where:
G_{avg} = Weighted average specific gravity of soils
R_1 = Percent of soil particles retained on the 4.75 mm (No. 4) sieve
P_1 = Percent of soil particles passing the 4.75 mm (No. 4) sieve
G_1 = Apparent specific gravity of soil particles retained on the 4.75 mm (No. 4) sieve
G_2 = Specific gravity of soil particles passing the 4.75 mm (No. 4) sieve

3. Unless stated otherwise, T 180 shall be used.
4. The use of an extruder is optional when the sample being tested is granular.

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Determining the Standard Density of Coarse Granular Materials Using the Vibratory Compactor   ATM 212

1. Scope

This method determines the maximum density values of granular materials for a standard compaction energy. The method accounts for variations in the maximum attainable density of a given material due to fluctuations in gradation.

With the specific gravity and the compacted density of the plus 4.75 mm (no. 4) and the minus 4.75 mm (No. 4) fractions, a chart and/or curve of standard density values versus percent passing the No. 4 sieve can be plotted.

This test method is applicable to granular materials with the gradation of the minus 75 mm (3 in) portion of the sample having 10-80 percent passing the 4.75 mm (No. 4) sieve and with the minus 4.75 mm (No. 4) portion of the sample having 10 percent or less passing the 75 µm (No. 200) sieve.

Note 1: The Vibratory Compaction Test was developed for sandy gravels whose fine fraction is non-plastic and highly permeable or free draining. When the fine fraction is primarily a soil with some plasticity and low permeability or not free draining, WAQTC FOP for AASHTO T 99/T 180 will be used. With borderline materials, both tests shall be applied, and the one yielding the highest unit weight value will be used.

2. Apparatus

- A vibratory spring-loaded compactor essentially conforming to specifications that can be obtained from the State Materials Engineer.
- Standard Mold and base with and a piston to fit inside the mold with a maximum 1.5 mm (1/16") clearance between piston and mold.
- A 0.014 m^3 (1/2 ft^3) mold with a piston to fit inside mold having a maximum 1.5 mm (1/16 in) clearance between piston and mold.

Note 2: The molds and pistons will be constructed of metal of such dimensions as to remain rigid and inflexible under test conditions.

- Spacer blocks of varying heights compatible with the compactor and pistons.
- Measuring device, accurate and readable to 0.1 mm (0.01 in) with a minimum 300 mm (6 in) length.
- A 75 mm (3 in) and a 4.75 mm (No. 4) sieve conforming to AASHTO M 92 requirements.
- Balance or scale: Capacity sufficient for the principle sample mass, readable to 0.1 percent or 0.1 g and meeting the requirements of AASHTO M 231.

Note 3: For the fine aggregate compaction test, this would require a scale with a capacity of at least 20 kg (45 lb) and readable to 5 g (0.01 lb) or better.

Note 4: For the fine aggregate moisture content, this would require a scale with a capacity of at least 1000 g and readable to 0.1 g or better.

Note 5: For the coarse aggregate compaction test, this would require a scale with a capacity of at least 20 kg (45 lb) and readable to 5 g (0.01 lb) or better.

- A 2.5 kg (5.5 lb) metal rammer conforming to the requirements of WAQTC FOP for AASHTO T 99.
- Tamping rod of straight steel, 16 mm (5/8 in) in diameter and approximately 400 mm (24 in) long having at least one end rounded to a hemispherical tip.

- Graduated cylinder, 1000 ml capacity, readable to 5 ml.
- A stopwatch or timer accurate to 1 second.
- Miscellaneous tools including pans, spoon, trowel, mechanical mixer (optional), etc.

3. Equipment Calibration

Calibration data will be updated annually or more frequently if justified by use. Calibration information will be recorded and accessible for every test.

Calibration of the Standard Mold:

1. Measure the top and bottom diameter of the mold to the nearest 0.1 mm (0.01 in) and average the results to obtain the mean diameter of the mold. Calculate the area of the average diameter by the formula:

$$A = \pi \times (0.5 \times d)^2$$

Where:
A = Area of mean diameter, in^2 or mm^2,
π = 3.1416,
d = mean diameter, in or mm.

2. Assemble the mold, measure the overall height of the mold to the nearest 0.1 mm (0.01 in) at least 4 different places around the circumference of the mold and average the measurements. Record this as Height of Mold.

3. Calculate the Mold Conversion Factor by:

$$C = \frac{1{,}000{,}000{,}000}{A} \text{ or } \frac{1728}{A} \text{ USC}$$

Where:
C = Mold Conversion Factor, (1,000,000,000 = mm^3/m^3 and 1728 = in^3/ft^3),
A = Area of mean diameter.

4. Record the result as the Small Mold Conversion Factor to 0.01.

5. Calibration of the 0.014 m^3 Mold (Large): Calibrate this mold using the same procedure as described for the small mold above and record the result to 0.01 as the Large Mold Conversion Factor.

4. Sample Preparation

1. Sample the material in accordance with WAQTC FOP for AASHTO T 2. Prepare the field sample by splitting out a representative portion in accordance with WAQTC FOP for AASHTO T 248, Method A, to provide sufficient material for the following tests.
   - Sieve Analysis in accordance with WAQTC FOP for AASHTO T 27/T 11.
   - Coarse Aggregate Apparent Specific Gravity in accordance with WAQTC FOP for AASHTO T 85.
   - Fine Aggregate Apparent Specific Gravity in accordance with AASHTO T 84 or AASHTO T100.
   - Compaction sample to provide sufficient material for the compaction specimens detailed below.
2. Dry the compaction sample to constant mass in accordance with WAQTC FOP for AASHTO T 255.
3. Scalp the plus 75 mm (3 in) material from the compaction sample and discard, if not needed for any other tests. Separate the remainder of the compaction sample into coarse [minus 75 mm (3 in) to 4.75 mm (No. 4)] and fine [minus 4.75 mm (No. 4)] aggregate portions.

4. The quantity of material necessary to complete tests on both fractions is:
    a. Fine aggregate, minimum of 3 portions approximately 6 kg (13 lb) each.
    b. Coarse aggregate:
        1) For material containing 5 percent or less of 19.0 mm (3/4 in) material, a portion of the minus 19.0 mm (3/4 in) aggregate of approximately 6 kg (13 lb).
        2) For material containing more than 5 percent plus 19.0 mm (3/4 in) aggregate a portion of 18 to 20 kg (40 to 45 lb).

5. Procedure

1. Compaction Test of the Fine Fraction
    a. Assemble the Standard Mold and determine its mass, along with the Piston, to the nearest 5 g (0.01 lb). Record this as the Mass of Mold Assembly.
    b. Using one of the fine aggregate portions, add an amount of water estimated to produce a saturated sample when compacted and mix thoroughly.
        1) When the material is at its saturation point, free water (a drop or two) will show at the base of the mold at about the. 227 kg (500 lb) load of the first compression run. The ideal saturation point would be a bead of water around the base of the mold at the end of the 10-minute compaction run. Most materials will yield the highest density at that moisture content. Some materials may continue to gain density at higher moisture contents; however, this is due to the washing out of fines, which will alter the character of the sample. Therefore, if severe washing-out or pumping of fines occurs (as evidenced by dirty water flooding off of the base or pumped on top of the piston), the sample is beyond the saturation point, will be discarded and a lower moisture content tried for the saturation point.
        2) Moisture contents beyond the saturation point need not be tested.
    c. Set the piston aside and place the sample in the mold in three approximately equal layers. Consolidate each lift by 25 strokes of the tamping rod followed by 25 blows of the manual rammer. If severe displacement of the material occurs, adjust the blow strength by limiting the height of each blow to produce the maximum compaction and minimum displacement. The surface of the top lift should be finished as level as possible.
    d. Place the piston on top of the sample and mount the mold on the jack platform in the compactor. Spacers between the load spring and piston must be used to adjust the elevation of the mold so the hammers strike the mold in the center of the lift area. Elevate the mold until the loading head seats on top of the piston. Apply an initial seating load of approximately 45 kg (100 lbs) on the sample.
    e. Start the vibratory hammers and, by elevating the jack, begin the loading rate procedure.

The load application rate to 2000 lbs. is applied as follows:

Load	Elapsed Time
0 to 225 kg (500 lb)	1 minute
225 kg to 450 kg (1000 lb)	1-1/2 minutes
450 kg to 900 kg (2000 lb)	2 minutes

f. Upon reaching the 900 kg (2000 lb) load at the end of the 2-minute cycle, stop the hammers, release the load on the jack, and return to zero pressure.

g. Repeat Steps (e) and (f) four additional times. After the last run remove the mold from the compactor.

h. Measure the height of the compacted sample, to the top of the piston, to the nearest 0.1 mm (0.01 in) by measuring from the top of the mold to the surface of the sample at a minimum of 4 different places evenly spaced around the circumference of the mold. Record and average these measurements. Subtract this average from the overall height of the mold and record as the Height of Sample.

i. Determine the mass of the specimen in the mold to the nearest 5 g (0.01 lb). Record this as Mass of Mold Assembly + Aggregate.

j. Remove the specimen from the mold and determine the moisture content in accordance with WAQTC FOP for AASHTO T 255, recording the data on the Vibratory Compaction Worksheet.

k. Repeat Steps (b) thru (j) at lower or higher moisture content increments of approximately 1 percent intervals to determine the maximum density value for the material. Three tests are usually sufficient.

2. Compaction Test of the Coarse Fraction:

   a. For minus 19 mm (3/4 in) aggregates:

      1) Determine the mass of the coarse aggregate to the nearest 5 g (0.01 lb). Record this mass as Net Mass of Coarse Aggregate.

      2) Add 2.5 percent moisture to the sample, mix thoroughly and place in the Standard C.B.R. mold in approximately three equal lifts. Compact each lift with 25 blows of the tamping rod (omit hammering). Avoid the loss of any material during this operation, or the net mass of coarse aggregate must be determined again, after determining the height of the sample and drying the material to constant mass.

      3) Follow the procedures outlined in steps 1d. through 1g.

   b. For plus 19 mm (3/4 in) aggregates:

      1) Determine the mass of the coarse aggregate to the nearest 5 g (0.01 lb) or better. Record this mass the Net Mass of Coarse Aggregate.

      2) Divide the sample into three representative and approximately equal portions.

      3) Place one of the portions into the 0.014 m^3 (1/2 ft^3) mold. Level the surface by hand and consolidate the layer with 25 strokes of the tamping rod, using the rounded end. Distribute the strokes evenly over the entire cross section of the material rodding full depth, if possible, without hitting the bottom too hard.

4) Repeat this procedure for the other lifts, penetrating, if possible, into the lower layer. Avoid the loss of any material during this operation, or the net mass of coarse aggregate must be re-determined after determining the height of the sample.

4. Position the piston on the sample, mount the mold in the compactor and follow the procedure described in steps 1d. through 1g.

6. Calculations

1. Determine the dry density of each of the fine aggregate points as follows:

   a. Calculate the net mass of aggregate by:

$$e = c - d$$

Where:
e = net mass of aggregate, kg (lb)
c = mass of mold assembly + aggregate, kg (lb)
d = mass of mold assembly.

   b. Calculate the wet density by:

$$g = \frac{e \times b}{f}$$

Where:
g = wet unit weight, kg/m^3 (lb/ft^3)
e = net mass of aggregate, kg (lb)
b = mold conversion factor, metric (USC), and
f = height of sample, mm (in).

   c. Calculate the dry density of each of the fine fraction specimens as follows:

$$h = \frac{g}{1+n}$$

Where:
h = dry density for moisture content n, kg/m^3 (lb/ft^3)
g = wet density, kg/m^3 (lb/ft^3)
n = moisture content, expressed as a decimal.

   d. The maximum dry density (D_f) for the fine fraction is the highest density at or below the saturation point.

2. Calculate the maximum dry density (D_C) of the coarse fraction by:

$$D_c = \frac{u \times r}{v}$$

Where:
D_C = dry unit weight, kg/m^3 (lb/ft^3)
u = net mass of aggregate, kg (lb)
r = mold conversion factor, metric (USC)
v = height of sample, mm (in).

3. Determine the apparent specific gravity of the fine aggregate in accordance with AASHTO T 84.

4. Determine the apparent specific gravity of the coarse aggregate in accordance with WAQTC FOP for AASHTO T 85.
5. Plotting the "Maximum Dry Density vs. the Percent Passing 4.75 mm (No. 4) Sieve" curve is based on complex theoretical formulae. Programs for solution of these formulae, which produce curve data points and charts, have been developed for spreadsheets. These programs are available from the Statewide/ Regional laboratories.

7. Report

The results shall be reported on Department forms. In addition to the standard conformance tests for the material, in chart form the Maximum Dry Density shall be reported to the nearest 1 kg/m^3 (0.1 lb/ft^3) vs. the Percent Passing 4.75 mm (No. 4) in whole percentages from 0 to 100 percent. The data may be displayed graphically in addition to the chart.

IN-PLACE DENSITY AND MOISTURE CONTENT OF SOIL AND SOIL-AGGREGATE BY NUCLEAR METHODS (SHALLOW DEPTH) (See Addendum for DOT&PF Guidelines)
FOP FOR AASHTO T 310

Scope

This procedure covers the determination of density, moisture content, and relative compaction of soil, aggregate, and soil-aggregate mixes in accordance with AASHTO T 310. This field operating procedure is derived from AASHTO T 310. The nuclear moisture-density gauge is used in the direct transmission mode.

Apparatus

- Nuclear density gauge with the factory matched standard reference block.
- Drive pin, guide/scraper plate, and hammer for testing in direct transmission mode.
- Transport case for properly shipping and housing the gauge and tools.
- Instruction manual for the specific make and model of gauge.
- Radioactive materials information and calibration packet containing:
  - Daily Standard Count Log.
  - Factory and Laboratory Calibration Data Sheet.
  - Leak Test Certificate.
  - Shippers Declaration for Dangerous Goods.
  - Procedure Memo for Storing, Transporting and Handling Nuclear Testing Equipment.
  - Other radioactive materials documentation as required by local regulatory requirements.
- Sealable airtight containers and utensils for moisture content determinations.

Radiation Safety

This method does not purport to address all of the safety problems associated with its use. This test method involves potentially hazardous materials. The gauge utilizes radioactive materials that may be hazardous to the health of the user unless proper precautions are taken. Users of this gauge must become familiar with the applicable safety procedures and governmental regulations. All operators will be trained in radiation safety prior to operating nuclear density gauges. Some agencies require the use of personal monitoring devices such as a thermoluminescent dosimeter or film badge. Effective instructions together with routine safety procedures such as source leak tests, recording and evaluation of personal monitoring device data, etc., are a recommended part of the operation and storage of this gauge.

Calibration

Calibrate the nuclear gauge as required by the agency. This calibration may be performed by the agency using manufacturer's recommended procedures or by other facilities approved by the agency. Verify or re-establish calibration curves, tables, or equivalent coefficients every 12 months.

Standardization

1. Turn the gauge on and allow it to stabilize (approximately 10 to 20 minutes) prior to standardization. Leave the power on during the day's testing.
2. Standardize the nuclear gauge at the construction site at the start of each day's work and as often as deemed necessary by the operator or agency. Daily variations in standard count shall not exceed the daily variations established by the manufacturer of the gauge. If the daily variations are exceeded after repeating the standardization procedure, the gauge should be repaired and or recalibrated.
3. Record the standard count for both density and moisture in the Daily Standard Count Log. The exact procedure for standard count is listed in the manufacturer's Operators Manual.

***Note 1*:** New standard counts may be necessary more than once a day. See agency requirements.

Overview

There are two methods for determining in-place density of soil / soil aggregate mixtures. See agency requirements for method selection.

- Method A Single Direction
- Method B Two Direction

Procedure

1. Select a test location(s) randomly and in accordance with agency requirements. Test sites should be relatively smooth and flat and meet the following conditions:
    a. At least 10 m (30 ft) away from other sources of radioactivity
    b. At least 3 m (10 ft) away from large objects
    c. The test site should be at least 150 mm (6 in.) away from any vertical projection, unless the gauge is corrected for trench wall effect.
2. Remove all loose and disturbed material, and remove additional material as necessary to expose the top of the material to be tested.
3. Prepare a flat area sufficient in size to accommodate the gauge. Plane the area to a smooth condition so as to obtain maximum contact between gauge and the material being tested. For Method B, the flat area must be sufficient to permit rotating the gauge 90 or 180 degrees about the source rod.
4. Fill in surface voids beneath the gauge with native fines passing the 4.75 mm (No. 4) sieve or finer. Smooth the surface with the guide plate or other suitable tool. The depth of the native fines filler should not exceed approximately 3 mm (1/8 in.).
5. Make a hole perpendicular to the prepared surface using the guide plate and drive pin. The hole shall be at least 50 mm (2 in.) deeper than the desired probe depth, and shall be aligned such that insertion of the probe will not cause the gauge to tilt from the plane of the prepared area. Remove the drive pin by pulling straight up and twisting the extraction tool.

6. Place the gauge on the prepared surface so the source rod can enter the hole without disturbing loose material.
7. Insert the probe in the hole and lower the source rod to the desired test depth using the handle and trigger mechanism.
8. Seat the gauge firmly by partially rotating it back and forth about the source rod. Ensure the gauge is seated flush against the surface by pressing down on the gauge corners, and making sure that the gauge does not rock.
9. Pull gently on the gauge to bring the side of the source rod nearest to the scaler/detector firmly against the side of the hole.
10. Perform one of the following per agency requirements:
    a. **Method A Single Direction:** Take a test consisting of the average of two, one minute readings, and record both density and moisture data. The two wet density readings should be within 32 kg/m^3 (2 lb/ft^3) of each other. The average of the two wet densities and moisture contents will be used to compute dry density.
    b. **Method B Two Direction:** Take a one-minute reading and record both density and moisture data. Rotate the gauge 90 degrees or 180, pivoting it around the source rod. Reseat the gauge by pulling gently on the gauge to bring the side of the source rod nearest to the scaler/detector firmly against the side of the hole and take one-minute reading. (In trench locations, rotate the gauge 180 degrees for the second test.) Some agencies require multiple one-minute readings in both directions. Analyze the density and moisture data. A valid test consists of wet density readings in both gauge positions that are within 50 kg/m^3 (3 lb/ft^3). If the tests do not agree within this limit, move to a new location. The average of the wet density and moisture contents will be used to compute dry density.
11. If required by the agency, obtain a representative sample of the material, 4 kg (9 lb) minimum, from directly beneath the gauge full depth of material tested. This sample will be used to verify moisture content and / or identify the correct density standard. Immediately seal the material to prevent loss of moisture.

    The material tested by direct transmission can be approximated by a cylinder of soil approximately 300 mm (12 in.) in diameter directly beneath the centerline of the radioactive source and detector. The height of the cylinder will be approximately the depth of measurement. When organic material or large aggregate is removed during this operation, disregard the test information and move to a new test site.

12. To verify the moisture content from the nuclear gauge, determine the moisture content with a representative portion of the material using the FOP for AASHTO T 255/T 265 or the FOP for AASHTO T 217. If the moisture content from the nuclear gauge is within ±1% the nuclear gauge readings can be accepted. Retain the remainder of the sample at its original moisture content for a one-point compaction test under the FOP for AASHTO T 272, or for gradation, if required.

    Note 2: Example: A Gauge reading of 16.8% moisture and an oven dry of 17.7% are within the ±1% requirements. Moisture correlation curves will be developed according to agency guidelines. These curves should be reviewed and possibly redeveloped every 90 days.

13. Determine the dry density by one of the following.

a. From nuclear gauge readings, compute by subtracting the mass (weight) of the water (kg/m^3 or lb/ft^3) from the wet density (kg/m^3 or lb/ft^3) or compute using the % moisture by dividing wet density from the nuclear gauge by 1 + moisture content expressed as a decimal.

b. When verification is required and the nuclear gauge readings cannot be accepted, the moisture content is determined by the FOP for AASHTO T 255/T 265 or the FOP for AASHTO T 217, compute dry density by dividing wet density from the nuclear gauge by 1 + moisture content expressed as a decimal.

Percent Compaction

- Percent compaction is determined by comparing the in-place dry density as determined by this procedure to the appropriate agency density standard. For soil or soil-aggregate mixes, these are moisture-density curves developed using the FOP for AASHTO T 99/ T 180. When using curves developed by the FOP for AASHTO T 99 / T 180, it may be necessary to use the FOP for AASHTO T 224 and FOP for AASHTO T 272 to determine maximum density and moisture determinations.

  For coarse granular materials, the density standard may be density-gradation curves developed using a vibratory method such as AKDOT&PF's ATM 212, ITD's T 74, WSDOT's TM 606, or WFLHD's Humphrys.

  See appropriate agency policies for use of density standards.

Calculation

Wet Density readings from gauge: 1963 kg/m^3 (121.6 lb/ft^3)
1993 kg/m^3 (123.4 lb/ft^3)

Ave: 1978 kg/m^3 (122.5 lb/ft^3)

Moisture readings from gauge: 14.2% & 15.4% = Ave 14.8%

Moisture content from the FOP's for AASHTO T 255/ T 265 or T 217: 15.9%

Moisture content is greater than 1% different so the gauge moisture cannot be used.

Calculate the dry density as follows:

$$\rho_d = \left(\frac{\rho_w}{w + 100} \right) \times 100 \qquad \text{or} \qquad \rho_d = \left(\frac{\rho_w}{\frac{w}{100} + 1} \right)$$

Where:

ρ_d = Dry density, kg/m^3 (lb/ft^3)
ρ_w = Wet density, kg/m^3 (lb/ft^3)
w = Moisture content from the FOP's for AASHTO T 255 / T 265 or T 217, as a percentage

$$\rho_d = \left(\frac{1978 kg/m^3 or 122.5 lb/ft^3}{15.9 + 100} \right) \times 100 \qquad \rho_d = \left(\frac{1978 kg/m^3 or 122.5 lb/ft^3}{\frac{15.9}{100} + 1} \right)$$

Corrected for moisture Dry Density: 1707 kg/m^3 (105.7 lb/ft^3)

Report

Results shall be reported on standard forms approved by the agency. Include the following information:

- Location of test, elevation of surface, and thickness of layer tested.
- Visual description of material tested.
- Make, model and serial number of the nuclear moisture-density gauge.
- Wet density.
- Moisture content as a percent, by mass, of dry soil mass.
- Dry density.
- Standard density.
- Percent compaction.
- Name and signature of operator.

Addendum WAQTC for AASHTO T 310

Following are guidelines for the use of WAQTC FOP for AASHTO T 310 by the State of Alaska DOT&PF.

1. The procedure designated as Method A will be used.
2. Record density to the nearest 0.1 lb/ft^2 and moisture to the nearest 0.1%.
3. Report percent compaction to the nearest whole percent.
4. WAQTC FOP for AASHTO T 217 will not be used.
5. The visual description of the material will be the material classification, i.e. Borrow, D-1, etc.
6. The offset factor (k) shall be used to correct the moisture content reading from the gauge.
   a. Determine the offset factor (k) by:
      1) Average five gauge derived moisture contents. .
      2) Average 5 moisture contents determined by WAQTC FOP for AASHTO T 255/T 265 taken from the locations used to determine the gauge derived moistures.
      3) Calculate the offset factor (k) using the following formula.

$$k = \frac{\%M_{LAB} - \%M_{GAUGE}}{100 + \%M_{GAUGE}} \times 1000$$

   b. Follow the gauge Manufacturer's instructions to enable the offset function to correct the moisture reading.
   c. Be sure to disengage the offset function upon completion of test.

      Note: This procedure is set up for Troxler gauges (should note in Addendum)

5. When testing in place density on crushed materials, determine if you need to dig up a sample from the test location based on the following criteria.
   a. If the Standard Density is determined by ATM 212, and the test meets the minimum density requirement using the density from the peak of the curve, a sample is not required.
   b. If it does not meet the above condition or the Standard Density is determined using WAQTC FOP for AASHTO T 99/T 180, a sample may be required to determine the plus No. 4, minus No. 4 ratio for ATM 212, or the percent oversize for correcting the Standard Density determined by WAQTC FOP for AASHTO T 99/T 180 according to WAQTC FOP for AASHTO T 224.

CORRECTION FOR COARSE PARTICLES IN THE SOIL COMPACTION TEST
WAQTC FOP FOR AASHTO T 224 (See Addendum for DOT&PF Guidelines)

Scope

This procedure covers the adjustment of the maximum dry density determined by AASHTO T 99, or T 180 to compensate for coarse particles retained on the 4.75 mm (No. 4) or 19.0 mm (3/4 in.) sieve. For Methods A and B of AASHTO T 99 and T 180 the adjustment is based on the percent, by mass, of material retained on the 4.75 mm (No. 4) sieve and the bulk specific gravity G_{sb} of the material retained on the 4.75 mm (No. 4) sieve. A maximum of 40% of the material can be retained on the 4.75 mm (No. 4) sieve for this method to be used. For Methods C and D of AASHTO T 99 and AASHTO T 180, the adjustment is based on the percent, by mass, of material retained on the 19.0 mm (3/4 in.) sieve and the bulk specific gravity G_{sb} of the material retained on the 19.0 mm (3/4 in.) sieve. A maximum of 30% of the material can be retained on the 19.0 mm (3/4 in.) sieve for this method to be used. Whether the split is on the 4.75 mm (No. 4) or the 19.0 mm (3/4 in.) sieve all material retained on that sieve is defined as oversized material.

This method applies to soils with percentages up to the maximums listed above for oversize particles. A correction may not be practical for soils with only a small percentage of oversize material. Agency shall specify a minimum percentage below which the method is not needed. If not specified, this method applies when more than 5 percent by weight of oversize particles is present.

Adjustment Equation

Along with density the moisture content can be corrected. The moisture content can be determined by the FOP for AASHTO T 255 / T 265, FOP for AASHTO T 217, or the nuclear density gauge moisture content reading from the FOP for AASHTO T 310. If the nuclear gauge moisture reading is used or when the moisture content is determined on the entire sample (both fine and oversized particles) the use of the adjustment equation is not needed. Combined moisture contents with material having an appreciable amount of silt or clay should be performed using FOP for AASHTO T 255 / T 265 (Soil). Moisture contents used from FOP for AASHTO T 310 must meet the criteria for that method.

When samples are split for moisture content (oversized and fine materials) the following adjustment equations must be followed.

1. Split the sample into oversized material and fine material.
2. Dry the oversized material following the FOP for AASHTO T 255 / T 265 (Aggregate). If the fine material is sandy in nature dry using the FOP for AASHTO T 255 / T 265 (Aggregate), or FOP for AASHTO T 217. If the fine material has any appreciable amount of clay, dry using the FOP for AASHTO T 255 / T 265 (Soil) or FOP for AASHTO T 217.
3. Calculate the dry mass of the oversize and fine material as follows.

$$M_D = \frac{M_m}{(1 + MC)}$$

Where:

M_D = mass of dry material (fine or oversize particles).

M_m = mass of moist material (fine or oversize particles).

MC = moisture content of respective fine or oversized, expressed as a decimal.

4. Calculate the percentage of the fine and oversized particles by dry weight of the total sample as follows: See note 2.

$$P_f = \frac{100\, M_{DF}}{(M_{DF} + M_{DC})} \qquad 73.0\% = \frac{(100)\,(15.4\text{ lbs})}{(15.4\text{lbs} + 5.7lbs)} \qquad 73.0\% = \frac{(100)\,(7.034\text{kg})}{(7.034\text{kg} + 2.602kg)}$$

And

$$P_c = \frac{100\, M_{DC}}{(M_{DF} + M_{DC})} \qquad 27.0\% = \frac{(100)\,(5.7\text{lbs})}{(15.4\text{lbs} + 5.7lbs)} \qquad 27.0\% = \frac{(100)\,(2.602\text{kg})}{(7.034\text{kg} + 2.602kg)}$$

Or for P_c $\quad P_c = 100 - P_f$

Where:

P_f = percent of fine particles, of sieve used, by weight.

P_C = percent of oversize particles, of sieve used, by weight.

M_{DF} = mass of fine particles.

M_{DC} = mass of oversize particles.

5. Calculate the corrected moisture content as follows:

$$MC_T = \frac{[(MC_F)\,(P_f) + (MC_c)(P_c)]}{100} \qquad 8.3\% = \frac{[(10.6)\,(73.0) + (2.1)(27.0)]}{100}$$

MC_T = corrected moisture content of combined fines and oversized particles, expressed as a % moisture.

MC_F = moisture content of fine particles, as a % moisture.

MC_C = moisture content of oversized particles, as a % moisture.

Note 1: Moisture content of oversize material can be assumed to be two (2) percent for most construction applications.
Note 2: In some field applications agencies will allow the percentages of oversize and fine materials to be determined with the materials in the wet state.

Adjustment Equation Density

6. Calculate the corrected dry density of the total sample (combined fine and oversized particles) as follows:

$$D_d = \frac{100\, D_f k}{[(D_f)(P_c) + (k)(P_f)]} \quad \text{or} \quad D_d = \frac{100}{\frac{P_f}{D_f} + \frac{P_c}{k}}$$

Where:

D_d = corrected total dry density (combined fine and oversized particles) kg/m^3 (lb/ft^3).
D_f = dry density of the fine particles kg/m^3 (lb/ft^3), determined in the lab.
P_C = percent of oversize particles, of sieve used, by weight.
P_f = percent of fine particles, of sieve used, by weight.
k = Metric:
1,000 * Bulk Specific Gravity (G_{sb})
(oven dry basis) of coarse particles (kg/m^3).

k = English:
62.4 * Bulk Specific Gravity (G_{sb})
(oven dry basis) of coarse particles (lb/ft^3).

Note 3: If the specific gravity is known, then this value will be used in the calculation. For most construction activities the specific gravity for aggregate may be assumed to be 2.600.

Calculation

06

Sample Calculations:

- Metric:

Maximum laboratory dry density (D_f):	2329 kg/m^3
Percent coarse particles (P_C):	27%
Percent fine particles (P_f):	73%
Mass per volume coarse particles (k):	(2.697) (1000) = 2697 kg/m^3

$$D_d = \frac{(100)\,(2329 kg/m^3)(2697 kg/m^3)}{[(2329 kg/m^3)\,(27) + (2697 kg/m^3)(73)]}$$

$$D_d = \frac{628{,}131{,}300.0}{[62{,}883.0 + 196{,}881]}$$

$$D_d = \frac{628{,}131{,}300.0}{259{,}764.0}$$

$D_d = 2418.1$ say $2418\ kg/m^3$

- English:

  Maximum laboratory dry density (D_F): 140.4 lb/ft^3
  Percent coarse particles (P_C): 27%
  Percent fine particles (Pf): 73%
  Mass per volume of coarse particles (k): (2.697) (62.4) = 168.3 lb/ft^3

$$D_d = \frac{(100)\,(140.4\ lb/ft^3)(168.3\ lb/ft^3)}{[(140.4\ lb/ft^3)\,(27) + (168.3 lb/ft^3)(73)]}$$

$$D_d = \frac{2{,}362{,}932.0}{[3790.8 + 12285.9]}$$

$$D_d = \frac{2{,}362{,}932.0}{16{,}076.7}$$

$D_d = 146.98$ say $147.0\ lb/ft^3$

Report

Results shall be reported on standard forms approved by the agency. Report adjusted maximum dry density to the closest 1 kg/m^3 (0.1 lb/ft^3).

Addendum WAQTC FOP for AASHTO T 224

Following are guidelines for the use of WAQTC FOP for AASHTO T 224 by the State of Alaska DOT&PF.

1. The maximum allowable oversized (+3/4" (19 mm)) material is 40 percent. The maximum dry density to be used with material containing 30 to 40 percent oversized is the oversized correction calculated at 30 percent.

2. When materials has more than 40% retained on the 3/4" (19mm) sieve, record the percent oversize, the moisture content, and record the test as Too Coarse To Test (TCTT).

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SAMPLING OF AGGREGATES (See Addendum for DOT&PF Guidelines)
FOP FOR AASHTO T 2

Scope

This procedure covers sampling of fine and coarse aggregates (FA and CA) in accordance with AASHTO T 2. Sampling from conveyor belts, transport units, roadways, and stockpiles is covered.

The specifications for some materials may require the contractor to provide a mechanical sampling system at crushers, screening operations, and mixing plants. This system is normally a permanently attached device that allows a sample container to pass perpendicularly through the entire stream of material or diverts the entire stream of material into the container. The sample container is normally larger at the bottom than the top (triangular shaped), with the slotted opening in the top based on the size of aggregate being sampled.

Operation may be hydraulic, pneumatic, or manual, and shall allow the sample container to pass through the stream at least twice, once in each direction, without overfilling. With manually operated systems, a consistent operating speed is difficult to maintain and may result in variably sized, non-representative samples. For this reason, some agency specifications require that the sampling device be automatic or semi-automatic.

Apparatus

- Shovels, scoops, sampling tubes of acceptable dimensions.
- Custom built sampling devices suitable for varied sampling scenarios, and sampling containers.

Procedure - General

Sampling is as important as testing, and the technician shall use every precaution to obtain samples that will show the true nature and condition of the materials the sample represents.

1. Wherever samples are taken, obtain multiple increments of approximately equal size..

2. Mix the increments thoroughly to form a field sample that meets or exceeds the minimum mass recommended in Table 1.

   Note 1: Based upon the tests required, the sample size may be four times that shown in Table 1 of the FOP for AASHTO T 27/T 11, if that mass is more appropriate. As a general rule the field sample size should be such that, when split twice will provide a testing sample of proper size.

Table 1
Sample Sizes

Nominal Maximum Size* mm (in.)		Minimum Mass g (lb)	
2.36	(No. 8)	10,000	(25)
4.75	(No. 4)	10,000	(25)
9.5	(3/8)	10,000	(25)
12.5	(1/2)	15,000	(35)
19.0	(3/4)	25,000	(55)
25.0	(1)	50,000	(110)
37.5	(1 1/2)	75,000	(165)
50	(2)	100,000	(220)
63	(2 1/2)	125,000	(275)
75	(3)	150,000	(330)
90	(3 1/2)	175,000	(385)

* One sieve larger than the first sieve to retain more than 10 percent of the material using an agency specified set of sieves based on cumulative percent retained. Where large gaps in specification sieves exist, intermediate sieve(s) may be inserted to determine nominal maximum size. Maximum size is one size larger than nominal maximum size.

Procedure – Specific Situations

In all situations, determine the time or location for sampling in a random manner.

A. Conveyor Belts

Avoid sampling at the beginning or end of the aggregate run due to the potential for segregation.

Method A (From the Belt): Stop the belt. Set the sampling device in place on the belt, avoiding intrusion by adjacent material. Scoop off the sample, including all fines. Obtain a minimum of 3 increments.

Method B (From the Belt Discharge): Pass a sampling device through the full stream of the material as it runs off the end of the conveyor belt. The sampling device may be manually, semi-automatic or automatically powered. The sample container shall pass through the stream at least twice, once in each direction, without overfilling while maintaining a constant speed during the sampling process.

B. Transport Units

Divide the unit into four quadrants. Dig down approximately 0.3 m (1 ft) in each quadrant and obtain material. Combine to form a single sample.

C. Roadways

Obtain three increments of approximately equal size and combine. Take the full depth of the material to be sampled, being careful to exclude underlying material.

Note 2: If from a berm or windrow the entire cross-section must be sampled after the last mixing pass and prior to spreading and compacting. This may yield extra large samples and may not be the preferred sampling location. Do not sample from the beginning or the end of a berm or windrow.

D. Stockpiles

Note 3: Sampling at stockpiles should be avoided whenever possible due to problems involved in obtaining a representative gradation of material

1. Create, with a loader if one is available, vertical faces in the top, middle, and bottom third of the stockpile. When no equipment is available a shovel may be used to create vertical faces.
2. Prevent sloughing by shoving a flat board in against the vertical face. Sample from the horizontal surface at the intersection of the horizontal and vertical faces. Take at least one increment from each of the top, middle, and bottom thirds of the pile and combine.
3. When sampling sand, remove the outer layer that may have become segregated. Using a sampling tube, obtain material from five random locations on the pile and mix thoroughly to form one sample.

Addendum WAQTC FOP for AASHTO T 2

Following are guidelines for the use of WAQTC FOP for AASHTO T 2 by the State of Alaska DOT&PF.

1. When sampling sand from a stockpile, the use of the sampling tube is optional.
2. Table 1, Minimum (Field) Sample Size, is modified to allow for reduced sample sizes in accordance with the Alaska DOT&PF Guidelines for WAQTC FOP for AASHTO T 27/T 11 (i.e. the field sample size is such that when split twice, it will provide a testing sample of proper size for WAQTC FOP for AASHTO T 27/T 11).

Table 1
Sample Sizes

Nominal Maximum Size*,		Minimum Mass,	
Standard mm	Alternate inches	kg	lb
2.36	No. 8	10	25
4.75	No. 4	10	25
9.5	3/8”	10	25
12.5	1/2”	15	35
19.0	3/4”	25	55
25.0	1”	45	100
37.5	1/1/2”	65	145
50	2”	85	190
75	3”	125	275

*Nominal Maximum Size: One sieve larger than the first sieve to retain more than 10 percent of the material using an agency specified set of sieves based on cumulative percent retained. Where large gaps in specification sieves exist, intermediate sieve(s) may be inserted to determine nominal maximum size.

REDUCING SAMPLES OF AGGREGATES TO TESTING SIZE
FOP FOR AASHTO T 248 (See Addendum for DOT&PF Guidelines)

Scope

This procedure covers the reduction of samples to the appropriate size for testing in accordance with AASHTO T 248. Techniques are used that minimize variations in characteristics between test samples and field samples. Method A (Mechanical Splitter) and Method B (Quartering) are covered.

This procedure applies to fine aggregate (FA), coarse aggregate (CA), and mixes of the two, and may also be used on soils.

Samples of fine aggregates that are drier than the saturated surface dry (SSD) condition shall be reduced by a mechanical splitter according to Method A. Samples of FA that are at SSD or wetter than SSD shall be reduced by Method B, or the entire sample may be dried to the SSD condition, using temperatures that do not exceed those specified for any of the tests contemplated, and then reduced to test sample size using Method A. Samples of CA or mixtures of FA and CA may be reduced by either method. As a quick determination, if the fine aggregate will retain its shape when molded with the hand it is wetter that SSD.

Apparatus

Method A – Mechanical Splitter

Splitter chutes:

- Even number of equal width chutes
- Discharge alternately to each side
- Minimum of 8 chutes for CA, 12 chutes for FA
- Width
  - Minimum 50 percent larger than largest particle
  - A maximum chute width of 19 mm (3/4 in.) for dry fine aggregate passing 9.5 mm (3/8 in.) sieve

Splitter receptacles:

- Capable of holding two halves of the sample following splitting.
- Hopper or straightedge pan width equal to or slightly less than the overall width of the assembly of chutes.
- Capable of feeding the splitter at a controlled rate.

The splitter and accessory equipment shall be so designed that the sample will flow smoothly without restriction or loss of material.

Method B – Quartering

- Straightedge scoop, shovel, or trowel
- Broom or brush
- Canvas or plastic sheet, approximately 2 by 3 m (6 by 9 ft)

Sample Preparation

If the FA sample is wetter than the SSD condition and Method A – Mechanical Splitter is to be used, dry the material using temperatures not exceeding those specified for any of the tests contemplated for the sample.

Note 1: It may be undesirable to split some FA / CA mixtures that are over SSD condition using Method A.

Procedure

Method A – Mechanical Splitter

Place the sample in the hopper or pan and uniformly distribute it from edge to edge so that approximately equal amounts flow through each chute. The rate at which the sample is introduced shall be such as to allow free flowing through the chutes into the hoppers below. Split the sample from one of the two hoppers as many times as necessary to reduce the sample to the size specified for the intended test. The portion of the material collected in the other receptacle may be reserved for reduction in size for other tests. As a check for effective splitting determine the mass of each part of the split. If the ratio of the two masses differs by more than 5 percent, corrective action must be taken.

Calculation

Splitter check: 5127 total sample mass

Splitter pan #1: 2583
Splitter pan #2: 2544

$$\frac{2544}{2583} \text{X}100 = 98.5 \qquad 100-98.5 = 1.5\%$$

Method B – Quartering

Use either of the following two procedures or a combination of both.

Procedure # 1: Quartering on a clean, hard, level surface:

1. Place the sample on a hard, clean, level surface where there will be neither loss of material nor the accidental addition of foreign material.
2. Mix the material thoroughly by turning the entire sample over a minimum of three times. With the last turning, shovel the entire sample into a conical pile by depositing each shovelful on top of the preceding one.
3. Flatten the conical pile to a uniform thickness and diameter by pressing down with a shovel. The diameter should be four to eight times the thickness.
4. Divide the flattened pile into four approximately equal quarters with a shovel or trowel.
5. Remove two diagonally opposite quarters, including all fine material, and brush the cleared spaces clean.
6. Successively mix and quarter the remaining material until the sample is reduced to the desired size.
7. The final test sample consists of <u>two diagonally opposite</u> quarters.

Procedure # 2: Quartering on a canvas or plastic sheet:

1. Place the sample on the sheet.
2. Mix the material thoroughly by turning the entire sample over a minimum of three times. Lift each corner of the sheet and pulling it over the sample toward the diagonally opposite corner, causing the material to be rolled. With the last turning, form a conical pile.
3. Flatten the conical pile to a uniform thickness and diameter by pressing down with a shovel. The diameter should be four to eight times the thickness.
4. Divide the flattened pile into four approximately equal quarters with a shovel or trowel, or, insert a stick or pipe beneath the sheet and under the center of the pile, then lift both ends of the stick, dividing the sample into two roughly equal parts. Remove the stick leaving a fold of the sheet between the divided portions. Insert the stick under the center of the pile at right angles to the first division and again lift both ends of the stick, dividing the sample into four roughly equal quarters.
5. Remove two diagonally opposite quarters, being careful to clean the fines from the sheet.
6. Successively mix and quarter the remaining material until the sample size is reduced to the desired size.
7. The final test sample consists of <u>two diagonally opposite</u> quarters.

Addendum WAQTC FOP for AASHTO T 248

Following are guidelines for the use of WAQTC FOP for AASHTO T 248 by the State of Alaska DOT&PF.

1. When determining the correct number of chutes, the chutes will be a minimum of 50% larger than the largest particle, utilizing the maximum number of chutes possible.

SIEVE ANALYSIS OF FINE AND COARSE AGGREGATES
FOP FOR AASHTO T 27 (See Addendum for DOT&PF Guidelines)

MATERIALS FINER THAN 75 µm (No. 200) SIEVE IN MINERAL AGGREGATE BY WASHING (See Addendum for DOT&PF Guidelines)
FOP FOR AASHTO T 11

Scope

Sieve analyses determine the gradation or distribution of aggregate particles within a given sample in order to determine compliance with design and production standards.

Accurate determination of material smaller than 75 µm (No. 200) cannot be made with AASHTO T 27 alone. If quantifying this material is required, it is recommended that AASHTO T 27 be used in conjunction with AASHTO T 11. Following the procedure in AASHTO T 11, the sample is washed through a 75 µm (No. 200) sieve. The amount of material passing this sieve is determined by comparing dry sample masses before and after the washing process.

This procedure covers sieve analysis in accordance with AASHTO T 27 and materials finer than 75 µm (No. 200) in accordance with AASHTO T 11 performed in conjunction with AASHTO T 27. The procedure includes three method choices, A, B and C.

Apparatus

- Balance or scale: Capacity sufficient for the masses shown in Table 1, accurate to 0.1 percent of the sample mass or readable to 0.1 g. Meeting the requirements of AASHTO M 231.
- Sieves – Meeting the requirements of AASHTO M 92.
- Mechanical sieve shaker – Meeting the requirements of AASHTO T 27.
- Suitable drying equipment (see FOP for AASHTO T 255).
- Containers and utensils: A pan or vessel of a size sufficient to contain the sample covered with water and to permit vigorous agitation without loss of any part of the sample or water.
- Optional Mechanical washing device

Sample Preparation

Obtain samples in accordance with the FOP for AASHTO T 2 and reduce to the size shown in Table 1 in accordance with the FOP for AASHTO T 248.
These sample sizes are standard for aggregate testing but, due to equipment restraints, samples may need to be partitioned into several "subsamples." For example, a gradation that requires 100 kg (220 lbs) of material would not fit into a large tray shaker in one batch.

Some agencies permit reduced sample sizes if it is proven that doing so is not detrimental to the test results. Some agencies require larger sample sizes.
Check agency guidelines for required or permitted test sample sizes.

Table 1
Sample Sizes for Aggregate Gradation Test

Nominal Maximum Size* mm (in.)		Minimum Mass g (lb)	
4.75	(No. 4)	500	(1)
6.3	(1/4)	1000	(2)
9.5	(3/8)	1000	(2)
12.5	(1/2)	2000	(4)
19.0	(3/4)	5000	(11)
25.0	(1)	10,000	(22)
37.5	(1 1/2)	15,000	(33)
50	(2)	20,000	(44)
63	(2 1/2)	35,000	(77)
75	(3)	60,000	(130)
90	(3 1/2)	100,000	(220)
100	(4)	150,000	(330)
125	(5)	300,000	(660)

Nominal Maximum size: One sieve larger than the first sieve to retain more than 10 percent of the material using an agency specified set of sieves based on cumulative percent retained. Where large gaps between specification sieves exist, intermediate sieve(s) may be inserted to determine nominal maximum size.

Selection of Procedure

Agencies may specify what method will be performed. If a method is not specified method A will be performed.

Overview

Method A

- Determine dry mass of original sample
- Wash through a 75µm (No. 200) sieve
- Determine dry mass of washed sample
- Sieve material

Method B

- Determine dry mass of original sample
- Wash through a 75µm (No. 200) sieve
- Determine dry mass of washed sample
- Sieve coarse material
- Determine mass of fine material
- Reduce fine portion
- Determine mass of reduced portion
- Sieve fine portion

Method C

- Determine dry mass of original sample
- Sieve coarse material
- Determine mass of fine material
- Reduce fine portion
- Determine mass of reduced portion
- Wash through a 75µm (No. 200) sieve
- Determine dry mass of washed sample
- Sieve fine portion

Sample Sieving

In all procedures it is required to shake the sample over nested sieves. Sieves are selected to furnish information required by specification. The sieves are nested in order of decreasing size from the top to the bottom and the sample, or a portion of the sample, is placed on the top sieve.

Sieves are shaken in a mechanical shaker for approximately 10 minutes, or the minimum time determined to provide complete separation for the sieve shaker being used.

Time Evaluation

The minimum time requirement should be evaluated for each shaker at least annually, by the following method: Continue shaking for a sufficient period and in such a manner that, after completion, not more than 0.5 percent by mass of the total sample passes any sieve during one minute of continuous hand sieving.

Provide a snug-fitting pan and cover, and hold in a slightly inclined position in one hand. Strike the side of the sieve sharply and with an upward motion against the heel of the other hand at the rate of about 150 times per minute, turning the sieve about one sixth of a revolution at intervals of about 25 strokes. In determining sufficiency of sieving for sizes larger than 4.75 mm (No. 4), limit the material on the sieve to a single layer of particles.

Overload Determination

Additional sieves may be necessary to provide other information, such as fineness modulus, or to keep from overloading sieves. The sample may also be sieved in increments. For sieves with openings smaller than 4.75 mm (No. 4), the mass retained on any sieve shall not exceed 7 kg/m^2 (4 g/in^2) of sieving surface. For sieves with openings 4.75 mm (No. 4) and larger, the mass, in grams shall not exceed the product of 2.5 x (sieve opening in mm) x (effective sieving area). See Table 2.

Table 2
Maximum Allowable Mass of Material Retained on a Sieve, g
Nominal Sieve Size, mm (in.)
exact size is smaller see AASHTO T 27

Sieve Size mm (in.)		203 ϕ (8)	305 ϕ (12)	305 x 305 (12 x 12)	350 x 350 (14 x 14)	372 x 580 (16 x 24)
				Sieving Area m^2		
		0.0285	0.0670	0.0929	0.1225	0.2158
90	(3 1/2)	*	15,100	20,900	27,600	48,500
75	(3)	*	12,600	17,400	23,000	40,500
63	(2 1/2)	*	10,600	14,600	19,300	34,000
50	(2)	3600	8400	11,600	15,300	27,000
37.5	(1 1/2)	2700	6300	8700	11,500	20.200
25.0	(1)	1800	4200	5800	7700	13,500
19.0	(3/4)	1400	3200	4400	5800	10,200
16.0	(5/8)	1100	2700	3700	4900	8600
12.5	(1/2)	890	2100	2900	3800	6700
9.5	(3/8)	670	1600	2200	2900	5100
6.3	(1/4)	440	1100	1500	1900	3400
4.75	(No. 4)	330	800	1100	1500	2600
-4.75	(-No. 4)	200	470	650	1200	1300

Procedure Method A

1. Dry the sample to a constant mass in accordance with the FOP for AASHTO T 255, and record to the nearest 0.1 percent of the total sample mass or 0.1 g.
2. When the specification requires that the amount of material finer than 75 µm (No. 200) be determined, perform Step 3 through Step 9 otherwise, skip to Step 10.

3. Nest a sieve, such as a 2.0 mm (No. 10), above the 75 µm (No. 200) sieve.
4. Place the test sample in a container and add sufficient water to cover it.

Note 1: A detergent, dispersing agent, or other wetting solution may be added to the water to assure a thorough separation of the material finer than the 75 µm (No. 200) sieve from the coarser particles. There should be enough wetting agent to produce a small amount of suds when the sample is agitated. Excessive suds may overflow the sieves and carry material away with them.

5. Agitate vigorously to ensure complete separation of the material finer than 75 µm (No. 200) from coarser particles and bring the fine material into suspension above the coarser material. When using a mechanical washing device, exercise caution to not degrade the sample.
6. Immediately pour the wash water containing the suspended and dissolved solids over the nested sieves, being careful not to pour out the coarser particles.
7. Add a second change of water to the sample remaining in the container, agitate, and repeat Step 6. Repeat the operation until the wash water is reasonably clear. If a detergent or dispersing agent is used, continue washing until the agent is removed.
8. Remove the upper sieve and rinse the material retained on the 0.75 mm (No.200) sieve until water passing through the sieve is reasonably clear.

9. Return all material retained on the nested sieves to the container by flushing into the washed sample.
10. Dry the washed aggregate to constant mass in accordance with the FOP for AASHTO T 255, and then cool prior to sieving. Record the "dry mass after washing".
11. Select sieves to furnish the information required by the specifications. Nest the sieves in order of decreasing size from top to bottom and place the sample, or a portion of the sample, on the top sieve.
12. Place sieves in mechanical shaker and shake for the minimum time determined to provide complete separation for the sieve shaker being used approximately 10 minutes.

Note 2: Excessive shaking (more than 10 minutes) may result in degradation of the sample.

13. Determine the individual or cumulative mass retained on each sieve and the pan to the nearest 0.1 percent or 0.1 g. Ensure that all material trapped in the openings of the sieve are cleaned out and included in the mass retained.

Note 3: Use coarse wire brushes to clean the 600 µm (No. 30) and larger sieves, and soft bristle brushes for smaller sieves.

14. In the case of coarse / fine aggregate mixtures, the minus 4.75mm (No. 4) may be distributed among two or more sets of sieves to prevent overloading of individual sieves.

Calculations

The total mass of the material after sieving, for both coarse and fine portions should check closely with the original mass of sample placed on the sieves. If performing T 11 with T 27 this would be the dry mass after wash. If performing just T 27 this would be the original dry mass. When the masses before and after sieving differ by more than 0.3 percent do not use the results for acceptance purposes.

Calculate the total percentages passing, individual or cumulative percentages retained, or percentages in various size fractions to the nearest 0.1 percent by dividing the masses for method A, or adjusted masses for methods B and C, on the individual sieves by the total mass of the initial dry sample. If the same test sample was first tested by T 11, use the total dry sample mass prior to washing in T 11 as the basis for calculating all percentages. Report percent passing as indicated in the "Report" section at the end of this FOP.

Percent Retained:

Where:

IPR= Individual Percent Retained

CPR= Cumulative Percent Retained

M= Total Dry Sample mass before washing

IMR= Individual Mass Retained OR Adjusted Individual mass from Methods B or C

CMR= Cumulative Mass Retained OR Adjusted Individual mass From Methods B or C

$$IPR = \frac{IMR}{M} X100 \quad \textbf{OR} \quad CPR = \frac{CMR}{M} X100$$

Percent Passing (Calculated):

Where:

PP= Percent Passing

PPP= Previous Percent Passing

PP = PPP-IPR OR PP = 100-CPR

Method A Sample Calculation

Calculate percent retained on and passing each sieve on the basis of the total mass of the initial dry sample. This will include any material finer than 75 µm (No. 200) that was washed out.

Example:

Dry mass of total sample, before washing: 5168.7 g

Dry mass of sample, after washing out the 75µm (No. 200) minus: 4911.3 g

Amount of 75µm (No. 200) minus washed out: 5168.7 g – 4911.3 g = 257.4 g

Gradation on All Sieves

Sieve Size mm (in.)	Individual Mass Retained g	Individual Percent Retained	Cum. Mass Retained g	Cum. Percent Retained	Calc'd Percent Passing	Reported Percent Passing*
19.0 (3/4)	0	0	0	0.0	100.0	100
12.5 (1/2)	724.7	14.0	724.7	14.0	86.0	86
9.5 (3/8)	619.2	12.0	1343.9	26.0	74.0	74
4.75 (No. 4)	1189.8	23.0	2533.7	49.0	51.0	51
2.36 (No. 8)	877.6	17.0	3411.3	66.0	34.0	34
1.18 (No. 16)	574.8	11.1	3986.1	77.1	22.9	23
0.600 (No. 30)	329.8	6.4	4315.9	83.5	16.5	16
0.300 (No. 50)	228.5	4.4	4544.4	87.9	12.1	12
0.150 (No. 100)	205.7	4.0	4750.1	91.9	8.1	8
0.075 (No. 200)	135.4	2.6	4885.5	94.5	5.5	5.5
Pan	20.4		4905.9			

*Report 75 µm (No. 200) sieve to 0.1 percent. Report all others to 1 percent.

Check sum: [(4911.3 -4905.9) / 4911.3] X 100 = 0.11 % is within the 0.3 percent requirement.

Percent Retained:

$$9.5\text{ mm (3/8) Sieve } 12.0\% = \frac{619.0}{5168.7} X100 \text{ OR } \quad 26.0\% = \frac{1343.9}{5168.7} X100$$

Percent Passing (Calculated):

9.5 mm (3/8) Sieve 74.0% = 86.0 - 12.0 or 74.0% = 100 – 26.0

Procedure Method B

1. Perform steps 1 thru 10 from the "Procedure Method A" then continue as follows:
2. Select sieves to furnish information required by the specifications. Nest the sieves in order of decreasing size from top to bottom through the 4.75 mm (No.4) with a pan at the bottom to retain the minus 4.75 mm (No. 4).
3. Place the sample, or a portion of the sample, on the top sieve. Sieves may already be in the mechanical shaker or place the sieves in the mechanical shaker and shake for the minimum time determined to provide complete separation for the sieve shaker being used approximately 10 minutes.

Note 2: Excessive shaking (more than 10 minutes) may result in degradation of the sample.

4. Determine the individual or cumulative mass retained on each sieve to the nearest 0.1 percent or 0.1 g. Ensure that all material trapped in the openings of the sieve are cleaned out and included in the mass retained.

Note 3: Use coarse wire brushes to clean the 600 µm (No. 30) and larger sieves, and soft hair bristle for smaller sieves.

5. Determine the mass of the pan [minus 4.75 mm (No. 4)] (M_1).
6. Reduce the minus 4.75 mm (No. 4) using a mechanical splitter in accordance with the FOP for AASHTO T 248 to produce a sample with a mass of 500 g minimum. Determine and record the mass of the minus 4.75 mm (No. 4) split (M_2).
7. Select sieves to furnish information required by the specifications. Nest the sieves in order of decreasing size from top to bottom through the 75 µm (No. 200) with a pan at the bottom to retain the minus 75µm (No. 200).
8. Repeat steps 3 and 4, Method B, with the minus 4.75 mm (No. 4) including determining the mass of the material in the pan.

9a. Compute the "Adjusted Individual Mass Retained" of the size increment of the original sample as follows when determining "Individual Mass Retained".

$$A = \frac{M_1}{M_2} \times B$$

where:

A = Adjusted individual mass retained of the size increment on a total sample basis

M_1 = mass of minus 4.75mm (No. 4) sieve in total sample

M_2 = mass of minus 4.75mm (No. 4) sieve actually sieved

B = individual mass of the size increment in the reduced portion sieved.

9b. Compute the "Adjusted Cumulative Mass Retained" of the size increment of the original sample as follows when determining "Cumulative Mass Retained":

$$C = \left(\frac{M_1}{M_2} \times B\right) + D$$

where:

C = Total cumulative mass retained of the size increment based on a total sample

M_1 = mass of minus 4.75mm (No. 4) sieve in total sample

M_2 = mass of minus 4.75mm (No. 4) sieve actually sieved

B = cumulative mass of the size increment in the reduced portion sieved.

D = cumulative mass of plus 4.75mm (No. 4) portion of sample.

Method B Sample Calculation

Sample calculation for percent retained and percent passing each sieve in accordance with Method B when the previously washed 4.75mm (No. 4) minus material is split:

Example:

Dry mass of total sample, before washing: 3214.0 g

Dry mass of sample, after washing out the 75 µm (No. 200) minus: 3085.1 g

Amount of 75 µm (No. 200) minus washed out: 3214.0 g – 3085.1 g = 128.9 g

Gradation on Coarse Sieves

Sieve Size mm (in.)	Individual Mass Retained, g	Individual Percent Retained	Cumulative Mass Retained, g	Cumulative Percent Retained	Calculated Percent Passing
16.0 (5/8)	0	0	0	0	100
12.5 (1/2)	161.1	5.0	161.1	5.0	95.0
9.50 (3/8)	481.4	15.0	642.5	20.0	80.0
4.75 (No. 4)	475.8	14.8	1118.3	34.8	65.2
Pan	1966.7 **(M_1)**		3085.0		

Coarse check sum: [(3085.1 -3085.0) / 3085.1] X 100 = 0.00 % is within the 0.3 percent requirement.

Note 4: The pan mass determined in the laboratory (M_1) and the calculated mass (3085.1 – 1118.3 = 1966.8) should be the same if no material was lost.

The pan (1966.7 g) was reduced in accordance with the FOP for AASHTO T 248, so that at least 500 g are available. In this case, the mass determined was **512.8 g**. This is $\mathbf{M_2}$.

In order to account for the fact that only a portion of the minus 4.75mm (No. 4) material was sieved, the mass of material retained on the smaller sieves is adjusted by a factor equal to M_1/M_2. The factor determined from M_1/M_2 must be carried to three decimal places. Both the individual mass retained and cumulative mass retained formulas are shown.

Individual mass retained:

M_1 = mass of the minus 4.75mm (No. 4) before split.

M_2 = mass before sieving from the split of the minus 4.75 mm (No. 4).

$$\frac{M_1}{M_2} = \frac{1{,}966.7\text{ g}}{512.8\text{ g}} = 3.835$$

Each “individual mass retained” on the fine sieves must be multiplied by this adjustment factor.

For example, the overall mass retained on the 2.00mm (No. 10) sieve is:

3.835 x 207.1 g = 794.2 g as shown in the following table.

Final Gradation on All Sieves
Calculation by Individual Mass

Sieve Size mm (in.)	Individual Mass Retained g		Adjusted Individual Mass Retained g	Individual Percent Retained	Calc'd Percent Passing	Reported Percent Passing*
16.0 (5/8)	0		0	0.0	100.0	100
12.5 (1/2)	161.1		161.1	5.0	95.0	95
9.5 (3/8)	481.4		481.4	15.0	80.0	80
4.75 (No. 4)	475.8		475.8	14.8	65.2	65
2.0 (No. 10)	207.1	*x 3.835*	794.2	24.7	40.5	40
0.425 (No. 40)	187.9	*x 3.835*	720.6	22.4	18.1	18
0.210 (No. 80)	59.9	*x 3.835*	229.7	7.1	11.0	11
0.075 (No. 200)	49.1	*x 3.835*	188.3	5.9	5.1	5.1
Pan	7.8	*x 3.835*	29.9			
Dry mass of total sample, before washing: 3214.0 g						

*Report 75 µm (No. 200) sieve to 0.1 percent. Report all others to 1 percent

Fine check sum: [(512.8-511.8) / 512.8] X 100 = 0.2% is within the 0.3 percent requirement.

For Percent Passing (Calculated) see "Calculation" under Method A

Cumulative mass retained:

M_1 = mass of the minus 4.75 mm (No. 4) before split.

M_2 = mass before sieving of the split of the minus 4.75 mm (No. 4).

$$\frac{M_1}{M_2} = \frac{1{,}966.7 \text{ g}}{512.8 \text{ g}} = 3.835$$

Each "cumulative mass retained" on the fine sieves must be multiplied by this adjustment factor then the cumulative mass of plus 4.75 mm (No. 4) portion of sample is added to equal the adjusted cumulative mass retained .

For example, the adjusted cumulative mass retained on the 0.425 mm (No. 40) sieve is:

3.835 x 395.0 g = 1514.8 g

1514.8 + 1118.3 g = 2633.1"Total Cumulative Mass Retained" as shown in the following table

Final Gradation on All Sieves
Calculation by Cumulative Mass

Sieve Size mm (in.)	Cumulative Mass Retained g	Adjusted Cumulative Mass Retained g	Total Cum. Mass Retnd. g	Cum. Percent Retnd.	Calc'd Percent Passing	Reported Percent Passing*
16.0 (5/8)	0		0	0.0	100.0	100
12.5 (1/2)	161.1		161.1	5.0	95.0	95
9.5 (3/8)	642.5		642.5	20.0	80.0	80
4.75 (No. 4)	1118.3		**1118.3**	34.8	65.2	65
2.0 (No. 10)	207.1 *x 3.835*	794.2 *+ 1118.3*	1912.5	59.5	40.5	40
0.425 (No. 40)	395.0 *x 3.835*	1514.8 *+ 1118.3*	2633.1	81.9	18.1	18
0.210 (No. 80)	454.9 *x 3.835*	1744.5 *+ 1118.3*	2862.8	89.1	10.9	11
0.075 (No. 200)	504.0 *x 3.835*	1932.8 *+ 1118.3*	3051.1	94.9	5.1	5.1
Pan	511.8 *x 3.835*	1962.8 *+ 1118.3*	3081.1			

*Report 75 µm (No. 200) sieve to 0.1 percent. Report all others to 1 percent

Fine check sum: [(512.8-511.8) / 512.8] X 100 = 0.2% is within the 0.3 percent requirement.

For Percent Passing (Calculated) see "Calculation" under Method A

Procedure Method C

1. Dry sample in accordance with FOP for AASHTO T 255. Determine and record the total dry mass of the sample to the nearest 0.1 percent.

Note 5: AASHTO T 27 allows for coarse aggregate to be run in a moist condition unless the nominal maximum size of the aggregate is smaller than 12.5 mm (1/2 in.), the coarse aggregate (CA) contains appreciable material finer than 4.75 mm (No. 4), or the coarse aggregate is highly absorptive.

2. Break up any aggregations or lumps of clay, silt or adhering fines to pass the 4.75 mm (No. 4) sieve. If substantial coatings remain on the coarse particles in amounts that would affect the percent passing any of the specification sieves, the sample should be tested with either Method A or Method B.
3. Select sieves to furnish information required by the specifications. Nest the sieves in order of decreasing size from top to bottom through the 4.75 mm (No.4) with a pan at the bottom to retain the minus 4.75 mm (No. 4).
4. Place the sample, or a portion of the sample, on the top sieve. Sieves may already be in the mechanical shaker or place the sieves in the mechanical shaker and shake for the minimum time determined to provide complete separation for the sieve shaker being used, approximately 10 minutes.

Note 2: Excessive shaking (more than 10 minutes) may result in degradation of the sample.

5. Determine the individual or cumulative mass retained on each sieve to the nearest 0.1 percent or 0.1 g. Ensure that all material trapped in the openings of the sieve are cleaned out and included in the mass retained.

Note 3: Use coarse wire brushes to clean the 600 µm (No. 30) and larger sieves, and soft bristle brush for smaller sieves.

6. Determine the mass of the pan [minus 4.75 mm (No. 4)] (M_1).
7. Reduce the minus 4.75mm (No. 4) using a mechanical splitter in accordance with the FOP for AASHTO T 248 to produce a sample with a mass of 500 g minimum.
8. Determine and record the mass of the minus 4.75mm (No. 4) split (M_3).
9. Perform steps 3 thru 10 of Method A (Wash) on the minus 4.75mm (No. 4) split.
10. Select sieves to furnish information required by the specifications. Nest the sieves in order of decreasing size from top to bottom through the 75µm (No. 200) with a pan at the bottom to retain the minus 75 µm (No. 200).
11. Repeat steps 4 and 5, Method C, with the minus 4.75mm (No. 4) including determining the mass of the pan.

12a. Compute the "Adjusted Individual Mass Retained" of the size increment of the original sample as follows when determining "Individual Mass Retained":

where:

$$A = \frac{M_1}{M_3} \text{ x } B$$

A = Adjusted individual mass of the size increment on a total sample basis

M_1 = mass of the minus 4.75mm (No. 4) sieve in total sample

M_3 = mass of reduced portion of the minus 4.75mm (No. 4) before washing

B = mass of the size increment in the reduced portion sieved.

12b. Compute the "Adjusted Cumulative Mass Retained" of the size increment of the original sample as follows when determining "Cumulative Mass Retained":

$$C = \left(\frac{M_1}{M_3} \times B \right) + D$$

where:

C = Total cumulative mass of the size increment based on a total sample

M_1 = mass of fraction finer than 4.75mm (No. 4) sieve in total sample

M_3 = mass of reduced portion of material finer than 4.75mm (No. 4) before washing

B = cumulative mass of the size increment in the reduced portion sieved.

D = cumulative mass of plus 4.75mm (No. 4) portion of sample.

Method C Sample Calculation

Sample calculation for percent retained and percent passing each sieve in accordance with Method C when the 4.75mm (No. 4) minus material is split and then washed:

Dry Mass of total sample: 3304.5 g

Dry Mass of minus 4.75mm (No. 4) split before wash: 527.6

Dry Mass of minus 4.75mm (No. 4) split after wash: 495.3

Gradation on Coarse Sieves

Sieve Size mm (in.)	Individual Mass Retained, g	Individual Percent Retained	Cumulative Mass Retained, g	Cumulative Percent Retained	Cal'd Percent Passing
16.0 (5/8)	0	0	0	0	100.0
12.5 (1/2)	125.9	3.8	125.9	3.8	96.2
9.50 (3/8)	478.2	14.5	604.1	18.3	81.7
4.75 (No. 4)	691.5	20.9	1295.6	39.2	60.8
Pan	2008.9 **(M_1)**		3304.5		
Total Dry Mass = 3304.5					

Coarse check sum: [(3304.5 -3304.5) / 3304.5] X 100 = 0.0 % is within the 0.3 percent requirement

Note 4: The pan mass determined in the laboratory (M1) and the calculated mass (3304.5 – 1295.6 = 2008.9) should be the same if no material was lost.

The pan (2008.9 g) was reduced in accordance with the FOP for AASHTO T 248, so that at least 500 g are available. In this case, the mass determined was **527.6 g**. This is **M_3**.

In order to account for the fact that only a portion of the minus 4.75 mm (No. 4) material was washed and sieved, the mass of material retained on the smaller sieves is adjusted by a factor equal to M_1/M_3. The factor determined from M_1/M_3 must be carried to three decimal places. Both individual mass retained and cumulative mass retained formulas are shown.

<u>Individual mass retained:</u>

M_1 = mass of the minus 4.75mm (No. 4) before split.

M_3 = mass before washing of the split of the minus 4.75mm (No. 4).

$$\frac{M_1}{M_3} = \frac{2008.9\ g}{527.6\ g} = 3.808$$

Each "individual mass retained" on the fine sieves must be multiplied by this adjustment factor.

For example, the overall mass retained on the 2.00 mm (No. 10) sieve is:

3.808 x 194.3 = 739.9   as shown in the following table

Final Gradation on All Sieves
Calculation by Individual Mass

Sieve Size mm (in.)	Individual Mass Retained g	Adjusted Individual Mass Retained g	Individual Percent Retained	Calculated Percent Passing	Reported Percent Passing*
16.0 (5/8)	0	0	0.0	100.0	100
12.5 (1/2)	125.9	125.9	3.8	96.2	96
9.5 (3/8)	478.2	478.2	14.5	81.7	82
4.75 (No. 4)	691.5	691.5	20.9	60.8	61
2.0 (No. 10)	194.3 *x 3.808*	739.9	22.4	38.4	38
0.425 (No. 40)	171.3 *x 3.808*	652.3	19.7	18.7	19
0.210 (No. 80)	65.2 *x 3.808*	248.3	7.5	11.2	11
0.075 (No. 200)	53.6 *x 3.808*	204.1	6.2	5.0	5.0
Pan	10.7 *x 3.808*	40.7			
Dry mass of minus 4.75 mm (No. 4) sample, before washing: 527.6 g Dry mass of minus 4.75 mm (No. 4) sample, after washing: 495.3 g					

*Report 75 µm (No. 200) sieve to 0.1 percent. Report all others to 1 percent

Fine check sum: [(495.3 – 495.1) / 495.3] X 100 = 0.04% is within the 0.3 percent requirement.

For Percent Passing (Calculated) see Calculation under Method A

<u>Cumulative mass retained:</u>

M_1 = mass of the minus 4.75mm (No. 4) before split.

M_3 = mass before washing of the split of the minus 4.75mm (No. 4).

$$\frac{M_1}{M_3} = \frac{2008.9 \text{ g}}{527.6 \text{ g}} = 3.808$$

Each "cumulative mass retained" on the fine sieves must be multiplied by this adjustment factor then the cumulative mass of plus 4.75 mm (No. 4) portion of sample is added to equal the adjusted cumulative mass retained .

For example, the adjusted cumulative mass retained on the0.425.00 mm (No. 40) sieve is:

3.808 x 4365.6 g = 1392.2g

1392.2 + 1295.6 g = 2687.8 "Total Cumulative Mass Retained" as shown in the following table

Final Gradation on All Sieves
Calculation by Cumulative Mass

Sieve Size mm (in.)	Cumulative Mass Retained g	Adjusted Cumulative Mass Retained g	Total Cum. Mass Retnd. g	Cum. Percent Retnd.	Cal'd Percent Passing	Reported Percent Passing*
16.0 (5/8)	0		0	0.0	100.0	100.0
12.5 (1/2)	125.9		125.9	3.8	96.2	96
9.5 (3/8)	604.1		604.1	18.3	81.7	82
4.75 (No. 4)	1295.6		**1295.6**	39.2	60.8	61
2.0 (No. 10)	194.3 *x 3.808*	739.9 + *1295.6*	2035.5	61.6	38.4	38
0.425 (No. 40)	365.6 *x 3.808*	1392.2 + *1295.6*	2687.8	81.3	18.7	19
0.210 (No. 80)	430.8 *x 3.808*	1640.5 + *1295.6*	2936.1	88.9	11.1	11
0.075 (No. 200)	484.4 *x 3.808*	1844.6 + *1295.6*	3140.2	95.0		5.0
Pan	495.1 *x 3.808*	1885.3 + *1295.6*	3180.9			

Dry mass of minus 4.75 mm (No. 4) sample, before washing: 527.6 g
Dry mass of minus 4.75 mm (No. 4) sample, after washing: 495.3 g

*Report 75 µm (No. 200) sieve to 0.1 percent. Report all others to 1 percent

Fine check sum: [(495.3 – 495.1) / 495.3] X 100= 0.04% is within the 0.3 percent requirement.

For Percent Passing (Calculated) see "Calculation" under Method A

Fineness Modulus

Fineness Modulus (FM) is used in determining the degree of uniformity of the aggregate gradation in PCC mix designs. It is an empirical number relating to the fineness of the aggregate. The higher the FM, the coarser the aggregate. Values of 2.40 to 3.00 are common for FA in PCC.

The sum of the cumulative percentages retained on specified sieves 150 mm (6"), 75 mm (3"), 37.5 mm (11/2), 19.0 mm (3/4), 9.5 mm (3/8), 4.75 mm (No.4), 2.36 mm (No.8), 1.18 mm (No.16), 0.60 mm (No.30), 0.30 mm (No.50), and 0.15 mm (No.100) divided by 100 gives the FM.

Sample Calculation

	Example A				Example B		
	Percent				Percent		
		Retained				Retained	
Sieve Size mm (in)	Passing		On Spec'd Sieves*		Passing		On Spec'd Sieves*
75*(3)	100	0	0		100	0	0
63(21/2)	100	0	--		100	0	--
50(2)	100	0	--		100	0	--
37.5*(11/2)	100	0	0		100	0	0
25(1)	53	47	--		100	0	--
19*(3/4)	15	85	85		100	0	0
12.5(1/2)	0	100	--		100	0	--
9.5*(3/8)	0	100	100		100	0	0
6.3(1/4)	0	100	--		100	0	--
4.75*(No.4)	0	100	100		100	0	0
2.36*(No.8)	0	100	100		87	13	13
1.18*(No.16)	0	100	100		69	31	31
0.60*(No.30	0	100	100		44	56	56
0.30*(No.50)	0	100	100		18	82	82
0.15*(100)	0	100	100		4	96	96
			$\Sigma = 785$				$\Sigma = 278$
			FM = 7.85				FM = 2.78

In decreasing size order, each * sieve is one-half the size of the preceding * sieve.

Report

Results shall be reported on standard forms approved for use by the agency. Depending on the agency, this may include:

- Mass retained on each sieve
- Percent retained on each sieve
- Cumulative mass retained on each sieve
- Cumulative percent retained on each sieve
- Percent passing each sieve to the nearest 1 percent except for the percent passing the 75 µm (No. 200) sieve, which shall be reported to the nearest 0.1 percent
- FM to the nearest 0.01

Addendum WAQTC FOP for AASHTO T 27/T 11

Following are guidelines for the use of WAQTC FOP for AASHTO T 27/T 11 by the State of Alaska DOT&PF.

1. Delete Table 1and replace with Table 3:

Table 3
Sample sizes for Aggregate Sieve Analysis

Nominal Maximum Size*		Minimum Mass	
Standard mm	Alternate In	kg	lb
4.75	No. 4	0.5	1
6.3	1/4″	1	2
9.5	3/8″	1	2
12.5	1/2″	2	4
19.0	3/4″	5	11
25.0	1″	10	22
37.5	1-1/2″	15	33
50	2″	20	44
75	3″	30	66

*Nominal Maximum size: One sieve larger than the first sieve to retain more than 10 percent of the material using an agency specified set of sieves based on cumulative percent retained. Where large gaps between specification sieves exist, intermediate sieve(s) may be inserted to determine nominal maximum size.

2. AKDOT&PF does not allow the coarse aggregate to be run in a moist condition for sieve analysis.
3. Unless otherwise specified, Method C shall be used.

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DETERMINING THE PERCENTAGE OF FRACTURE IN COARSE AGGREGATE
FOP FOR AASHTO TP 61

Scope

This procedure covers the determination of the percentage, by mass, of a coarse aggregate (CA) sample that consists of fractured particles meeting specified requirements in accordance with AASHTO TP 61.

In this procedure, a sample of aggregate is screened on the sieve separating CA and fine aggregate (FA). This sieve will be identified in the agency's specifications, but might be the 4.75 mm (No. 4) sieve. CA particles are visually evaluated to determine conformance to the specified fracture. The percentage of conforming particles, by mass, is calculated for comparison to the specifications.

Apparatus

- Balance or scale: Capacity sufficient for the principle sample mass, accurate to 0.1 percent of the sample mass or readable to 0.1 g. Meets the requirements of AASHTO M 231
- Sieves, meeting requirements of AASHTO M 92.
- Splitter, meeting the requirements of FOP for AASHTO T 248.

Terminology

1. Fractured Face – An angular, rough, or broken surface of an aggregate particle created by crushing or by other means. A face is considered a "Fractured Face" whenever one-half or more of the projected area, when viewed normal to that face, is fractured with sharp and well defined edges. This excludes small nicks.
2. Fractured particle – A particle of aggregate having at least the minimum number of fractured faces specified. (This is usually one or two.)

Sampling and Sample Preparation

1. Sample and reduce the aggregate in accordance with the FOPs for AASHTO T 2 and T 248.
2. When the specifications list only a total fracture percentage, the sample shall be prepared in accordance with Method 1. When the specifications require that the fracture be counted and reported on each sieve, the sample shall be prepared in accordance with Method 2.
3. Method 1 - Combined Fracture Determination

   a. Dry the sample sufficiently to obtain a clean separation of FA and CA material in the sieving operation.

b. Sieve the sample in accordance with the FOP for AASHTO T 27/ T 11 over the 4.75 mm (No. 4) sieve, or the appropriate sieve listed in the agency's specifications for this material.

Note 1: Where necessary wash the sample over the sieve or sieves designated for the determination of fractured particles to remove any remaining fine material, and dry to a constant mass in accordance with the FOP for AASHTO T 255.

c. Reduce the sample using Method A, Mechanical Splitter, in accordance with the FOP for AASHTO T 248 to the appropriate test size. This test size should be slightly larger than shown in Table 1, to account for loss of fines through washing, if necessary.

Table 1
Sample Size
Method 1 (Combined Sieve Fracture)

Nominal Maximum Size* mm (in.)	Minimum Sample Mass Retained on 4.75 mm (No. 4) Sieve g (lb)
37.5 (1 1/2)	2500 (6)
25.0 (1)	1500 (3.5
19.0 (3/4)	1000 (2.5)
12.5 (1/2)	700 (1.5)
9.5 (3/8)	400 (0.9)
4.75 (No. 4)	200 (0.4)

***** One sieve larger than the first sieve to retain more than 10 percent of the material using an agency specified set of sieves based on cumulative percent retained. Where large gaps in specification sieves exist, intermediate sieve(s) may be inserted to determine nominal maximum size.

4. Method 2 – Individual Sieve Fracture Determination

a. Dry the sample sufficiently to obtain a clean separation of FA and CA material in the sieving operation. A washed sample from the gradation determination (the FOP for T 27/T 11) may be used.

b. If not, sieve the sample in accordance with the FOP for AASHTO T 27 over the sieves listed in the specifications for this material.

Note 2: If overload (buffer) sieves are used the material from that sieve must be added to the next specification sieve.

c. Select a representative portion from each sieve by splitting or quartering in accordance with the FOP for AASHTO T 248. The size of test sample for each sieve should be at least as large as shown in Table 2.

Note 1: Where necessary wash the sample over the sieve or sieves designated for the determination of fractured particles to remove any remaining fine material, and dry to a constant mass in accordance with the FOP for AASHTO T 255.

Table 2
Sample Size
Method 2 (Individual Sieve Fracture)

Sieve Size mm (in.)	Minimum Sample Mass g (lb)
31.5 (1 1/4)	1500 (3.5)
25.0 (1)	1000 (2.2)
19.0 (3/4)	700 (1.5)
16.0 (5/8)	500 (1.0)
12.5 (1/2)	300 (0.7)
9.5 (3/8)	200 (0.5)
6.3 (1/4)	100 (0.2)
4.75 (No. 4)	100 (0.2)
2.36 (No. 8)	25 (0.1)
2.00 (No. 10)	25 (0.1)

Note 3: If fracture is determined on a sample obtained for gradation, use the mass retained on the individual sieves, even if it is less than the minimum listed in Table 2. If less than 5 percent of the total mass is retained on a single specification sieve, include that material on the next smaller specification sieve. If a smaller specification sieve does not exist this material shall not be included in the fracture determination.

Procedure

1. After cooling, spread the dried sample on a clean, flat surface large enough to permit careful inspection of each particle. To verify that a particle meets the fracture criteria, hold the aggregate particle so that the face is viewed directly.
2. To aid in making the fracture determination separate the sample into three categories:
   - Fractured particles meeting the criteria
   - Particles not meeting the criteria
   - Questionable or borderline particles
3. Determine the dry mass of particles in each category to the nearest 0.1 g.

   Note 4: If, on any determination, more than 15 percent of the total mass of the sample is placed in the questionable category, repeat the sorting procedure until no more than 15 percent is present in that category.

Calculation

Calculate the mass percentage of fractured faces to the nearest 1 percent using the following formula:

$$P = \frac{\left(\frac{Q}{2}+F\right)}{(F+Q+N)}\times 100$$

where: P = Percent of fracture
F = Mass of fractured particles
Q = Mass of questionable or borderline particles.
N = Mass of unfractured particles

Example:

F = 632.6 g, Q = 97.6 g, N = 352.6 g

P =

$$\frac{\left(\frac{97.6}{2}+632.6\right)}{(632.6+97.6+352.6)}\times 100 = 62.9$$

P= 63%

Report

Results shall be reported on standard forms approved for use by the agency. Report fracture to the nearest 1 percent.

Determining the Percentage of Flat and Elongated Particles in Coarse Aggregate ATM 306

1. Scope

This procedure covers the determination of the percentages of flat (thin) and elongated particles in coarse aggregates.

2. Apparatus

The apparatus used shall consist of any suitable equipment, by means of which aggregate particles may be tested for compliance, at the dimensional ratios desired, with the definitions given below. Types of acceptable apparatus are:

- ASTM Proportional Caliper Device meeting the requirements of ASTM D 4791. Illustrated in Figure 1.
- Balance or scale: Capacity sufficient for the principle sample mass, readable 0.1 percent or 0.1 g and meeting the requirements of AASHTO M 231.

Note: For this test, this would require a scale with a capacity of at least 1200 g and readable to 0.1 g, or better.

- Sieves, meeting the requirements of AASHTO M 92.

3. Definitions

1. Length — maximum dimension of the particle.
2. Thickness — maximum dimension perpindicular to the length and width.
3. Flat ("Thin") & Elongated Particle — a particle having a ratio of length to thickness greater than that specified.

4. Sampling and Sample Preparation

1. Sample the aggregate in accordance with the WAQTC FOP for AASHTO T 2.
2. Dry the sample to constant mass in accordance with WAQTC FOP for AASHTO T 255/T 265. Separate the sample in accordance with WAQTC FOP for AASHTO T 27/T 11 or use the gradation sample from that procedure or WAQTC FOP for AASHTO T 30, separating the coarse aggregate into the size fractions shown in Table 1.
3. Reduce the sample in accordance with WAQTC FOP for AASHTO T 248 Method A, to the appropriate test size as shown in Table 1 or use the material from WAQTC FOPs for AASHTO T 27/T 11 or AASHTO T 30. The test sample size should be slightly larger than shown in Table 1, to account for loss of fines through washing, if necessary. If the test is performed on a sample obtained for gradation, use the mass retained on the individual sieves, even if it is below the minimums listed in Table 1.

Table 1

Sample Size

Size Fraction		Minimum Sample Mass
(mm)	(in)	g
37.5 to 19.0	1½ to ¾	1000
19.0 to 9.5	¾ to ⅜	500
9.5 to 4.75	⅜ to No. 4	100

Note 1: If this test is performed using a sample obtained for gradation, use the mass retained for the size fraction, regardless of the sample mass required by Table 1. If less than 5 percent of the total mass is retained on a single specification sieve, include that material on the next smaller specification sieve.

5. Procedure

1. Unless specified, the caliper ratio shall be 1:5.
2. Determine and record the total dry mass of the size grouping to be tested to the nearest 0.1g.
3. Flat and Elongated Particle Test — Recombine, if necessary, all of the particles from the above process.
    a. Set the larger opening to the particle's length. The particle is flat and elongated if the particle's thickness can pass completely through the smaller opening.
    b. Determine and record the mass of the flat and elongated particles to the nearest 0.1 g.

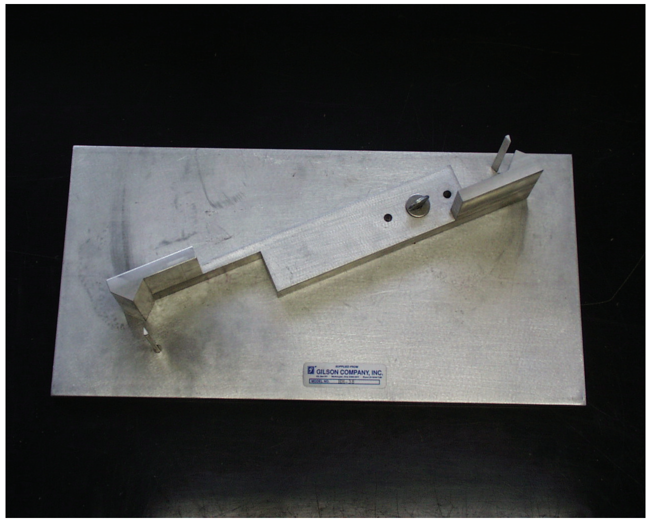
6. Calculation

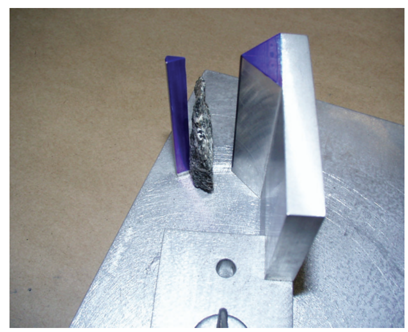
3. Calculate the cumulative percent retained of each size group in relation to the plus 4.75 mm (No. 4) by dividing the percent retained of the smallest sieve size of each size group by the percent retained from the original gradation of the plus 4.75 mm (No. 4).
4. Calculate the individual percent retained of each size group by subtracting the cumulative percent retained in Step 1 of each size group from the cumulative percent retained of the next larger size group.
5. Calculate the percent each fraction type for each test specimen by dividing the mass of that fraction by the total sample mass.
6. Calculate the weighted percent for each fraction type each size group by multiplying the percent flat-elongated of that size group by the individual percent retained of that size group.
7. Calculate the total percentage of flat-elongated particles of the as-received gradation by adding together the weighted percent flat-elongated of each size group and multiplying this total by 100.

7. Report

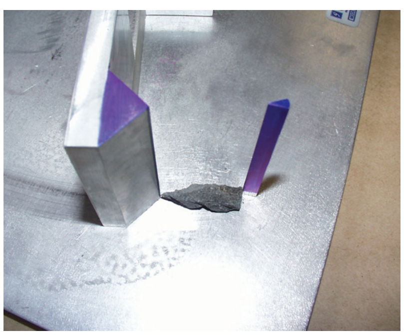
Report the required data on Department forms to the nearest whole percent.

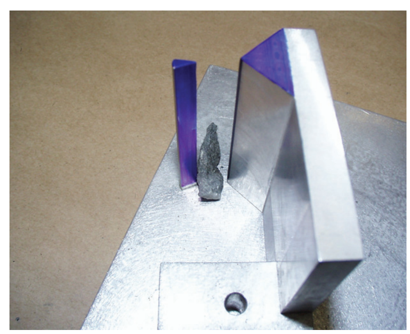
ASTM Proportional Caliper
Figure 1



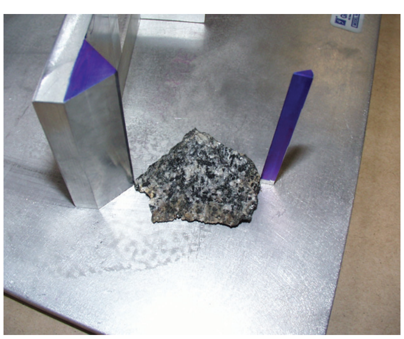


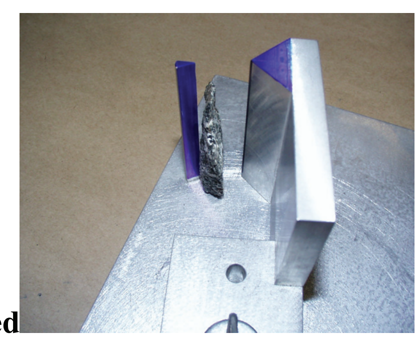
Flat





Elongated





Flat & Elongated

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PLASTIC FINES IN GRADED AGGREGATES AND SOILS BY THE USE OF THE SAND EQUIVALENT TEST
WAQTC FOP FOR AASHTO T 176

Scope

This procedure covers the determination of plastic fines in accordance with AASHTO T 176. It serves as a rapid test to show the relative proportion of fine dust or clay-like materials in fine aggregates (FA) and soils.

Apparatus

See AASHTO T 176 for a detailed listing of sand equivalent apparatus. Note that the siphon tube and blow tube may be glass or stainless steel as well as copper.

- Graduated plastic cylinder.
- Rubber stopper.
- Irrigator tube.
- Weighted foot assembly: There are two models of the weighted foot assembly. The older model has a guide cap that fits over the upper end of the graduated cylinder and centers the rod in the cylinder. It is read using a slot in the centering screws. The newer model has a sand reading indicator 254 mm (10 in.) above this point and is preferred for testing clay-like materials.
- Siphon assembly: The siphon assembly will be fitted to a 4-L (1 gal) bottle of working calcium chloride solution placed on a shelf 915 ±25 mm (36 ±1 in.) above the work surface.
- Weighted foot assembly having a mass of 1000 ± 5 g.
- Measuring can having a capacity of 85 ±5 ml (3 oz.).
- Funnel with a wide-mouth for transferring sample into graduated cylinder.
- Quartering cloth – 600 mm (2 ft) square nonabsorbent cloth, such as plastic or oil cloth.
- Mechanical splitter – see FOP for AASHTO T 248.
- Strike off bar – A straight edge or spatula.
- Clock or watch reading in minutes and seconds.
- Manually operated sand equivalent shaker capable of producing an oscillating motion at a rate of 100 complete cycles in 45 ±5 seconds, with a hand assisted half stroke length of 127 ±5 mm (5 ±2 in.). It may be held stable by hand during the shaking operation. It is recommended that this shaker be fastened securely to a firm and level mount, by bolts or clamps, if a large number of determinations are to be made.
- Mechanical shaker – See AASHTO T 176 for equipment and procedure.
- Oven capable of maintaining a temperature of 110 ±5°C (230 ±9°F).
- Thermometer – Calibrated liquid-in-glass or electronic digital type designed for total immersion and accurate to 0.1°C (0.2°F).

Materials

- Stock calcium chloride solution: Obtain commercially prepared calcium chloride stock solution meeting AASHTO requirements.
- Working calcium chloride solution: Dilute one 3 oz measuring can (85 ±5 mL) of stock calcium chloride solution to 3.8 L (1 gal) with distilled or demineralized water. (The graduated cylinder filled to 111.8 mm [4.4 in.] contains 88 mL.)

> ***Note 1:*** *Mix the working solution thoroughly. Add 85ml (3oz) of stock solution to a clean, empty 3.8L (1qt) jug, add approximately one 1L (1qt) and agitate vigorously for 2 or 3 minutes. Add the remainder of the water in approximately 1L (1qt) increments repeating the agitation process.*
>
> ***Note 2:*** *Tap water may be used if it is proven not to be detrimental to the test and if it is allowed by the agency.*
>
> ***Note 3:*** *The shelf life of the working solution is approximately 30 days. Working solutions more than 30 days old shall be discarded.*

Control

The temperature of the working solution should be maintained at 22 ±3°C (72 ±5°F) during the performance of the test. If field conditions preclude the maintenance of the temperature range, reference samples should be submitted to the Central/Regional Laboratory, as required by the agency, where proper temperature control is possible. Samples that meet the minimum sand equivalent requirement at a working solution temperature outside of the temperature range need not be subject to reference testing.

Sample Preparation

1. Obtain the sample in accordance with FOP for AASHTO T 2 and reduce in accordance with FOP for AASHTO T 248.

2. Prepare sand equivalent test samples from the material passing the 4.75 mm (No. 4) sieve. If the material is in clods, break it up and rescreen it over a 4.75 mm (No. 4) sieve. All fines shall be cleaned from particles retained on the 4.75 mm (No. 4) sieve and included with the material passing that sieve.

3. Split or quarter 1000 to 1500 g of material from the portion passing the 4.75 mm (No. 4) sieve. Use extreme care to obtain a truly representative portion of the original sample.

> ***Note 4:*** *Experiments show that, as the amount of material being reduced by splitting or quartering is decreased, the accuracy of providing representative portions is reduced. It is imperative that the sample be split or quartered carefully. When it appears necessary, dampen the material before splitting or quartering to avoid segregation or loss of fines.*
>
> ***Note 5****:* All tests including Reference Tests will be performed utilizing Alternative Method No. 2 as described in AASHTO T 176 unless specifications call for oven dry samples.

4. The sample must have the proper moisture content to achieve reliable results. This condition is determined by tightly squeezing a small portion of the thoroughly mixed sample in the palm of the

hand. If the cast that is formed permits careful handling without breaking, the correct moisture content has been obtained. If the material is too dry, the cast will crumble and it will be necessary to add water and remix and retest until the material forms a cast.

Note 6: Clean sands having little 75 µm(No.200) such as sand for Portland Cement Concrete (PCC) may not form a cast.

If the material shows any free water, it is too wet to test and must be drained and air dried, and mixed frequently to ensure uniformity. This drying process should continue until squeezing provides the required cast.

If the moisture content is altered to provide the required cast, the altered sample should be placed in a pan, covered with a lid or with a damp cloth that does not touch the material, and allowed to stand for a minimum of 15 minutes. Samples that have been sieved without being air dried and still retain enough natural moisture are exempted from this requirement.

5. Place the sample on the quartering cloth and mix by alternately lifting each corner of the cloth and pulling it over the sample toward the diagonally opposite corner, being careful to keep the top of the cloth parallel to the bottom, thus causing the material to be rolled. When the material appears homogeneous, finish the mixing with the sample in a pile near the center of the cloth.

6. Fill the measuring can by pushing it through the base of the pile while exerting pressure with the hand against the pile on the side opposite the measuring can. As the can is moved through the pile, hold enough pressure with the hand to cause the material to fill the tin to overflowing. Press firmly with the palm of the hand, compacting the material and placing the maximum amount in the can. Strike off the can level full with the straight edge or spatula.
7. When required, repeat steps (5) and (6) to obtain additional samples.

Procedure

1. Start the siphon by forcing air into the top of the solution bottle through the tube while the pinch clamp is open.
2. Siphon 101.6 ±2.5 mm (4 ±0.1 in.) of working calcium chloride solution into the plastic cylinder. Pour the prepared test sample from the measuring can into the plastic cylinder using the funnel to avoid spilling. Tap the bottom of the cylinder sharply on the heel of the hand several times to release air bubbles and to promote thorough wetting of the sample.
3. Allow the wetted sample to stand undisturbed for 10 ±1 minutes. At the end of the 10-minute period, stopper the cylinder and loosen the material from the bottom by simultaneously partially inverting and shaking the cylinder.

4. After loosening the material from the bottom of the cylinder, shake the cylinder and contents by any one of the following methods:
    a. Mechanical Method – Place the stoppered cylinder in the mechanical shaker, set the timer, and allow the machine to shake the cylinder and contents for 45 ±1 seconds.

Note 7: The next two methods – manually-operated shaker method and hand method – require that the operator meet certain qualifications. See AASHTO T 176 for a full description.

    b. Manually-operated Shaker Method – Secure the stoppered cylinder in the three spring clamps on the carriage of the manually-operated sand equivalent shaker and set the stroke counter to zero. Stand directly in front of the shaker and force the pointer to the stroke limit marker painted on the backboard by applying an abrupt horizontal thrust to the upper portion of the right hand spring strap.

Remove the hand from the strap and allow the spring action of the straps to move the carriage and cylinder in the opposite direction without assistance or hindrance. Apply enough force to the right hand spring steel strap during the thrust portion of each stroke to move the pointer to the stroke limit marker by pushing against the strap with the ends of the fingers to maintain a smooth oscillating motion. The center of the stroke limit marker is positioned to provide the proper stroke length and its width provides the maximum allowable limits of variation.

Proper shaking action is accomplished when the tip of the pointer reverses direction within the marker limits. Proper shaking action can best be maintained by using only the forearm and wrist action to propel the shaker. Continue shaking for 100 strokes.

c. Hand Method – Hold the cylinder in a horizontal position and shake it vigorously in a horizontal linear motion from end to end. Shake the cylinder 90 cycles in approximately 30 seconds using a throw of 229 mm ±25 mm (9 ±1 in.). A cycle is defined as a complete back and forth motion. To properly shake the cylinder at this speed, it will be necessary for the operator to shake with the forearms only, relaxing the body and shoulders.

5. Set the cylinder upright on the work table and remove the stopper.

6. Insert the irrigator tube in the cylinder and rinse material from the cylinder walls as the irrigator is lowered. Force the irrigator through the material to the bottom of the cylinder by applying a gentle stabbing and twisting action while the working solution flows from the irrigator tip. Work the irrigator tube to the bottom of the cylinder as quickly as possible, since it becomes more difficult to do this as the washing proceeds. This flushes the fine material into suspension above the coarser sand particles.

   Continue to apply a stabbing and twisting action while flushing the fines upward until the cylinder is filled to the 381 mm (15 in.) mark. Then raise the irrigator slowly without shutting off the flow so that the liquid level is maintained at about 381 mm (15 in.) while the irrigator is being withdrawn. Regulate the flow just before the irrigator is entirely withdrawn and adjust the final level to 381 mm (15 in.).

   Note 8: *Occasionally the holes in the tip of the irrigator tube may become clogged by a particle of sand. If the obstruction cannot be freed by any other method, use a pin or other sharp object to force it out, using extreme care not to enlarge the size of the opening. Also, keep the tip sharp as an aid to penetrating the sample.*

7. Allow the cylinder and contents to stand undisturbed for 20 minutes ±15 seconds. Start timing immediately after withdrawing the irrigator tube.

   Note 9: *Any vibration or movement of the cylinder during this time will interfere with the normal settling rate of the suspended clay and will cause an erroneous result.*

8. Clay and Sand Readings

   a. At the end of the 20-minute sedimentation period, read and record the level of the top of the clay suspension. This is referred to as the clay reading.

   Note 10: *If no clear line of demarcation has formed at the end of the 20-minute sedimentation period, allow the sample to stand undisturbed until a clay reading can be obtained, then immediately read and record the level of the top of the clay suspension and the total sedimentation time. If the total sedimentation time exceeds 30 minutes, rerun the test using three individual samples of the same material. Read and record the clay column height of the sample* *requiring the shortest sedimentation period only. Once a sedimentation time has been established, subsequent tests will be run using that time. The time will be recorded along with the test results on all reports.*

b. After the clay reading has been taken, place the weighted foot assembly over the cylinder and gently lower the assembly until it comes to rest on the sand. Do not allow the indicator to hit the mouth of the cylinder as the assembly is being lowered. Subtract 254 mm (10 in.) from the level indicated by the extreme top edge of the indicator and record this value as the sand reading.

c. If clay or sand readings fall between 2.5 mm (0.1 in.) graduations, record the level of the higher graduation as the reading. For example, a clay reading of 7.95 would be recorded as 8.0, a sand reading of 3.22 would be recorded as 3.3.

d. If two Sand Equivalent (SE) samples are run on the same material and the second varies by more than ±4 points, based on the first cylinder reading, additional tests shall be run.

e. If three or more Sand Equivalent (SE) samples are run on the same material, average the readings. If an individual reading varies by more than ±4 points, based on the average cylinder reading, additional tests shall be run.

Calculations

1. Calculate the SE to the nearest 0.1 using the following formula:

$$SE = \frac{\text{Sand Reading}}{\text{Clay Reading}} \times 100$$

For Example: Sand Reading = 3.3 and Clay Reading = 8.0

$$SE = \frac{3.3}{8.0} \times 100 = 41.25 \text{ or } 41.3$$

Note 11: *This example reflects the use of equipment made with English units. At this time, equipment made with metric units is not available.*

2. Report the SE as the next higher whole number. In the example above, the 41.3 would be reported as 42. An SE of 41.0 would be reported as 41.

3. In determining the average of the two samples, raise each calculated SE value to the next higher whole number before averaging. For example, calculated values of 41.3 and 42.8 would be reported as 42 and 43, respectively.

   Then average the two values:

   $$\frac{42+43}{2}=42.5$$

   If the average value is not a whole number, raise it to the next higher whole number – in this case: 43.

Report

Results shall be reported on standard forms approved for use by the agency.

Report results to the whole number.

SPECIFIC GRAVITY AND ABSORPTION OF COARSE AGGREGATE
WAQTC FOP FOR AASHTO T 85

Scope

This procedure covers the determination of specific gravity and absorption of coarse aggregate in accordance with AASHTO T 85. Specific gravity may be expressed as bulk specific gravity (G_{sb}), bulk specific gravity, saturated surface dry (G_{sb} SSD), or apparent specific gravity (G_{sa}). G_{sb} and absorption are based on aggregate after 15 hours soaking in water. This procedure is not intended to be used with lightweight aggregates.

Terminology

Absorption – the increase in the mass of aggregate due to water being absorbed into the pores of the material, but not including water adhering to the outside surface of the particles, expressed as a percentage of the dry mass. The aggregate is considered "dry" when it has been maintained at a temperature of 110 ±5°C (230 ±9°F) for sufficient time to remove all uncombined water.

Saturated Surface Dry (SSD**)** – condition of an aggregate particle when the permeable voids are filled with water, but no water is present on exposed surfaces.

Specific Gravity – the ratio of the mass, in air, of a volume of a material to the mass of the same volume of gas-free distilled water at a stated temperature.

Apparent Specific Gravity (G_{sa})– the ratio of the mass, in air, of a volume of the impermeable portion of aggregate to the mass of an equal volume of gas-free distilled water at a stated temperature.

Bulk Specific Gravity (G_{sb})– the ratio of the mass, in air, of a volume of aggregate (including the permeable and impermeable voids in the particles, but not including the voids between particles) to the mass of an equal volume of gas-free distilled water at a stated temperature.

Bulk Specific Gravity (SSD) (G_{sb} SSD)– the ratio of the mass, in air, of a volume of aggregate, including the mass of water within the voids filled to the extent achieved by submerging in water for approximately 15 hours (but not including the voids between particles), to the mass of an equal volume of gas-free distilled water at a stated temperature.

Apparatus

- Balance or scale with a capacity of 5 kg, sensitive to 1 g. Meeting the requirements of AASHTO M 231.
- Sample container, wire basket of 3.35 mm (No. 6) or smaller mesh, with a capacity of 4 to 7 L (1 to 2 gal) to contain aggregate with a nominal maximum size of 37.5 mm (1 1/2 in.) or smaller; larger basket for larger aggregates.
- Water tank, watertight and large enough to completely immerse aggregate and basket, equipped with an overflow valve to keep water level constant.
- Suspension apparatus: wire used to suspend apparatus shall be of smallest practical diameter.
- Sieves 4.75 mm (No. 4), or other sizes as needed, conforming to AASHTO M 92.

Sample Preparation

1. Obtain the sample in accordance with the FOP for AASHTO T 2 (see Note 1).
2. Mix the sample thoroughly and reduce it in accordance with the FOP for AASHTO T 248.
3. Reject all material passing the appropriate sieve by dry sieving and thoroughly washing to remove dust or other coatings from the surface. The minimum mass is given in Table

   Note 1: If this procedure is used only to determine the Bulk G_{sb} of oversized material for the FOP for AASHTO T 99 / T 180 and in the calculations for the FOP for AASHTO T 224. The material can be rejected over the appropriate sieve; T 99 / T 180 methods A & B 4.75 mm (No.4), T 99 / T 180 methods C & D the 19 mm (3/4 in).

Table 1

Nominal Maximum Size mm (in.)	Minimum Mass of Test Sample, g (lb)
12.5 (1/2) or less	2000 (4.4)
19.0 (3/4)	3000 (6.6)
25.0 (1)	4000 (8.8)
37.5 (1 1/2)	5000 (11)
50 (2)	8000 (18)
63 (2 1/2)	12,000 (26)
75 (3)	18,000 (40)

* One sieve larger than the first sieve to retain more than 10 percent of the material using an agency specified set of sieves based on cumulative percent retained. Where large gaps in specification sieves exist, intermediate sieve(s) may be inserted to determine nominal maximum size.

Procedure

1. Dry the test sample to constant mass at a temperature of 110 ±5°C (230 ±9°F) and cool in air at room temperature for 1 to 3 hours.

   Note 2: Where the absorption and specific gravity values are to be used in proportioning concrete mixtures in which the aggregates will be in their naturally moist condition, the requirement for initial drying to constant mass may be eliminated, and, if the surfaces of the particles in the sample have been kept continuously wet until test, the 15-hour soaking may also be eliminated.

2. Immerse the aggregate in water at room temperature for a period of 15 to 19 hours.

   Note 3: When testing coarse aggregate of large nominal maximum size requiring large test samples, it may be more convenient to perform the test on two or more subsamples, and then combine values obtained.

3. Place the empty basket into the water bath and attach to the balance. Inspect the immersion tank to insure the water level is at the overflow outlet height. Tare the balance with the empty basket attached in the water bath.
4. Remove the test sample from the water and roll it in a large absorbent cloth until all visible films of water are removed. Wipe the larger particles individually.

   Note 4: A moving stream of air may be used to assist in the drying operation, but take care to avoid evaporation of water from aggregate pores.

5. Determine the SSD mass of the sample, and record this and all subsequent masses to the nearest 0.1 g or 0.1 percent of the sample mass, whichever is greater. Designate this mass as “B”.

6. Re-inspect the immersion tank to insure the water level is at the overflow outlet height. Immediately place the SSD test sample in the sample container and weigh it in water maintained at 23.0 ±1.7°C (73.4 ±3°F). Shake the container to release entrapped air before recording the weight. Designate this submerged weight as "C".

   Note 5: The container should be immersed to a depth sufficient to cover it and the test sample during mass determination. Wire suspending the container should be of the smallest practical size to minimize any possible effects of a variable immersed length.

7. Remove the sample from the basket. Ensure all material has been removed. Place in a container of known mass.
8. Dry the test sample to constant mass in accordance with the FOP for AASHTO T 255 / T 265 (Aggregate) and cool in air at room temperature for 1 to 3 hours. Designate this mass as "A".

Calculations

Perform calculations and determine values using the appropriate formula below. In these formulas, A = oven dry mass, B = SSD mass, and C = weight in water.

Bulk specific gravity (G_{sb})

$$G_{sb} = A / (B-C)$$

Bulk specific gravity, SSD (G_{sb} SSD)

$$G_{sb}\ SSD = B / (B - C)$$

Apparent specific gravity (G_{sa})

$$G_{sa} = A / (A - C)$$

Absorption

$$\text{Absorption} = [(B - A) / A] \times 100$$

Sample Calculations

Sample	A	B	C	B - C	A - C	B - A
1	2030.9	2044.9	1304.3	740.6	726.6	14.0
2	1820.0	1832.5	1168.1	664.4	651.9	12.5
3	2035.2	2049.4	1303.9	745.5	731.3	14.2

Sample	G_{sb}	G_{sb} SSD	G_{sa}	Absorption	Reported
1	2.742	2.761	2.795	0.689	0.7
2	2.739	2.758	2.792	0.687	0.7
3	2.730	2.749	2.783	0.698	0.7
Average	2.737	2.756	2.790	0.691	0.7

These calculations demonstrate the relationship between G_{sb}, G_{sb} SSD, and G_{sa}. G_{sb} is always lowest, since the volume includes voids permeable to water. G_{sb} SSD is always intermediate. G_{sa} is always highest, since the volume does not include voids permeable to water. When running this test, check to make sure the values calculated make sense in relation to one another.

Report

Results shall be reported on standard forms approved by the agency. Report specific gravity values to 3 decimal places and absorption to 0.1 percent.

Nordic Abrasion Value of Coarse Aggregate ATM 312

1. Scope

This method describes the test procedure for the simulation of the abrasive action of traffic on coarse aggregates used in a surface layer to determine the ability of the aggregate to resist wear by abrasion from studded tires.

The test shall be performed on aggregates with a size fraction of 11.2 to 16.0 mm (7/16" to 5/8")

Note 1: Variations from this size range will not give consistent results.

The test is applicable to crushed and uncrushed natural and artificial aggregates.

This test method involves potentially hazardous materials, operations and equipment. This method does not purport to address all of the safety problems associated with it use.

2. Principle

A sample of a single-sized aggregate group, 11.2 to 16.0 mm (7/16" to 5/8"), is rotated together with steel balls and water in a steel drum. Three ribs, which are mounted on the interior of the drum, add to the abrading action of the aggregate particles and the steel balls. The contents roll within the drum with an abrading action. After the specified number of revolutions, the contents are removed from the drum and the aggregate portion is sieved on a 2.00 mm (No. 10) sieve to measure the wear as a percentage loss.

3. Apparatus

- Testing machine conforming to the design shown in Figure 1.
- The cylinder shall have an inside diameter of 206.5 ± 2 mm and an inside length of 335 ± 1 mm. Three ribs, each with a length of 333 ± 1 mm, shall be equally spaced around the internal circumference of the cylinder. The test drum shall be water-tight and made of a seamless steel tube conforming to according to grade *TS 5 of ISO 2604-2*, of outside diameter 219.1 and wall thickness of 6.3 mm. The cylinder shall rotate centrically with the axis in a horizontal position at a rate of 90 ± 3 rpm. A revolution counter shall automatically stop the rotation after 5400 revolutions.
- The three ribs shall be removable and made from spring steel as specified in *ISO 683-14* and designed in accordance with figure 1. The ribs, prior to their use in the test, shall be preground in the drum for 25 h using a hard aggregate, together with the normal proportions of steel balls and water.
- During the test the ribs will wear and their action will change. Each rib shall be replaced, when its loss in original mass exceeds 15 g.
- Ball bearings, 14.99-15.05 mm diameter, of a hardness between 62 and 65 HRC, as specified in *ISO*

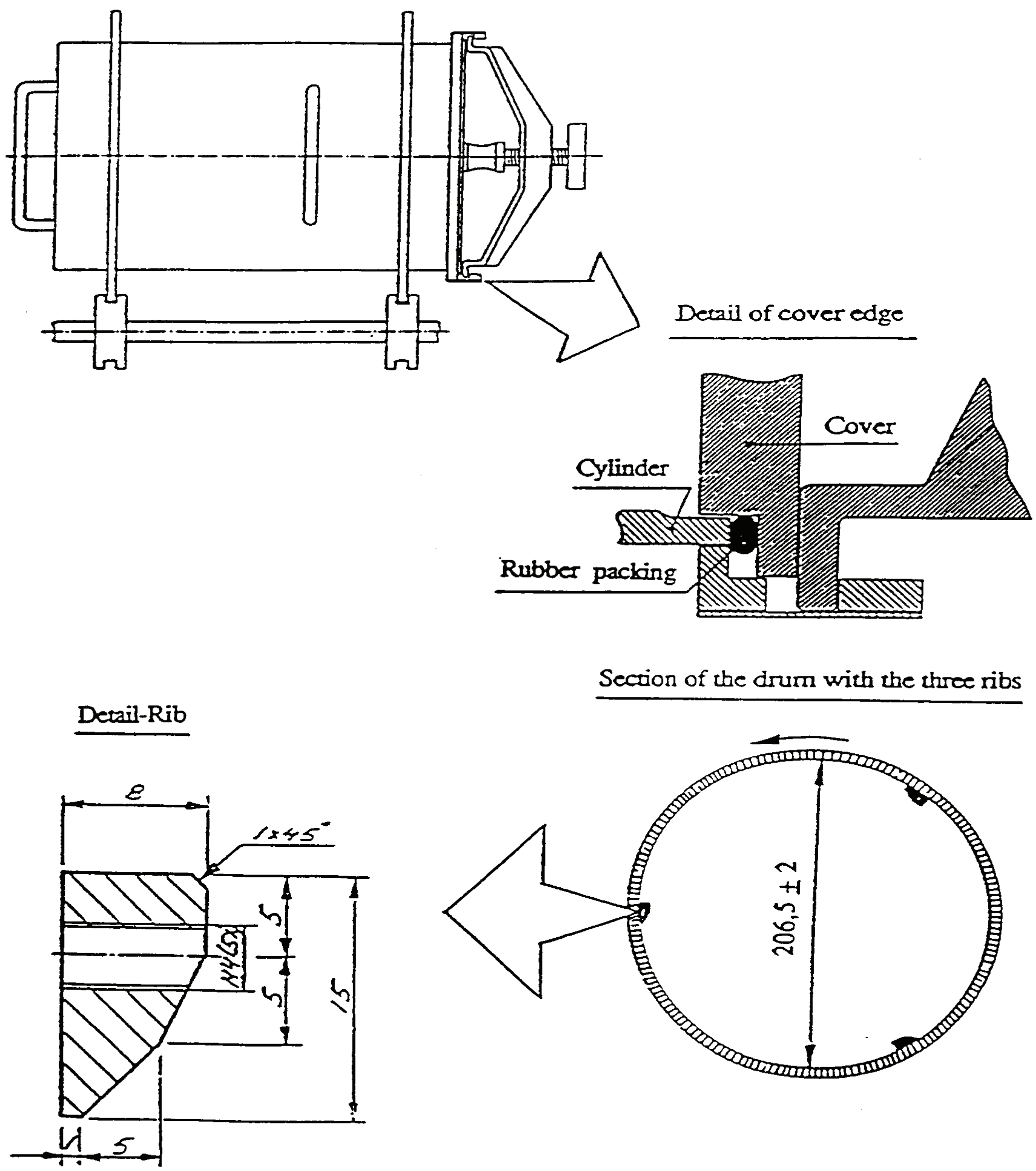

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Figure 1

- Gauge to control minimum ball size, e.g. two parallel bars 14.5 mm apart.
- Magnet (optional) for removal of the charge from the aggregate test sample after abrasion.

Note 3: Do not use too strong a magnet as the balls may become magnetized.

- Oven capable of maintaining a uniform temperature of 110 ± 5 °C (230 ± 9°F).
- Balance or scale: Capacity sufficient for the principle sample mass, readable to 0.1 percent or 0.1 g, of the total sample mass and meeting the requirements of AASHTO M 231.
- Sieves of the following sizes: 2.00 mm, 11.2 mm, and 16.0 mm (No. 10, 7/16" and 5/8").
- Bucket.
- Washing device.

4. Sampling

Obtain the sample in accordance with WAQTC FOP for AASHTO T 2.

5. Preparation Of Test Sample

Unprocessed Aggregate

1. Separate the sample on the 19 mm (3/4") sieve by hand or mechanical shaker, sieving the material for 5 minutes. Discard the minus 19 mm (3/4") material unless required for other testing.
2. Crush the plus 19 mm (3/4") aggregate, or a representative portion obtained in accordance with WAQTC FOP for AASHTO T 248, to pass the 19 mm (3/4") sieve. 3. Separate the material into the required test size, using 16 mm (5/8") sieve and 11.2 mm (7/16") sieves, in accordance with WAQTC FOP for AASHTO T 27/T 11. Discard all particles retained on the 16 mm (5/8") sieve and all the particles passing the 11.2 mm (7/16") sieve, unless required for other testing.
4. Proceed to Step 2 below.

Processed (already crushed) Aggregate

1. Separate the material into the required test size, using 16 mm (5/8") and 11.2 mm (7/16") sieves, in accordance with WAQTC FOP for AASHTO T 27/T 11. Discard all particles retained on the 5/8" (16 mm) sieve and all the particles passing the 11.2 mm (7/16") sieve, unless required for other testing.
2. Sample must have no more than 8 percent Flat and Elongated when tested in accordance with ATM 306 using a caliper ratio of 1:5.
3. Reduce the sample to test size (minimum of 3500 g) in accordance with WAQTC FOP for AASHTO T 248.
4. Wash the sample and dry to a constant mass in accordance with WAQTC FOP for AASHTO T 255/T 265.
5. Determine the apparent specific gravity of the sample, or a portion thereof, in accordance with WAQTC FOP for AASHTO T 85.
6. Determine the test sample mass by:

$$m_i = \frac{P_i}{2.66} \times 1000$$

Where m_i = mass of the test sample

p_i = apparent specific gravity of test sample.

7. Batch 3 test specimens at the calculated weight ± 5 g.

6. Procedure

1. Place the ball charge (7000 ± 10 g) and the test sample in the drum and add (2000 ± 10) ml. of water.
2. Rotate the drum at a speed of 90 ± 3 rpm for 5400 ± 10 revolutions.
3. After the specified number of revolutions, discharge the contents (sample and ball charge) from the drum into a bucket.
4. Wash the sample including the ball charge on a 2.00 mm (No. 10) sieve. Remove the steel balls from the sample with a magnet.

   Note 4: To avoid overloading the sieve, it may be necessary to divide the sample into smaller portions.

5. Dry the aggregate fraction retained on the 2.00 mm (No. 10) sieve, to a constant mass in accordance with WAQTC FOP for AASHTO T 255 and weigh to the nearest 0.1 g.

7. Calculation and Expression of Results

1. Calculate the individual Nordic Abrasion Values (A_N) to the nearest 0.1 percent as follows:

$$A_N = \left(\frac{m_i - m_2}{m_i}\right) x\, 100$$

Where m_i = Initial dry mass of the test sample.

m_2 = Dry mass of the aggregate after the test.

2. Compute and record the average of the individual Nordic Abrasion Values to the nearest 0.1 percent.

8. Report

The individual and average Nordic Abrasion values shall be reported on Department forms to the nearest 0.1 percent.

Degradation Value of Aggregates ATM 313

1. Scope

This test method describes the procedure for determining the durability of an aggregate. The durability of an aggregate as measured by the Degradation Value indicates the relative resistance of an aggregate to produce detrimental clay-like fines when subjected to a prescribed abrasion process in the presence of distilled or demineralized water.

2. Apparatus

- Jaw crusher with 150 mm (6") capacity.
- Sieves of the following sizes: 12.5 mm (½"), 6.3 mm (¼"), 2.00 mm (No. 10) and 75 µm (No. 200). Sieves shall conform to AASHTO M 92.
- Balance or scale: Capacity sufficient for the principle sample mass, readable to 0.1 percent or 0.1 g of the total sample mass and meeting the requirements of AASHTO M 231.
- 200 mm (8") sieve shaker with 45 mm (1¾") throw on cam at 285 ± 10 oscillations per minute.
- General Laboratory Interval Timer to control On-Off operation of sieve shaker. Timer will have a minimum 20 minute range accurate to ± 5 seconds.
- Plastic canister 190 mm (7 ½") in diameter and 150 mm (6") high, having a flat bottom or metal washing vessel conforming to AASHTO T 210 - 5.1.
- Distilled or demineralized water maintained at 22 ±3ºC (72 ± 5°F).
- Sample Washing Apparatus, consisting of a ring stand and ring capable of mounting a 230 mm mouth funnel with a 2.00 mm (No. 10) and 75 µm (No. 200) sieve setting on top of the funnel and a graduated cylinder calibrated at 500 ml with a rubber stopper.
- Graduated cylinder or pipette with 10 ml capacity graduated in 1 ml increments.
- Stock Sand Equivalent Solution prepared in accordance with WAQTC FOP for AASHTO T 176, using distilled water only. This solution should be stored in dark or opaque containers and protected from direct sunlight and heat. Solutions that have turned cloudy or formed precipitates will be discarded.
- Standard Sand Equivalent Cylinder with rubber stopper as described in WAQTC FOP for AASHTO T 176.
- Timer or Stopwatch, preferably with an alarm to indicate end of timed interval.
- Miscellaneous equipment including 500 ml wash bottle with a fine spray nozzle, pans, scoops, etc.

3. Degradation Test Area

The degradation test area must be free of vibration and direct sunlight, and maintained at a temperature of 22 ±3ºC (72 ± 5°F).

4. Sample Preparation

1. Unprocessed Aggregate
   a. Separate the aggregate on the 12.5 mm (½") sieve by hand or by mechanical shaker, sieving the material for 5 minutes. Discard the minus 12.5 mm (½") material unless required for other testing.

b. Crush the plus 12.5 mm (½") aggregate, or a representative portion obtained in accordance with WAQTC FOP for AASHTO T 248, to pass the 12.5 mm (½") sieve.

c. Proceed to Step 2 and process the same as already crushed aggregate.

2. Processed (already crushed) Aggregate

   a. Separate the material by hand sieving or by mechanical shaker, sieving the material for 5 minutes, into 2 size groups: minus 12.5 mm (½") to plus 6.3 mm (¼") and minus 6.3 mm (¼") to plus 2.00 mm (No. 10).

   b. Reduce each size grouping to a representative sample in accordance with WAQTC FOP for AASHTO T 248, Method A, such that there will be a minimum of 500 grams after washing.

   c. Wash each size grouping over a 2.00 mm (No. 10) sieve and dry to a constant mass in accordance with WAQTC FOP for AASHTO T 255/T 265.

   d. Weigh out a 500 ±1 g portion of each size grouping.

5. Procedure

1. Combine both sample portions in the plastic canister, add 200 ml of distilled or demineralized water and cover tightly. Do not allow the sample to soak more than 5 minutes before testing.

2. Place the canister in the degradation sieve shaker and run for 20 minutes ±5 seconds. Do not allow the sample to set for more than 5 minutes after agitation is completed.

3. Remove the canister and wash the material through nested 2.00 mm (No. 10) and 75 µm (No. 200) sieves. Continue washing until the wash water is clear and has reached the 500-ml mark on the graduated cylinder.

4. In instances where highly degradable materials are encountered and the sample cannot be washed clean with 500-ml. of water:

   a. Continue washing using water sparingly, until the wash water is clear. If a change in receiver cylinders is required, be very careful not to lose any of the wash water.

   b. To achieve the required 500 ml. volume, allow the wash water to settle until clear, then siphon or pipette off the excess water, being careful not to remove any of the settled material.

   c. Use of a centrifuge to settle the material is allowed but extreme care must be taken to preclude any loss of material in transferring from the cylinders to the centrifuge bottles and then back to a single cylinder. The solution must be brought to a volume of 500 ml before proceeding to Step 5. Removal of extra water by oven-dried evaporation is not allowed.

5. Place the Sand Equivalent Cylinder upright in a vibration free area out of direct sunlight. Measure and pour 7 ml of the Stock Sand Equivalent Solution into the cylinder.

6. Bring all of the solids in the 500 ml of wash water into suspension by capping the graduated cylinder with the palm of the hand or a rubber stopper, then turning the graduated cylinder upside down and right side up 10 times or until material is in suspension, allowing the bubble to traverse from one end to the other and back again, as rapidly as possible (approximately 35 seconds).

7. Immediately pour the solution into the Sand Equivalent Cylinder, fill to the 15 mark, and plug with a rubber stopper.

8. Mix the contents of the Sand Equivalent Cylinder by turning the cylinder upside down and right side up allowing the bubble to traverse from one end to the other and back again. This is one cycle. Repeat this cycle 20 times as rapidly as possible (approximately 35 seconds).

9. Place the cylinder on a vibration free platform out of direct sunlight, remove stopper and immediately start the timer or stopwatch that is pre-set for 20 minutes.

10. After 20 minutes, immediately read and record the height of the sediment to the nearest 0.1 graduation.

6. Calculations

Determine the Degradation Value by Table I, next page, which is derived from the following formula.

$$D = \left(\frac{15 - H}{15 + 1.75H} \right) x\, 100$$

Where:
D = Degradation value.
H = Height of sediment in cylinder.

Values may range from 0 to 100 with high values representing more suitable material. The formula and chart place doubtful materials at about the midrange (30-70) of the scale, with poor ones below and good ones above that range.

7. Report

Report degradation values to the nearest whole number.

Table 1

Degradation Value, "D"

H	D	H	D	H	D	H	D	H	D
0.1	98	3.1	58	6.1	35	9.1	19	12.1	8
0.2	96	3.2	57	6.2	34	9.2	19	12.2	8
0.3	95	3.3	56	6.3	33	9.3	18	12.3	7
0.4	93	3.4	55	6.4	33	9.4	18	12.4	7
0.5	91	3.5	54	6.5	32	9.5	17	12.5	7
0.6	90	3.6	54	6.6	32	9.6	17	12.6	6
0.7	88	6.7	53	6.7	31	9.7	17	12.7	6
0.8	87	3.8	52	6.8	30	9.8	16	12.8	6
0.9	85	3.9	51	6.9	30	9.9	16	12.9	6
1.0	84	4.0	50	7	29	10.0	15	13.0	5
1.1	82	4.1	49	7.1	29	10.1	15	13.1	5
1.2	81	4.2	48	7.2	28	10.2	15	13.2	5
1.3	79	4.3	48	7.3	28	10.3	14	13.3	4
1.4	78	4.4	47	7.4	27	10.4	14	13.4	4
1.5	77	4.5	46	7.5	27	10.5	13	13.5	4
1.6	75	4.6	45	7.6	26	10.6	13	13.6	4
1.7	74	4.7	44	7.7	26	10.7	13	13.7	3
1.8	73	4.8	44	7.8	25	10.8	12	13.8	3
1.9	71	4.9	43	7.9	25	10.9	12	13.9	3
2.0	70	5.0	42	8	24	11.0	12	14.0	3
2.1	69	5.1	41	8.1	24	11.1	11	14.1	2
2.2	68	5.2	41	8.2	23	11.2	11	14.2	2
2.3	67	5.3	40	8.3	23	11.3	11	14.3	2
2.4	66	5.4	39	8.4	22	11.4	10	14.4	1
2.5	65	5.5	39	8.5	22	11.5	10	14.5	1
2.6	63	5.6	38	8.6	21	11.6	10	14.6	1
2.7	62	5.7	37	8.7	21	11.7	9	14.7	1
2.8	61	5.8	37	8.8	20	11.8	9	14.8	0
2.9	60	5.9	36	8.9	20	11.9	9	14.9	0
3.0	59	6.0	35	9.0	20	12.0	8	15.0	0

Expansive Breakdown of Stone on Soaking in Ethylene Glycol
ATM 314

1. Scope

This method covers a procedure for subjecting samples of stone to immersion in ethylene glycol and observation of the effects of such immersion in accordance with CRD-D 148-69.

2. Principle of Method

Ethylene glycol is one of the materials that reacts with swelling clays of the montmorillonite group to form an organo-clay complex having a larger basal spacing than that of the clay mineral itself. Hence a sample of stone containing swelling clay of the montmorillonite group will be expected to undergo expansive breakdown upon soaking in ethylene glycol, if the amount, distribution, state of expansion, and ability to take up glycol is such as to cause such breakdown to occur. If such breakdown does occur, it may be expected that similar breakdown may occur if similar rock samples are exposed, for longer times, to wetting and drying or freezing and thawing in a water soaked condition in service.

3. Reagent

Ethylene Glycol – The regent used in this method shall be ethylene glycol meeting the requirements of ASTM D 2693.

4. Apparatus

- Jaw crusher with 150 mm (6") capacity.
- Sieves of the following sizes: 75 mm (3") and 19.0 mm (¾") and conforming to AASHTO M 92.
- Balance or scale: Capacity sufficient for the principle sample mass, readable to 0.1 percent or 0.1 g of the total sample mass and meeting the requirements of AASHTO M 231.
- Container shall be of suitable plastic, non-reactive with the reagent and of sufficient size to hold the test sample and sufficient reagent to cover all particles of the sample to a depth of not less that 10 mm (1/2") capped with a tight-fitting cover.

5. Sampling and Sample Preparation

1. Obtain representative samples of the stone in accordance with WAQTC FOP for AASHTO T 2.
2. Crush the rock to pass a 75 mm (3") sieve.
3. Separate the material into the required test size, using 75 mm (3") and 19 mm (¾") sieves, in accordance with WAQTC FOP for AASHTO T 27/T 11. Discard all particles retained on the 75 mm (3") sieve and all particles passing the 19 mm (¾") sieve, unless required for other testing.
4. Reduce the sample to a test size of 5 ± 2 kg (11 ± 1 lb) in accordance with WAQTC FOP for AASHTO T 248, Method A.
5. When a sample of the stipulated mass and particle size has been prepared, it shall be washed to remove dust, loosely adherent coatings, and chips. After being washed, dry to a constant mass in accordance with WAQTC FOP for AASHTO T 255/T 265 except that constant mass shall be regarded as having been attained when the loss in weight between successive weighing at intervals of not less than 4 hours does not exceed 0.1 percent. Determine the number of particles and the mass before immersion to the nearest 0.1 percent of the total sample mass.

6. Procedure

1. The sample shall be placed in the container and immersed in the reagent so that all particles are covered to a depth of at least 12.5 mm (½").
2. At intervals not to exceed 3 days, examine the sample and note significant changes. The normal duration of the test shall be 15 days.

   Note 3: Further information of value may be obtained in certain cases by continuing the treatment beyond 15 days: in other cases expansive breakdown may have been too extensive at earlier periods that no information of value will be obtained by continuing the treatment for the full 15 days.

3. When the exposure has been terminated, the sample shall be thoroughly washed and sieved by hand over a 19 mm (¾") sieve to remove the reagent from the surfaces of the particles and to remove fragments that will pass a 19 mm (¾") sieve. The material remaining on the sieve shall be dried to constant weight as described in Step 4 of the Sampling and Sample Preparation, and the total mass after immersion determined to the nearest 0.1 percent of the total sample mass.

7. Calculations

Calculate the total percent loss by:

$$\left(\frac{M_B - M_A}{M_B}\right) x\,100$$

where:
M_B = Mass before immersion, and
M_A = Mass after immersion.

8. Report

Report the percent loss to the nearest 1 percent on department forms.

SAMPLING BITUMINOUS MATERIALS (See Addendum for DOT&PF Guidelines)
WAQTC FOP FOR AASHTO T 40

Scope

The procedure covers obtaining samples of liquid bituminous materials in accordance with AASHTO T 40. Sampling of solid and semi-solid bituminous materials – included in AASHTO T 40 – is not covered here.

Agencies may be more specific on exactly who samples, where to sample, and what type of sampling device to use.

Procedure

1. Coordinate sampling with contractor or supplier.
2. Use appropriate safety equipment and precautions for hot liquids.
3. Allow a minimum of 4 L (1 gal) to flow before obtaining a sample(s).
4. Obtain samples of:
   - Asphalt binder from Hot Mix Asphalt (HMA) Plant from the line between the storage tank and the mixing plant while the plant is in operation, or from the delivery truck.
   - Cutback and Emulsified asphalt from distributor spray bar or application device; or from the delivery truck before it is pumped into the distributor. Sample emulsified asphalt at delivery or prior to dilution.

Containers

Sample containers must be new, and the inside may not be washed or rinsed. The outside may be wiped with a clean, dry cloth.

All samples shall be put in 1 L (1 qt) containers and properly identified on the outside of the container with contract number, date sampled, data sheet number, brand and grade of material, and sample number. Include lot and sublot numbers when appropriate.

- Emulsified asphalt: Use wide-mouth plastic jars with screw caps. Protect the samples from freezing since water is a part of the emulsion. The sample container should be completely filled to minimize a skin formation on the sample.
- Asphalt binder and Cutbacks: Use metal cans.

Note: The sample container shall not be submerged in solvent, nor shall it be wiped with a solvent saturated cloth. If cleaning is necessary, use a clean dry cloth.

Addendum WAQTC FOP for AASHTO T 40

The following guidelines for the use of WAQTC FOP for AASHTO T 40 by the State of Alaska DOT&PF.

1. When obtaining samples from HMA plants, sample only from the line between the storage tank and the mixing plant while the plant is in operation.
2. Sample containers for elastomer modified asphaltic cements must be new, and the inside may not be washed or rinsed. The outside may be wiped with a clean, dry cloth. All samples shall be put in 1 L (1 qt) wide mouth metal containers and properly identified on the outside of the container with contract number; date and time sampled, supplier, batch number and grade of material; and sample number. Include lot and sub-lot numbers when appropriate.
3. When sampling emulsified asphalt, use 1 gallon wide mouth plastic containers.

SAMPLING OF BITUMINOUS PAVING MIXTURES
FOP FOR AASHTO T 168 (See Addendum for DOT&PF Guidelines)

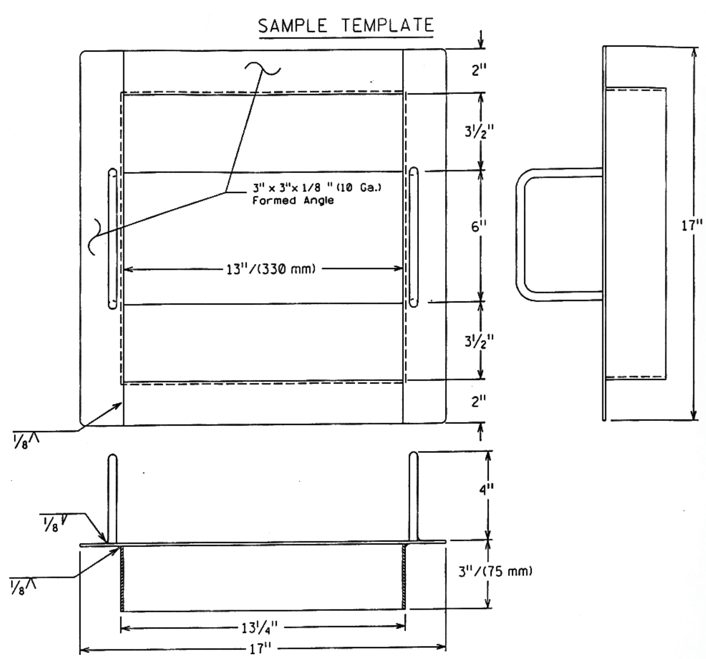
Scope

This procedure covers the sampling of bituminous paving mixtures from HMA plants, haul units, and roadways in accordance with AASHTO T 168. Sampling is as important as testing, and every precaution must be taken to obtain a truly representative sample.
The sampling of aggregate used in bituminous paving mixtures shall be in accordance with the FOP for AASHTO T 2.

Apparatus

- Flat-bottomed scoop 150 x 400 x 100 mm (6 x 16 x 4 in.) if sampling from a roadway
- Shovel
- Sample containers: such as cardboard boxes, metal cans, stainless steel bowls, or other agency-approved containers
- Template to match conveyor belt shape
- Scoops, trowels, or other equipment to obtain mix
- Sampling plate: heavy gauge metal plate 380 mm x 380 mm (15 in x 15 in) minimum 8 gauge thick with a wire attached to one corner long enough to reach from the center of the paver to the outside of the farthest auger extension. Holes ¼" in diameter should be provided in each corner.
- Cookie cutter sampling device: A 330 mm (13 in.) square sampling template, constructed from 75 mm x 50 mm x 3 mm (3 in. x 2 in. x 1/8 in.) formed steel angle with two 100mm x 150 mm x 9 mm (4 in. x 6 in. x 3/8 in.) handles. See diagram.

  Note 1: Sampling Plate and Cookie cutter may be sized appropriately to accommodate sample size requirements.



General Comments

1. Samples of mix upon which acceptance or rejection is based shall be selected at random, and may be obtained by, or under the observation of, the purchaser or authorized representative.

   Note 2: Care shall be taken to prevent contamination of bituminous mixes by dust or other foreign matter, and to avoid segregation of aggregate and bituminous materials.

2. Some agencies require mechanical sampling devices for hot mix asphalt (HMA) and cold feed aggregate on some projects. These are normally permanently attached devices that allow a sample container to pass perpendicularly through the entire stream of material or divert the entire stream of material into the container. Operation may be hydraulic, pneumatic, or manual and allows the sample container to pass through the stream twice, once in each direction, without overfilling. Special caution is necessary with manually operated systems since a consistent speed is difficult to maintain and non-representative samples may result. Check agency requirements for the specifics of required sampling systems.

Sample Size

Sample size depends on the test methods specified by the agency for acceptance. Check agency requirement for the size required.

Sampling

- **General**
  1. The material shall be inspected to determine variations. The seller shall provide equipment for safe and appropriate sampling including sampling devices on plants, when required.
  2. Place dense graded mixture samples in cardboard boxes, stainless steel bowls or other agency approved containers. Place open graded mixture samples in stainless steel bowls. Do not put open graded mixture samples in boxes until they have cooled to the point that bituminous material will not migrate from the aggregate.
  3. Sampling from the Roadway will require the contractor to repair the sampled location.

- **Sampling from a Conveyor Belt**
  1. Stop the conveyor belt.
  2. Select at least three areas of approximately equal size on the belt for sampling.
  3. Insert template, the shape of which conforms to the shape of the belt, in each of the locations to be sampled.
  4. Obtain three approximately equal increments of material that will form a sample of the required size when combined.
  5. Scoop all material between template into a suitable container.

- **Attached Sampling Devices**
  1. When using an attached sampling device, pass the container twice through the material perpendicularly without overfilling the container.
  2. Repeat until proper sample size has been obtained.

- **Sampling from Haul Units**
  1. Obtain samples in four approximately equal increments from haul units.
  2. Obtain each increment from approximately 300 mm (12 in.) below the surface, in each of the four quadrants of the load.
  3. Combine the increments to form a sample of the required size.
- **Sampling from a Roadway Prior to Compaction (Scoop Method)**
  1. Obtain samples in approximately equal increments, after placement and prior to rolling, using the scoop.
  2. Make a vertical face with the shovel about 750 mm (30 in.) parallel with centerline.
  3. Pull the material back approximately 450 mm (18 in.).
  4. Place the scoop on the pavement or base as flat as possible at one side of the vertical face and fill the scoop. Make sure that sufficient pressure is exerted on the scoop to remove all of the material to its full depth.
  5. Close the lid and remove the scoop when it is full.
  6. Repeat Steps 2 through 5 to obtain the required sample size.
- **Sampling from Roadway Prior to Compaction (Plate Method)**

  Plate Method using the "cookie cutter" sampling device

  There are two conditions that will be encountered when sampling Hot Mix Asphalt (HMA) from the roadway prior to compaction. The two conditions are:

  1. Laying HMA on grade or untreated base material requires Method 1.
  2. Laying HMA on existing asphalt or laying a second lift of HMA requires Method 2.

  <u>SAFETY:</u>

  Sampling is performed behind the paving machine and in front of the breakdown roller. For safety, the roller must remain at least 3 m (10 ft) behind the sampling operation until the sample has been taken and the hole filled with loose HMA.

  Method 1 requires a plate to be placed in the roadway in front of the paving operation and therefore there is always concern with moving, operating equipment. It is safest to stop the paving train while a plate is installed in front of the paver. When this is not possible the following safety rules must be followed.

  1. The plate placing operation must be at least 3 m (10 ft) in front of the paver or pickup device. The technician placing the plate must have eye contact and communication with the paving machine operator. If eye contact cannot be maintained at all time, a third person must be present to provide communication between the operator and the technician.
  2. No technician is to be between the asphalt supply trucks and the paving machine. The exception to this rule is if the supply truck is moving forward creating a windrow, in which case the technician must be at least 3m (10 ft) behind the truck.

3. At any time the Engineer feels that the sampling technique is creating an unsafe condition, the operation is to be halted until it is made safe or the paving operation will be stopped while the plate is being placed.

Method 1 - Obtaining a Sample on Untreated Base:

1. Following the safety rules detailed above, the technician is to:
    a. Smooth out a location in front of the paver at least 0.5 m (2 ft) inside the edge of the mat.
    b. Lay the plate down diagonally with the direction of travel, keeping it flat and tight to the base with the lead corner facing the paving machine.
2. Secure the plate in place by driving a nail through the hole in the lead corner of the plate.
3. Pull the wire, attached to the outside corner of the plate, taut past the edge of the HMA mat and secure with a nail.
4. Let the paving operation proceed over the plate and wire. Immediately proceed with the sampling.
5. Using the exposed end of the wire, pull the wire up through the fresh HMA to locate the corner of the plate. Place the "cookie cutter" sample device, just inside the end of the wire; align the cutter over the plate. Press "cookie cutter" device down through the HMA to the plate.
6. Using a small square tipped shovel and/or scoop, carefully remove all the HMA from inside of the cutter and place in a sample container.
7. Remove the sample cutter and the plate from the roadway. The hole made from the sampling must be filled with loose HMA.

Method 2 - Obtaining a Sample on Asphalt Surface:

1. After the paving machine has passed the sampling point, immediately place the "cookie cutter" sampling device on the location to be sampled. Push the cutter down through the HMA until it is flat against the underlying asphalt mat.
2. Using a small square tipped shovel and/or scoop, carefully remove all the HMA from inside of the cutter and place in a sample container. The hole made from sampling must filled with loose HMA.

Identification and Shipping

1. Identify sample containers as required by the agency.
2. Ship samples in containers that will prevent loss, contamination, or damage.

Addendum WAQTC FOP for AASHTO T 168

Following are guidelines for the use of WAQTC FOP for AASHTO T 168 by the State of Alaska DOT&PF.

1. When allowed by specification, sampling methods found in ATM 403 may be used.

2. When sampling asphalt from a mat after compaction, sample in accordance with Section 413, WAQTC TM 11, "Sampling Bituminous Material after compaction (Obtaining Cores)."

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Sampling Hot Mix Asphalt ATM 403

1. Scope

This method describes the procedures used for sampling Hot Mix Asphalt (HMA).

2. Significance and Use

This method provides procedures for sampling HMA in the field.

2.1. Sampling is equally as important as the testing, and the sampler shall use every precaution to obtain samples that will yield an acceptable estimate of the nature and conditions of the materials for which they represent.

2.2. Care shall be taken in sampling to avoid segregation of the material being sampled, and to prevent contamination by dust or other foreign matter.

3. Equipment

3.1 Flat scoop with vertical sides or a square point shovel

3.2 Plate with small lip (approximately ½”) and of sufficient size and rigidity to accommodate required sample. Plate to have wire(s) attached to allow the plate to be located and removed from the mat after paver travels past it.

3.3 Approved sample containers including new cardboard boxes, clean metal buckets, cans or bowls.

3.4 Miscellaneous tools, scrapper, scoop, gloves, etc.

4. Sampling from the Auger

4.1 Obtain samples from the accessible portion of the auger, using a square point shovel.

4.2 Place the shovel in front of the auger, with the blade flat upon the surface to be paved.

4.3 Allow the front face of the HMA coming off the auger to cover the shovel. Remove the shovel before the auger reaches the shovel by lifting it upward as vertically as possible being careful not to lose material.

4.4 Repeat the procedure at least three times, but as many times as necessary to obtain a sample of the required size.

4.5 Place the sample in an approved container for transport to Lab.

5. Lipped Plate Sampling

5.1 When using a pickup machine:

5.1.1 Stop the paver and pickup machine.

5.1.2 Place plate(s) underneath the pickup machine, midway between and just behind the rear tires and right in front of the paver.

5.2 When using dump trucks:

5.2.1 Stop the paver after the truck is attached to the paver.

5.2.2 Place plate(s) at the midpoint of the axis of the paver and behind the truck tires.

Note: when placing plate(s), avoid influence from truck tires, pickup machine tires, and paver tracks or tires.

5.3. Run an attached wire perpendicular to the direction of the paver, beyond the farthest auger extension and/or the ski.

5.4. Hold the wire to the ground with your foot.

5.5. Allow the paving operation to resume.

5.6. When the paver has passed over the plate position, pull up on the wire to locate the plate. Remove the plate(s) laden with mix from the HMA mat by lifting vertically being careful not to disturb the mix at the edge of the plate.

5.7. Place the sample in an approved container for transport to the Lab.

Note: make sure to hold the wire down on the ground so the ski will not snag it.

6. Windrow Sampling

6.1 When HMA is dumped in a windrow, sample in three locations equidistantly spaced longitudinally along the top of the middle third of the windrow.

6.2 Obtain sample increments by removing and discarding the top 12 inches of the windrow. Remove a portion by digging vertically down with a square point shovel. Repeat for each increment.

6.3 Combine the three increments to form the composite sample.

6.4 Place the sample in an approved container for transport to the Lab.

REDUCING SAMPLES OF HOT MIX ASPHALT TO TESTING SIZE
FOP FOR WAQTC TM 5 (See Addendum for DOT&PF Guidelines)

Significance

Samples of bituminous paving mixes taken in accordance with AASHTO T 168 are composites and are large to increase the likelihood that they are representative of the product being tested. Materials sampled in the field need to be reduced to appropriate sizes for testing. As a general rule, field samples should be of a size that splitting once will result in the required test sample size. It is extremely important that the procedure used to reduce the field sample not modify the material properties.

Scope

This method covers the procedure reducing samples of Hot Mixed Asphalt (HMA). The samples are to be acquired in accordance with AASHTO T 168 and the increments placed in an agency approved suitable container. The sample is to be representative of the average of the HMA being produced.

Apparatus

- Flat-bottom scoop,
- Non-stick splitting surface such as metal, paper, or heat-resistant plastic,
- Large spatulas, trowels, metal straightedge or 12 in. dry wall taping knife, sheet metal quartering device,
- Thermostatically controlled oven capable of maintaining a temperature of at least 110°C (230°F) or high enough to heat the material to a pliable condition for splitting,
- Miscellaneous equipment including trowel(s), spatula(s), hot plate, non-asbestos heat-resistant gloves or mittens, pans, buckets, and cans.

Sample Preparation

The sample must be warm enough to separate. If not, warm in an oven until it is sufficiently soft to mix and separate easily. Do not exceed either the temperature or time limits specified in the test method(s) to be performed.

Overview

- Large Samples
- Method A: Loaf (Incremental) method
- Method B: Quartering by apex
- Method C: Quartering

Procedure

Large Samples, samples over 35 kg (75 lb)

1. Heat the trowel(s), spatula(s), and splitting apparatus to approximately 110°C (230°F).

2. Place the sample on a surface where there will be neither loss of material nor the accidental addition of foreign material. The surface may be covered with heavy paper or other suitable material. Remove the sample from the agency approved container by dumping into a conical pile.

3. Mix the material thoroughly by turning the entire sample over a minimum of four times. With the last turning, form the entire sample into a conical pile. Mixing may be accomplished by turning the pile with a heated spatula or by rolling the material over with paper or other material used for the rolling surface. Make a visual observation to determine that the material is homogenous.

***Note 1*:** Some HMA mixes are prone to segregation and manipulation of the material should be minimized.

4. Flatten the conical pile to a uniform thickness and diameter by pressing down with a hot spatula or trowel. The diameter should be four to eight times the thickness.
5. Divide the flattened pile into four approximately equal quarters with a heated spatula, trowel, flat metal plate, or sheet metal quartering splitter.
6. With the quartering device in place remove each quarter of the material and place in agency approved containers for testing, storage or shipment. Mark containers per the Sample Identification section.
7. Pay particular attention that excessive amounts of materials are not left on the splitting surface or splitting equipment.

8. When further reduction of the HMA is to be done at this time, reduce by using methods A, B, and C. A combination of the reduction methods may be used if allowed by the agency.

Reduction to Test Size

Method A (Loaf / Incremental method)

1. Place the sample on a surface where there will be neither loss of material nor the accidental addition of foreign material. The surface may be covered with heavy paper, or other suitable material. Remove the sample from the agency approved containers by dumping into a conical pile.
2. Mix the sample thoroughly by turning the entire sample over a minimum of four times. Alternately lift each corner of the paper and pull it over the sample diagonally toward the opposite corner causing the material to be rolled. With the last turning, lift both opposite corners to form a conical pile. Make a visual observation to determine that the material is homogenous.
3. Grasp the paper, roll the material into a loaf and flatten the top.
4. Pull the paper so at least ¼ of the length of the loaf is off the edge of the counter. Allow this material to drop into a container to be saved. As an alternate, using a straight edge, slice off approximately ¼ of the length of the loaf and place in a container to be saved.
5. Pull additional material (loaf) off the edge of the counter and drop the appropriate size sample into a sample pan or container. As an alternate, using a straight edge, slice off an appropriate size sample from the length of the loaf and place in a sample pan or container.
6. Repeat step 5 until the proper size sample has been acquired. Step 5 is to be repeated until all the samples for testing have been obtained.

Note 2 - When reducing the sample to test size it is advisable to take several small increments determining the mass each time until the proper minimum size is achieved. Unless the sample size is grossly in excess of the minimum or exceeds the maximum test size use the sample as reduced for the test.

Method B (Quartering by apex)

1. Place the sample on a surface where there will be neither loss of material nor the accidental addition of foreign material. The surface may be covered with heavy paper, or other suitable material. Remove the sample from the containers by dumping into a conical pile.
2. Mix the sample thoroughly by turning the entire sample over a minimum of four times. Alternately lift each corner of the paper and pull it over the sample diagonally toward the opposite corner causing the material to be rolled. With the last turning, lift both opposite corners to form a conical pile. Make a visual observation to determine that the material is homogenous.
3. Flatten the conical pile to a uniform thickness and diameter by pressing down with a hot spatula or trowel. The diameter should be four to eight times the thickness.
4. Quarter the flattened pile using a quartering device or straightedge.
5. With the quartering device in place using a straightedge (taping knife) slice through the quarter of the HMA from the apex of the quarter to the outer edge. Pull or drag the material from the quarter holding one edge of the straightedge (taping knife) in contact with the quartering device. Two straight edges may be used in lieu of the quartering device.
6. Slide or scoop the material into a sample pan. Repeat step 5 removing a similar amount of material from the opposite quarter. Step 5 is to be repeated until all the samples for testing have been obtained.

Note 3- When reducing the sample to test size it is advisable to take several small increments determining the mass each time until the proper minimum size is achieved. Unless the sample size is grossly in excess of the minimum or exceeds the maximum test size use the sample as reduced for the test.

Method C (Quartering)

1. Place the sample on a surface where there will be neither loss of material nor the accidental addition of foreign material. The surface may be covered with heavy paper, or other suitable material. Remove the sample from the containers by dumping into a conical pile.
2. Mix the sample thoroughly by turning the entire sample over a minimum of four times. Alternately lift each corner of the paper and pull it over the sample diagonally toward the opposite corner causing the material to be rolled. With the last turning, lift both opposite corners to form a conical pile. Make a visual observation to determine that the material is homogenous.
3. Flatten the conical pile to a uniform thickness and diameter by pressing down with a hot spatula or trowel. The diameter should be four to eight times the thickness.
4. Quarter the flattened pile using a quartering device or straightedge.
5. Remove the opposite quarters saving the material for future use.
6. Repeat step 2 through 5 until the proper size sample has been achieved.
7. When additional test specimens are required, dump the removed material into a conical pile as in step 1 and repeat steps 2 through 6. This process may be repeated until sample has been reduced to testing size for all tests.

Sample Identification

1. Identify the sample as required by the agency.
2. Samples shall be submitted in agency approved containers and secured to prevent contamination and spillage.
3. The exact disposition of each quarter of the original field sample shall be determined by the agency.

Addendum WAQTC TM 5

Following are guidelines for the use of WAQTC TM 5 by the State of Alaska DOT&PF.

1. A combination of the presented methods may be used in reducing an HMA sample to testing size.

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Asphalt Cement Content of Hot Mix Asphalt by the Nuclear Method ATM 405

1. Scope

This method covers the quantitative determination of the asphalt cement content of Hot Mix Asphalt by testing a sample with a device that utilizes neutron thermalization techniques. This is an adaptation of AASHTO T 287. Job mix design (JMD) calibration, cross calibration of master and field gauges and calibration transfer are included.

2. Referenced Documents

- WAQTC Standards:
  - FOP for AASHTO T 2, Sampling of Aggregates
  - FOP for AASHTO T 168, Sampling Bituminous Paving Mixtures
  - TM 5, Reducing Samples of Hot Mix Asphalt to Testing Size
  - FOP for AASHTO T 329, Moisture Content of Bituminous Mixes by Oven
- Other Documents:
  - Manufacturer's instruction manual.

3. Significance and Use

This method can be used for rapidly determining the asphalt content of HMA. Testing can be completed in a matter of minutes so that adjustments, if necessary, can be made in the asphalt metering system with a limited amount of mix production. The procedure is useful in the determination of asphalt content only, as it does not provide extracted aggregate for the gradation analysis.

4. Apparatus

- Nuclear asphalt content gauge system consisting of:
  - Neutron source: an encapsulated and sealed radioactive source
  - Thermal neutron detectors
  - Read-out instrument displaying, at a minimum, percent asphalt cement
  - Two or more stainless steel sample pans conforming to gauge requirements
- Sample containers with lids or other methods of closing to prevent contamination and of sufficient size to hold the entire sample. The containers should be able to withstand the reheating of the mix to mixing temperature.
- Sample quartering apparatus conforming to requirements of the WAQTC TM 5.
- Balance or scale: capable of determining mass to 15 kg, readable to 0.1 g and conforming to AASHTO M 231
- Drying oven, of either of the following types, capable of handling the volume and sample size expected for the project:
- Forced air, ventilated or convection oven capable of maintaining a temperature of 177 ±3°C (350 ±5°F)
- Leveling plate: Flat, rigid plate of metal with a minimum thickness of 10 mm (⅜ in) and slightly larger than the sample pans
- Thermometer with a temperature range of 10-300°C (50-500°F)
- Assorted pans, spoons, spatulas, and mixing bowls
- Radioactive materials information and calibration packet containing:

- Daily Background Count Log
- Leak Test Certificate
- Shippers Declaration for Dangerous Goods
- Procedure Memo for Storing, Transporting and Handling Nuclear Testing Equipment
- Other radioactive materials documentation as required by local regulatory requirements

5. Precautions

1. The equipment shall be so constructed as to be licensable in accordance with applicable health and safety regulations.
2. Equipment operators shall wear an approved form of radiation dosimetry (i.e., film badges, thermo luminescent dosimeter, etc) capable of monitoring the occupational radiation exposure.
3. Since nuclear equipment measures the total amount of hydrogen in the sample, this procedure is sensitive to changes in moisture content. It must be remembered that both asphalt cement and water contain hydrogen.
4. Keep any other source of neutron radiation at least 10 m (30 ft) from the equipment. Do not place the equipment where large amounts of hydrogenous material may be moved during the calibration or testing procedures (for example, water or plastic materials).
5. All personnel shall be kept at least 1 m (3 ft) away from the gauge during testing.

6. Standardization

1. Obtain and record a 16 minute background count, in accordance with manufacturer's procedure, each day prior to taking test measurements or whenever the gauge has been moved or the conditions within 1 m (3 ft) of the gauge have changed. The measurement time for the background count is the same as that used for test measurements.
2. If the background count has not changed by more than 2 percent from the previous background count, then the apparatus shall be considered stable and acceptable for use. If the gauge has been moved or if the surrounding conditions have changed, additional background counts must be obtained until the 2 percent standard is met.

7. Calibration

1. This method is sensitive to the type of aggregate, percentage and source of asphalt cement, and to the aggregate gradation. Accordingly, a calibration curve must be developed for each mix type. When changes occur, a new calibration should be run. The curve shall be established with 3 points. (See Attachment A)
2. Prior to the start of each test, verify that the activated calibration is correct.

8. Procedure

1. Determine the mass of a clean gauge sample pan, and use this to determine the sample mass in the pan, or tare the pan on the scale.
2. Using a hot asphalt concrete mixture sample having a temperature of 121° to 149°C (250° to 300°F) obtained in accordance with WAQTC FOP for AASHTO T 168, and reduced in accordance with WAQTC TM 5, fill the sample pan one-half full, evenly distributing the sample in the pan. Level the asphalt concrete mixture with a preheated trowel or spatula, spading as necessary to compact (usually 10 to 15 spades are sufficient), being careful to avoid segregating the mix or driving the fines into the bottom.

3. Fill the remainder of the pan until the mass of the asphalt concrete mixture in the pan is approximately equal to or up to 5 grams above the mass of mix used for the calibration samples. Level the top of the asphalt concrete mixture using a spatula or trowel and spade as necessary to compact (usually 10 to 15 spades are sufficient), avoiding segregation of the mix. Compact the sample into the pan, until it is level with the top of the pan, by standing on the metal plate and rocking/twisting back-and-forth.
4. Verify that the mass of mix is ± 5 g of the calibration mass. Record the mass of the asphalt concrete mixture in the pan.
5. If the gauge does not have temperature compensation capability, measure and record the temperature of the compacted specimen. This temperature must be within ± 5°C (± 9°F) of the calibration test specimen temperature.
6. Place the pan into the gauge. Perform a 16 minute count.
7. Determine and record the uncorrected asphalt cement content to the nearest 0.01 percent by direct readout from the gauge, from the calibration graph, or by the formula supplied by the manufacturer.
8. Using a representative portion of the original sample or a portion of the material removed from the gauge pan, determine the moisture in the mixture in accordance with the WAQTC FOP for AASHTO T 329 and record to the nearest 0.01 percent.

Note 1: When taking the moisture from the gauge pan sample, remove it immediately after completing the oil content test.

9. Calculation

1. Subtract the moisture content from the uncorrected asphalt cement content. Record this as the corrected asphalt cement content.

10. Report

Results shall be reported on standard forms approved by the agency. Report the following information.

- Make, model, and serial number of the nuclear asphalt content gauge.
- Date and source of calibration.
- Date of test.
- Name and signature of operator.
- Background count for the day of the test.
- Mix identification.
- Aggregate type and source(s); Asphalt cement source, type and grade.
- Calibration sample mass and temperature.
- Test sample mass and temperature, if gauge does not have temperature compensation capability
- Gauge reading, including print-out from gauge.
- Asphalt cement content value to the nearest 0.1 %.
- Attach the Nuclear Gauge print out to the report.

Attachment A ATM 405

1. Gauge Calibration

1. Obtain samples of aggregate in accordance with WAQTC FOP for AASHTO T 2. Approximately 50 kg (110 lb) total will be required for calibration specimens. Dry the aggregates in accordance with WAQTC FOP for AASHTO T 255/T 265, separate into sieve sizes determined by the JMD.

2. Blend the aggregate together at the proper proportion to match the job mix formula following steps 3 and 4.

3. Calculate the required cumulative mass for each specified sieve using the following formula:

$$X = \frac{(100 - P)}{100} \times T$$

   where:
   X = Required cumulative batch mass for each specified sieve
   P = Percent passing for each specified sieve according to the job mix formula
   T = Initial total aggregate mass

4. Correct for aggregate dust as follows.

   a. Prepare a wash gradation sample from the mass calculated in Step 4.
   b. Perform a washed gradation following WAQTC FOP for AASHTO T 27/T 11.
   c. Compute the corrected batch mass for each specified sieve for the calibration points using the following formula:

$$Z_n = \frac{X^2}{Y}$$

   where:
   Z_n = Adjusted cumulative batch mass for sieve size n.
   X = Pre-wash cumulative batch mass for each specified sieve.
   Y = Post-wash cumulative batch mass for each specified sieve.

5. Obtain samples of bituminous materials in accordance with WAQTC FOP for AASHTO T 40. Approximately 4 L (1 gal) will be required.

6. Calculate the mass of asphalt cement for each calibration point as follows:

$$B = E \times P_{bm}$$

   where:
   B = mass of asphalt cement to the nearest 0.1 g
   E = mass of mix
   P_{bm} = percent asphalt cement content by total mass of mixture, expressed as a decimal.

7. Use the three following asphalt cement contents:

   - Specified minus 1.0 percent
   - Specified (mix design value)
   - Specified plus 1.0 percent

8. Calculate the mass of aggregate required for each calibration point as follows:

$$A = E - B$$

where:

A = mass of aggregate to the nearest 0.1 g
B = mass of asphalt cement to the nearest 0.1 g
E = mass of mix

2. Preparation of Calibration Specimens

1. Heat the prepared aggregate specimens to the mixing temperature range midpoint for the asphalt cement ± 5°C (± 9°F) and hold at that temperature for three hours or to constant mass.

2. Heat the asphalt cement to the mid-point of the mixing temperature range ± 5°C (± 9°F) in a covered container(s). It is best to use the asphalt cement as soon as it reaches mixing temperature. If this is not possible, maintain the asphalt cement at this temperature, rather than cool and reheat it, but do not hold the sample at this temperature for more than 4 hours.

3. All bowls, sample pans, and tools should be heated to the mid-point of the mixing temperature range ± 5°C (± 9°F). An initial or "butter" mix is required to condition the mixing equipment. Mix a minimum of three asphalt concrete specimens to cover the approximate range of the design asphalt content. Mix one at the design asphalt content, one 1.0 percent above, and one 1.0 percent below, use the same grade and type of asphalt as will be used in the asphalt concrete mixture to be tested. Mix 100g over the target calibration mass for each specimen.

4. Fill the sample pan one-half full, evenly distributing the sample in the pan. Level the asphalt concrete mixture with a spatula or trowel and spade as necessary to compact, avoiding segregation of the mix. Fill the remainder of the pan until the weight of the asphalt concrete mixture in the pan equals the dry aggregate weight. If the pan is not full, fill the pan to the point that the asphalt concrete mixture is mounded slightly above the top of the pan. Record the weight of the asphalt concrete mixture in the pan. This is the weight that is to be used for all calibration and test samples using this calibration. Level the top of the asphalt concrete mixture using a spatula or trowel and spade as necessary to compact, avoiding segregation of the mix. Use the metal plate to consolidate the asphalt concrete mixture until it is level with the top edge of the pan. All specimens should be compacted at the mid-point of the mixing temperature range ± 5°C (± 9°F) to ensure that the mix will compact properly.

5. Place each calibration pan into the gauge and proceed in accordance with the manufacturer's instructions for operation of the equipment and the sequence of operations. Count each calibration sample for 16 minutes.

   Note: Do not forget to perform and record a background count as per the manufacturer's instructions.

6. For gauges that generate the calibration internally, print out the formula coefficients ("A" Values), the coefficient of fit and the calculated percent difference for each calibration point. The coefficient of fit must be between 0.998 and 1.000 for dense graded mix or 0.995 and 1.000 for open graded mix. Calibration points must have a calculated percent difference of less than 0.09 percent. If either requirement is not met, the calibration must be redone.

7. Store the acceptable calibration in the gauge's memory, using the job mix formula and the Contract number or an easily recognizable calibration number, according to the manufacturer's instructions.

8. For gauges other than the Troxler, prepare a calibration curve by plotting the calibration sample gauge readings versus asphalt cement content on linear graph paper, choosing convenient scale factors for gauge readings and asphalt cement content.

9. Calculate the correlation factor for gauges without internal calculations according the following formula:

$$CorrelationFactor = \sqrt{1 - \frac{\sum_i \left(Y_i - \hat{Y}_i \right)^2}{\sum_i \left(Y_i - \overline{Y}_i \right)^2}}$$

where:
Y_i = actual percent asphalt values for each sample
$\hat{Y}_i$ = calculated percent asphalt values from curve
$\overline{Y}_i$ = mean value of the actual percentages asphalt, and
i = number of calibration samples.

Attachment B ATM 405

1. Cross Calibration (Troxler 3241)

1. Cross calibrating creates a relationship between the field gauge and a master gauge. This allows testing of production mix with a field gauge without the need to perform physical calibrations. When several gauges are cross calibrated, the mix calibrations may be transferred to each. The master gauge is normally located at where the calibration sample pans are fabricated.
2. The central lab shall prepare the cross calibration samples. Prepare six calibration samples, using a locally available specification aggregate, with binder contents between 3 and 8 percent at 1 percent increments or per the gauge manufacturer's instructions. Mix the samples so that each pan of mix equals the base mass ± 5 g. Run each sample in the master gauge using a 16 minute count in the normal calibration mode. After all samples are run, the gauge will automatically calculate a coefficient of fit. The coefficient of fit must be at least 0.999.
3. Seal each pan to prevent change in hydrogen content and repeat steps 1 and 2. Sealed pans must meet same criteria.
4. Run each of the six sealed calibration samples in the field gauge while in cross calibration mode utilizing a 16 minute count. For each calibration sample, input the information from the master gauge into the field gauge. When the six cross calibration samples have been counted, print out the cross calibration data. The coefficient of fit must be .999 or 1.000. If this requirement is met, the master gauge and the field gauge are cross calibrated.

2. Calibration Transfer

When the field gauge has been cross calibrated with the master gauge a calibration transfer can be performed. JMD calibrations can now be transferred to the field gauge, using input data only. This transfer would be in lieu of calibrating the field gauge with a JMD calibration. Follow the manufacturer's instructions to perform this transfer.

Attachment C ATM 405

PERFORMANCE EXAM CHECKLIST

ASPHALT BINDER CONTENT OF BITUMINOUS MIXTURES BY THE NUCLEAR METHOD ATM 405

Participant Name ______________________________ Exam Date ______________

Procedure Element	Trial 1	Trial 2
1. Precautions for gauge adequately described?	_____	_____
2. Sample obtained as per AASHTO T 168?	_____	_____
3. Sample reduced as per WAQTC TM-5?	_____	_____
4. First layer properly consolidated?	_____	_____
5. Second layer properly consolidated?	_____	_____
6. Sample compacted using the correct size leveling plate?	_____	_____
7. Mass checks within ±5 g of base mass?	_____	_____
8. Temperature of mix recorded (if necessary)?	_____	_____
9. Correct calibration used?	_____	_____
10. 16 minute count taken and uncorrected binder content recorded to 0.01 percent?	_____	_____
11. Corrected binder content correctly determined and recorded to nearest 0.1 percent?	_____	_____

Comments: First trial: Pass ☐ Fail ☐ Second trial: Pass ☐ Fail ☐

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Signature of Examiner ____

DETERMINING THE ASPHALT BINDER CONTENT OF HOT MIX ASPHALT (HMA) BY THE IGNITION METHOD (See Addendum for DOT&PF Guidelines)
WAQTC FOP FOR AASHTO T 308

Scope

This procedure covers the determination of asphalt binder content of hot mix asphalt (HMA) by ignition of the binder at 538°C (1000°F) or less in a furnace; samples may be heated by convection or direct infrared irradiation. The aggregate remaining after burning can be used for sieve analysis using the FOP for AASHTO T 30.

Two methods – A and B – are presented.

Some agencies allow the use of recycled HMA. When using recycled HMA, check with the agency for specific correction procedures.

Background on Test Method

Binder in the HMA is ignited in a furnace. Asphalt binder content is calculated as the difference between the initial mass of the HMA and the mass of the residual aggregate, correction factor, and moisture content. The asphalt binder content is expressed as percent of moisture-free mix mass.

Sampling

1. Obtain samples of HMA in accordance with the FOP for AASHTO T 168.
2. Reduce HMA samples in accordance with the FOP for WAQTC TM 5.
3. If the mixture is not sufficiently soft to separate with a spatula or trowel, place it in a large flat pan in an oven at 125 ±5°C (257 ±9°F) until soft enough.
4. Test sample size shall be governed by nominal maximum aggregate size and shall conform to the mass requirement shown in Table 1. When the mass of the test specimen exceeds the capacity of the equipment used, the test specimen may be divided into suitable increments, tested, and the results appropriately combined through a weighted average for calculation of the binder content.

Note 1: Large samples of fine mixes tend to result in incomplete ignition of asphalt.

Table 1

Nominal Maximum Aggregate Size* mm (in.)	**Minimum Mass Specimen** g	**Maximum Mass Specimen** g
37.5 (1 ½)	4000	4500
25.0 (1)	3000	3500
19.0 (3/4)	2000	2500
12.5 (1/2)	1500	2000
9.5 (3/8)	1200	1700
4.75 (No. 4)	1200	1700

* One sieve larger than the first sieve to retain more than 10 percent of the material using an agency specified set of sieves based on cumulative percent retained. Where large gaps in specification sieves exist, intermediate sieve(s) may be inserted to determine nominal maximum size.

Apparatus

Note 2: The apparatus must be calibrated for the specific mix design. See "Correction Factors" at the end of this FOP.

There are two methods – A and B. The apparatus for the two methods are the same except that the furnace for Method A has an internal balance.

- Forced air ignition furnace, capable of maintaining the temperature at 578°C (1072°F).

  For Method A, the furnace will be quipped with an internal scale thermally isolated from the furnace chamber and accurate to 0.1 g. The scale shall be capable of determining the mass of a 3500 g sample in addition to the sample baskets. A data collection system will be included so that mass can be automatically determined and displayed during the test. The furnace shall have a built-in computer program to calculate change in mass of the sample baskets and provide for the input of a correction factor for aggregate loss. The furnace shall provide a printed ticket with the initial specimen mass, specimen mass loss, temperature compensation, correction factor, corrected binder content, test time, and test temperature. The furnace shall provide an audible alarm and indicator light when the sample mass loss does not exceed 0.01 % of the total sample mass for three consecutive minutes.

  Note 3: The furnace shall be designed to permit the operator to change the ending mass loss percentage from 0.01 percent to 0.02 percent.

  For both Method A and Method B, the furnace chamber dimensions shall be adequate to accommodate a 3500 g sample. The furnace door shall be equipped so that it cannot be opened during the ignition test. A method for reducing furnace emissions shall be provided and the furnace shall be vented so that no emissions escape into the laboratory. The furnace shall have a fan to pull air through the furnace to expedite the test and to eliminate the escape of smoke into the laboratory.

- Sample Basket Assembly: consisting of sample basket(s), catch pan, and basket guards. Sample basket(s) will be of appropriate size allowing samples to be thinly spread and allowing air to flow through and around the sample particles. Sets of two or more baskets shall be nested. A catch pan: of sufficient size to hold the sample basket(s) so that aggregate particles and melting binder falling through the screen mesh are caught. Basket guards will completely enclose the basket and be made of screen mesh, perforated stainless steel plate, or other suitable material.

  Note 4: Screen mesh or other suitable material with maximum and minimum opening of 2.36 mm (No. 8) and 600 µm (No. 30) respectively has been found to perform well.

- Thermometer, or other temperature measuring device, with a temperature range of 10 -260°C (50-500°F).
- Oven capable of maintaining 125 ±5°C (257 ±9°F).
- Balance or scale: capacity sufficient for the sample mass and conforming to the requirements of M 231, Class G2.
- **Safety equipment:** Safety glasses or face shield, high temperature gloves, long sleeve jacket, a heat resistant surface capable of withstanding 650°C (1202°F), and a protective cage capable of surrounding the sample baskets during the cooling period. Particle mask for use during removal of the sample from the basket assembly.

- Miscellaneous equipment: A pan larger than the sample basket(s) for transferring sample after ignition, spatulas, bowls, and wire brushes.

Procedure – Method A (Internal Balance)

1. Preheat the ignition furnace to 538°C (1000°F) or to the temperature determined in the "Correction Factor" section, Step 9 of this method. Manually record the furnace temperature (set point) prior to the initiation of the test if the furnace does not record automatically.
2. Dry the sample to constant mass, according to the FOP for AASHTO T 329; or determine the moisture content of a companion sample in accordance with the FOP for AASHTO T 329.
3. Determine and record the mass to the nearest 0.1 g of the sample basket assembly.
4. Evenly distribute the sample in the sample basket assembly, taking care to keep the material away from the edges of the basket. Use a spatula or trowel to level the sample.
5. Determine and record the total mass to the nearest 0.1 g of the sample and sample basket assembly. Calculate and record the initial mass of the sample (total mass minus the mass of the sample basket assembly) to the nearest 0.1 g. Designate this mass as (M_i).
6. Record the correction factor or input into the furnace controller for the specific HMA.
7. Input the initial mass of the sample (M_i) into the ignition furnace controller. Verify that the correct mass has been entered.

   CAUTION: Operator should wear safety equipment – high temperature gloves, face shield, fire-retardant shop coat – when opening the door to load or unload the sample.

8. Open the chamber door and gently set the sample basket assembly in the furnace. Carefully position the sample basket assembly so it is not in contact with the furnace wall**.** Close the chamber door and verify that the sample mass displayed on the furnace scale equals the total mass of the sample and sample basket assembly recorded in Step 5 within ±5 g.

   Note 5: Furnace temperature will drop below the set point when the door is opened, but will recover when the door is closed and ignition begins. Sample ignition typically increases the temperature well above the set point – relative to sample size and binder content.

9. Initiate the test by pressing the start button. This will lock the sample chamber and start the combustion blower.

   Safety note: Do not attempt to open the furnace door until the asphalt binder has been completely burned off.

10. Allow the test to continue until the stable light and audible stable indicator indicate that the change in mass does not exceed 0.01 % for three consecutive minutes. Press the stop button. This will unlock the sample chamber and cause the printer to print out the test results.

    Note 6: An ending mass loss percentage of 0.02 may be used, if allowed by the agency, when aggregate that exhibits an excessive amount of loss during ignition testing is used.

11. Open the chamber door, remove the sample basket assembly, and place on the cooling plate or block. Place the protective cage over the sample basket assembly and allow it to cool to room temperature (approximately 30 minutes).
12. Determine and record the total after ignition mass to the nearest 0.1 g. Calculate and record the mass of the sample, after ignition (total after ignition mass minus the mass of the sample basket assembly) to the nearest 0.1 g. Designate this mass as M_f.

13. Use the asphalt binder content percentage from the printed ticket. If the sample was not oven dried and a moisture content percentage has been determined, subtract the moisture content from the printed ticket asphalt binder content and report the difference as the corrected asphalt binder content.

$P_b = BC - M - C_f$ (if not input in the furnace controller)

where:

P_b = the corrected asphalt binder content as a percent by mass of the HMA

BC = asphalt binder content shown on printed ticket

M = percent moisture content as determined by the FOP for AASHTO T 329

C_f = correction factor as a percent by mass of the HMA sample

14. Asphalt binder content percentage can also be calculated using the formula from "Method B" Step 16.

Procedure – Method B (External Balance)

1. Preheat the ignition furnace to 538°C (1000°F) or to the temperature determined in the "Correction Factor" section Step 9. Manually record the furnace temperature (set point) prior to the initiation of the test if the furnace does not record automatically.
2. Dry the sample to constant mass, according to the FOP for AASHTO T 329; or determine the moisture content of a companion sample in accordance with the FOP for AASHTO T 329.
3. Determine and record the mass to the nearest 0.1 g of the sample basket assembly.
4. Place the sample basket(s) in the catch pan. Evenly distribute the sample in the sample basket(s), taking care to keep the material away from the edges of the basket. Use a spatula or trowel to level the sample.
5. Determine and record the total mass to the nearest 0.1 g of the sample and sample basket assembly. Calculate and record the initial mass of the sample (total mass minus the mass of the sample basket assembly) to the nearest 0.1 g. Designate this mass as (M_i).
6. Record the correction factor for the specific HMA.
7. Open the chamber door and gently set the sample basket assembly in the furnace. Carefully position the sample basket assembly so it is not in contact with the furnace wall. Burn the HMA sample in the furnace for 45 minutes or the length of time determined in "Correction Factor" section.
8. Open the chamber door, remove the sample basket assembly, and place on the cooling plate or block. Place the protective cage over the sample and allow it to cool to room temperature (approximately 30 min).
9. Determine and record the total after ignition mass to the nearest 0.1 g. Calculate and record the mass of the sample, after ignition (total after ignition mass minus the mass of the sample basket assembly) to the nearest 0.1 g.
10. Place the sample basket assembly back into the furnace.
11. Burn the sample for at least 15 minutes after the furnace reaches the set temperature.

12. Open the chamber door, remove the sample basket assembly, and place on the cooling plate or block. Place the protective cage over the sample basket assembly and allow it to cool to room temperature (approximately 30 min).
13. Determine and record the total after ignition mass to the nearest 0.1 g. Calculate and record the mass of the sample, after ignition (total after ignition mass minus the mass of the sample basket assembly) to the nearest 0.1 g.
14. Repeat Steps 10 through 13 until the change in measured mass, of the sample after ignition, does not exceed 0.01 percent of the previous sample mass, after ignition.

Note 7: An ending mass loss percentage of 0.02 may be used, if allowed by the agency, when aggregate that exhibits an excessive amount of loss during ignition testing is used.

15. Record the final value obtained as M_f, the final mass of the sample after ignition.
16. Calculate the asphalt binder content of the sample as follows:

$$P_b = \left[\frac{M_i - M_f}{M_i}\right] \times 100 - C_f - M$$

where:

P_b = the corrected asphalt binder content as a percent by mass of the HMA sample
M_f = the final mass of aggregate remaining after ignition
M_i = the initial mass of the HMA sample prior to ignition
C_f = correction factor as a percent by mass of the HMA sample

M= percent moisture content as determined by the FOP for AASHTO T 329.

Example

Initial Mass of Sample and Basket = 5292.7

Mass of Basket Assembly = 2931.5

$\mathbf{M_i}$ = 2361.2

Total Mass after First ignition + basket = 5154.4

Sample Mass after First ignition = 2222.9

Sample Mass after additional 15 min ignition = 2222.7

$$\frac{(2222.9 - 2222.7)}{2222.9} \times 100 = 0.009$$

not greater than 0.01% so, $\mathbf{M_f}$ = 2222.7

$$\frac{(2361.2 - 2222.7)}{2361.2} \times 100 - 0.42 - 0.04 = 5.41\%$$

$\mathbf{P_b}$= 5.41%

Gradation

1. Empty contents of the basket(s) into a flat pan, being careful to capture all material. Use a small wire brush to ensure all residual fines are removed from the baskets.

   Note 8: Particle masks are a recommended safety precaution.

2. Perform the gradation analysis in accordance with the FOP for AASHTO T 30.

Report

Results shall be reported on standard forms approved by the agency. Include:

- Method of test (A or B)
- Corrected asphalt binder content, P_b Per agency standard
- Correction factor, C_f to 0.01%
- Temperature compensation factor (if applicable)
- Total percent loss
- Sample mass
- Moisture content to 0.01 %
- Test temperature.

Attach the original printed ticket with all intermediate values (continuous tape) to the report for furnaces with internal balances.

Correction Factors

Asphalt Binder and Aggregate

Asphalt binder content results may be affected by the type of aggregate in the mixture and by the ignition furnace. Asphalt binder and aggregate correction factors must, therefore, be established by testing a set of correction specimens for each Job Mix Formula (JMF) mix design. Each ignition furnace will have its own unique correction factor determined in the location where testing will be performed.

This procedure must be performed before any acceptance testing is completed, and repeated each time there is a change in the mix ingredients or design. Any changes greater than 5% in stockpiled aggregate proportions should require a new correction factor.

All correction samples will be prepared by a central / regional laboratory unless otherwise directed.

Asphalt binder correction factor: A correction factor must be established by testing a set of correction specimens for each Job Mix Formula (JMF). Certain aggregate types may result in unusually high correction factors (> 1.0%). Such mixes should be corrected and tested at a lower temperature as described below.

Aggregate correction factor: Due to potential aggregate breakdown during the ignition process, a correction factor will need to be determined for the following conditions:

a. Aggregates that have a proven history of excessive breakdown

b. Aggregate from an unknown source.

This correction factor will be used to adjust the acceptance gradation test results obtained according to the FOP for AASHTO T 30.

Procedure

1. Obtain samples of aggregate in accordance with the FOP for AASHTO T 2.
2. Obtain samples of asphalt binder in accordance with the FOP for AASHTO T 40.

Note #9: Include other additives that may be required by the JMF.

3. Prepare an initial, or "butter," mix at the design asphalt binder content. Mix and discard the butter mix prior to mixing any of the correction specimens to ensure accurate asphalt content.
4. Prepare two correction specimens at the JMF design asphalt binder content. Aggregate used for correction specimens shall be sampled from material designated for use on the project. An agency approved method will be used to combine aggregate. An additional "blank" specimen shall be batched and tested for aggregate gradation in accordance with the FOP for AASHTO T 30. The gradation from the "blank" shall fall within the agency specified mix design tolerances.
5. Place the freshly mixed specimens directly into the sample basket assembly. If mixed specimens are allowed to cool prior to placement in the sample basket assembly, the specimens must be dried to constant mass according to the FOP for AASHTO T 329. Do not preheat the sample basket assembly.
6. Test the specimens in accordance with Method A or Method B of the procedure.
7. Once both of the correction specimens have been burned, determine the asphalt binder content for each specimen by calculation or from the printed oven tickets, if available.

8. If the difference between the asphalt binder contents of the two specimens exceeds 0.15%, repeat with two more specimens and, from the four results, discard the high and low result. Determine the correction factor from the two original or remaining results, as appropriate. Calculate the difference between the actual and measured asphalt binder contents for each specimen. The asphalt binder correction factor, C_f, is the average of the differences expressed as a percent by mass of HMA.
9. If the asphalt binder correction factor exceeds 1.0%, the test temperature must be lowered to 482 ±5°C (900 ±8°F) and new samples must be burned.

***Note 10**:* The temperature for determining the asphalt binder content of HMA samples by this procedure shall be the same temperature determined for the correction samples.

10. Perform a gradation analysis on the residual aggregate in accordance with the FOP for AASHTO T 30, if required. The results will be utilized in developing an "Aggregate Correction Factor" and should be calculated and reported to 0.1% except for the percent for the 75 µm (No. 200) sieve, which shall be calculated to the nearest 0.01%.
11. From the gradation results subtract the % passing for each sieve, for each sample, from the % passing each sieve of the "Blank" specimen gradation results from Step 4.
12. Determine the average difference of the two values. If the difference for any single sieve exceeds the allowable difference of that sieve as listed in Table 2, then aggregate gradation correction factors (equal to the resultant average differences) for all sieves shall be applied to all acceptance gradation test results determined by the FOP for AASHTO T 30. If the 75 µm (No. 200) is the only sieve outside the limits in Table 2, apply the aggregate correction factor to only the 75 µm (No. 200) sieve.

Table 2
Permitted Sieving Difference

Sieve	Allowable Difference
Sizes larger than or equal to 2.36 mm (No.8)	± 5.0%
Sizes larger than to 75 µm (No.200) and smaller than 2.36 mm (No.8)	± 3.0%
Sizes 75 µm (No.200) and smaller	± 0.50%

Examples:

Sieve Size mm (in.)	Correction factor Blank sample % Passing	Correction factor sample #1 % Passing	Correction factor sample #2 % Passing	Difference 1 / 2	Ave. Diff.	Sieves to adjust
19.0 (3/4)	100	100	100	0/0	0.0	
12.5 (1/2)	86.3	87.4	86.4	-1.1/-0.1	-0.6	
9.5 (3/8)	77.4	76.5	78.8	+0.9/-1.4	-0.5	
4.75 (No. 4)	51.5	53.6	55.9	-2.1/-4.4	-3.2	
2.36 (No. 8)	34.7	36.1	37.2	-1.4/-2.5	-2.0	
01.18 (No. 16)	23.3	25.0	23.9	-1.7/-0.6	-1.2	
0.600 (No. 30)	16.4	19.2	18.1	-2.8/-1.7	-2.2	
0.300 (No. 50)	12.0	11.1	12.7	+0.9/-0.7	+0.1	
0.150 (No. 100)	8.1	9.9	6.3	-1.8/+1.8	0.0	
75 µm (No. 200)	5.53	6.05	6.21	-0.52/-0.68	-0.60	- 0.60

In this example all acceptance gradation test results (FOP for AASHTO T 30) performed on the residual aggregate would have an "Aggregate Correction Factor". This factor would be - 0.60% on the 75 µm (No. 200) sieve and would be applied to the % passing 75 µm (No.200) sieve.

Sieve Size mm (in.)	Correction factor Blank sample % Passing	Correction factor sample #1 % Passing	Correction factor sample #2 % Passing	Difference 1 / 2	Ave. Diff.	Sieves to adjust
19.0 (3/4)	100	100	100	0/0	0.0	0.0
12.5 (1/2)	86.3	87.4	86.4	-1.1/-0.1	-0.6	-0.6
9.5 (3/8)	77.4	76.5	78.8	+0.9/-1.4	-0.5	-0.5
4.75 (No. 4)	51.5	55.6	57.9	-4.1/-6.4	-5.2	**-5.2**
2.36 (No. 8)	34.7	36.1	37.2	-1.4/-2.5	-2.0	-2.0
01.18 (No. 16)	23.3	25.0	23.9	-1.7/-0.6	-1.2	-1.2
0.600 (No. 30)	16.4	19.2	18.1	-2.8/-1.7	-2.2	-2.2
0.300 (No. 50)	12.0	11.1	12.7	+0.9/-0.7	+0.1	+0.1
0.150 (No. 100)	8.1	9.9	6.3	-1.8/+1.8	0.0	0.0
75 µm (No. 200)	5.53	6.05	6.21	-0.52/-0.68	-0.60	-0.60

In this example all acceptance gradation test results (FOP for AASHTO T 30) performed on the residual aggregate would have an "Aggregate Correction Factor". The correction factor for each sieve must be applied because the average difference on the 4.75mm (No. 4) is outside the tolerance from Table 2.

Addendum WAQTC FOP for AASHTO T 308

Following are guidelines for the use of WAQTC FOP for AASHTO T 308 by the State of Alaska DOT&PF.

1. Delete Step 9 in Calibration.
2. Oil content shall be calculated with masses determined on an external balance. This applies to all test samples as well as calibration samples.
3. Determine M_f approximately 30 minutes after removing from oven. M_f shall be determined no later then 3 hours after removal from oven.

MOISTURE CONTENT OF HOT MIX ASPHALT (HMA) BY OVEN METHOD
FOP FOR AASHTO T 329 (See Addendum for DOT&PF Guidelines)

Scope

This procedure covers the determination of moisture content of HMA in accordance with AASHTO T 329.

Background on Test Method

A test sample of HMA is dried in an oven. The moisture content is calculated by one of two methods depending upon agency standards.

- When asphalt binder content is reported as a percent of the initial mass of HMA, moisture content is reported as a percent of the initial, moist mass of mix.
- When asphalt binder content is reported as a percent of the mass of aggregate, moisture content is reported as a percent of the final, dry mass of mix.

Apparatus

- Balance or scale: 2 kg capacity, readable to 0.1 g conforming to AASHTO M 231.
- Forced Draft, Ventilated, or Convection Oven: Capable of maintaining the temperature surrounding the sample at 163 ±14°C (325 ±25°F).
- Sample Container: Clean, dry, not affected by heat and of sufficient size to contain a test sample without danger of spilling.
- Thermometer or other suitable device with a temperature range of 10-260°C (50-500°F).

Sample

The test sample shall be obtained in accordance with AASHTO T 168, and reduced in accordance with WAQTC TM 5. The size of the test sample shall be a minimum of 1000 g.

Procedure

1. Set the oven to a minimum of 105°C (221°F) but in no case should the Job Mix Formula (JMF) mixing temperature be exceeded.
2. Determine and record the mass of the sample container including release media to the nearest 0.1 g.
3. Place the test sample in the sample container.
4. Determine and record the temperature of the test sample.
5. Determine and record the total mass of the sample container and test sample to the nearest 0.1 g.
6. Calculate the initial, moist mass (M_i) of the test sample by subtracting the mass of the sample container determined in Step 2 from total mass of the sample container and the test sample determined in Step 5.
7. Dry the test sample to a constant mass in the sample container.

Note 1: Constant mass shall be defined as the mass at which further drying does not alter the mass by more than 0.05 percent. The sample shall be initially dried 90 minutes, and its mass determined at that time and at 30-minute intervals after that until a constant mass is reached.

8. Cool the sample container and test sample to ±7°C (15°F)of the temperature determined in Step 4.
9. Determine and record the total mass of the sample container and test sample to the nearest 0.1 g.

Note 2: Do not attempt to remove the test sample from the sample container for the purposes of determining mass.

10. Calculate the final, dry mass (M_f) of the test sample by subtracting the mass of the sample container determined in Step 2 from the total mass of the sample container and the test sample determined in Step 9.

Note 3: Moisture content and the number of samples in the oven will affect the rate of drying at any given time. Placing wet samples in the oven with nearly dry samples could affect the drying process.

Calculations

Constant Mass:

Calculate constant mass using the following formula:

$$\%Change = \frac{M_p - M_n}{M_p} \times 100$$

Where: M_p = previous mass measurement
M_n = new mass measurement

Example:

Mass of container: 232.6 g

Mass of container after first drying cycle: 1361.8 g

Mass, M_p, of possibly dry sample: 1361.8 g – 232.6 g = 1129.2 g

Mass of container and dry sample after second drying cycle: 1360.4 g
Mass, M_n, of dry sample: 1360.4 g – 232.6 g = 1127.8 g

$$0.12\% = \frac{1129.2 - 1127.8}{1129.2} \times 100$$

0.12% is not less than 0.05% so continue drying

Mass of container and dry sample after third drying cycle: 1359.9 g
Mass, M_n, of dry sample: 1359.9g – 232.6g = 1127.3g

$$0.04\% = \frac{1127.8 - 1127.3}{1127.8} \times 100$$

0.04% is less than 0.05% constant mass has been reached

This mass becomes the Dry mass (M_f) for calculating the moisture content.

Moisture Content:

Calculate the moisture content, as a percent, using one of the following two formulas.

Percent of Initial, Moist Mass:

$$\text{Moisture Content} = \frac{M_i - M_f}{M_i} \times 100$$

Where: M_i = initial, moist mass
M_f = final, dry mass

Example:

M_i = 1134.9 g
M_f = 1127.3 g

$$\text{Moisture Content} = \frac{1134.9\,\text{g} - 1127.3\,\text{g}}{1134.9\,\text{g}} \times 100 = 0.670, \textit{ say } 0.67\%$$

Percent of Final, Dry Mass:

$$\text{Moisture Content} = \frac{M_i - M_f}{M_f} \times 100$$

Where: M_i = initial, moist mass
M_f = final, dry mass

Example:

M_i = 1134.9 g
M_f = 1127.3 g

$$\text{Moisture Content} = \frac{1134.9\,\text{g} - 1127.3\,\text{g}}{1127.3\,\text{g}} \times 100 = 0.674, \textit{ say } 0.67\%$$

Report

Results shall be reported on standard forms approved for use by the agency. Report the moisture content to 0.01 percent.

Addendum WAQTC FOP for AASHTO T 329

Following are guidelines for the use of WAQTC FOP for AASHTO T 329 by the State of Alaska DOT&PF.

1. When determining constant mass, the initial drying time is 90 minutes minimum.

MECHANICAL ANALYSIS OF EXTRACTED AGGREGATE
FOP FOR AASHTO T 30 (See Addendum for DOT&PF Guidelines)

Scope

This procedure covers mechanical analysis of aggregate recovered from bituminous mix samples in accordance with AASHTO T 30. This FOP utilizes the aggregate recovered from the ignition oven used in AASHTO T 308. AASHTO T 30 was developed for analysis of extracted aggregate and, thus, includes references to extracted bitumen and filter element, which do not apply in this FOP.

Sieve analyses determine the gradation or distribution of aggregate particles within a given sample in order to determine compliance with design and production standards.

Apparatus

- Balance or scale: capacity sufficient for the sample mass, accurate to 0.1 percent of the sample mass or readable to 0.1 g
- Sieves
- Mechanical sieve shaker
- Suitable drying equipment (see FOP for AASHTO T 255)
- Containers and utensils – a pan or vessel of a size sufficient to contain the sample covered with water and to permit vigorous agitation without loss of any part of the sample or water

Sample Sieving

In all procedures it is required to shake the sample over nested sieves. Sieves are selected to furnish information required by specification. The sieves are nested in order of decreasing size from the top to the bottom and the sample, or a portion of the sample, is placed on the top sieve.

Sieves are shaken in a mechanical shaker for approximately 10 minutes, or the minimum time determined to provide complete separation for the sieve shaker being used.

Time Evaluation

The minimum time requirement should be evaluated for each shaker at least annually, by the following method: Continue shaking for a sufficient period and in such a manner that, after completion, not more than 0.5 percent by mass of the total sample passes any sieve during one minute of continuous hand sieving.

Provide a snug-fitting pan and cover, and hold in a slightly inclined position in one hand. Strike the side of the sieve sharply and with an upward motion against the heel of the other hand at the rate of about 150 times per minute, turning the sieve about one sixth of a revolution at intervals of about 25 strokes. In determining sufficiency of sieving for sizes larger than 4.75 mm (No. 4), limit the material on the sieve to a single layer of particles.

Overload Determination

Additional sieves may be necessary to keep from overloading the specified sieves. The sample may also be sieved in increments. For sieves with openings smaller than 4.75 mm (No. 4), the mass retained on any sieve shall not exceed 7 kg/m^2 (4 g/in^2) of sieving surface. For sieves with openings 4.75 mm (No. 4) and larger, the mass, in kg shall not exceed the product of 2.5 x (sieve opening in mm) x (effective sieving area). See Table 1.

Table 1
Maximum Allowable Mass of Material Retained on a Sieve, g
Nominal Sieve Size, mm (in.)
exact size is smaller see AASHTO T 27

Sieve Size mm (in.)		203 ϕ (8)	305 ϕ (12)	305 x 305 (12 x 12)	350 x 350 (14 x 14)	372 x 580 (16 x 24)
		Sieving Area m^2				
		0.0285	0.0670	0.0929	0.1225	0.2158
90	(3 1/2)	*	15,100	20,900	27,600	48,500
75	(3)	*	12,600	17,400	23,000	40,500
63	(2 1/2)	*	10,600	14,600	19,300	34,000
50	(2)	3600	8400	11,600	15,300	27,000
37.5	(1 1/2)	2700	6300	8700	11,500	20,200
25.0	(1)	1800	4200	5800	7700	13,500
19.0	(3/4)	1400	3200	4400	5800	10,200
16.0	(5/8)	1100	2700	3700	4900	8600
12.5	(1/2)	8900	2100	2900	3800	6700
9.5	(3/8)	6700	1600	2200	2900	5100
6.3	(1/4)	4400	1100	1500	1900	3400
4.75	(No. 4)	3300	8000	1100	1500	2600
-4.75	(-No. 4)	2000	4700	6500	1200	1300

Procedure

1. Using the aggregate sample obtained from the FOP for AAASHTO T 308, determine and record the mass of the sample. This mass shall agree with the mass of the aggregate remaining after ignition (M_f from T 308 within 0.1% of M).
2. Nest a sieve, such as a 2.0mm (No. 10), above the 75µm (No. 200) sieve.
3. Place the test sample in a container and add sufficient water to cover it. Add a detergent, dispersing agent, or other wetting solution to the water to assure a thorough separation of the material finer than the 75µm (No. 200) sieve from the coarser particles. There should be enough wetting agent to produce a small amount of suds when the sample is agitated. Excessive suds may overflow the sieves and carry material away with them.
4. Agitate vigorously to ensure complete separation of the material finer than 75µm (No. 200) from coarser particles and bring the fine material into suspension above the coarser material.
5. Immediately pour the wash water containing the suspended and dissolved solids over the nested sieves, being careful not to pour out the coarser particles.

6. Add a second change of water to the sample remaining in the container, agitate, and repeat Step 5. Repeat the operation until the wash water is reasonably clear. Continue washing until the agent is removed.
7. Rinse the material retained on the 0.75 mm (No.200) sieve until water passing through the sieve is reasonably clear.
8. Remove the upper sieve and rinse the material retained on the 0.75 mm (No.200) sieve until water passing through the sieve is reasonably clear.
9. Return all material retained on the nested sieves to the container by flushing into the washed sample.
10. Dry the washed aggregate to constant mass in accordance with the FOP for AASHTO T 255, and then cool prior to sieving. Record the "dry mass after washing".
11. Select sieves to furnish information required by the specifications. Nest the sieves in order of decreasing size from top to bottom and place the sample, or a portion of the sample, on the top sieve.
12. Place sieves in mechanical shaker and shake for the minimum time determined to provide complete separation for the sieve shaker being used, approximately 10 minutes.

Note 1: Excessive shaking (more than 10 minutes) may result in degradation of the sample.

13. Determine the mass retained on each sieve to the nearest 0.1 g. Ensure that all material trapped in the openings of the sieves are cleaned out and included in the mass retained.

Note 2: Use coarse wire brushes to clean the 600 µm (No. 30) and larger sieves, and soft bristle brushes for smaller sieves.

Calculation

1. The total mass of the material after sieving should check closely with the original mass of sample placed on the sieves (dry mass after washing). When the masses before and after sieving differ by more than 0.2 percent do not use the results for acceptance purposes.
2. Divide the masses in the individual sieves by the total dry mass before washing and multiply by 100 to determine the percent retained on and passing each sieve. Calculate the percent retained and passing each sieve to the nearest 0.1% except for the percent passing the 75 µm (No. 200) sieve, which shall be calculated to the nearest 0.01%.
3. Apply the Aggregate Correction Factor to the calculated percent passing, as required in the FOP for AASHTO T 308 "Correction Factor" Steps 10 through 12, to obtain the reported percent passing. Report percentages to the nearest 1% except for the percent passing the 75 µm (No. 200) sieve, which shall be reported to the nearest 0.1%.

    Example:

    Dry mass of total sample, before washing: 2422.3 g

    Dry mass of sample, after washing out the 75 µm (No. 200) minus: 2296.2

    Amount of 75 µm (No. 200) minus washed out: 2422.3 g – 2296.2g = 126.1 g

Gradation on All Screens

Sieve Size mm (in.)	Mass Retained g	Percent Retained	Cumulative Mass Retained g	Cum. Percent Retained	Calc'd Percent Passing	Agg. Corr. Factor From T-308	Reported Percent Passing
19.0 (3/4)	0.0		0.0	0	100.0		100
12.5 (1/2)	346.9	14.3	346.9	14.3	85.7		86
9.5 (3/8)	207.8	8.6	554.7	22.9	77.1		77
4.75 (No. 4)	625.4	25.8	1180.1	48.7	51.3		51
2.36 (No. 8)	416.2	17.2	1596.3	65.9	34.1		34
01.18 (No. 16)	274.2	11.3	1870.5	77.2	22.8		23
0.600 (No. 30)	152.1	6.3	2022.6	83.5	16.5		16
0.300 (No. 50)	107.1	4.4	2129.7	87.9	12.1		12
0.150 (No. 100)	96.4	4.0	2226.1	91.9	8.1		8
0.075 (No. 200)	63.5	2.59	2289.6	94.51	5.49	-0.60	4.9
Pan	5.7		2295.3				

Check sum: 2296.2 –2295.3 / 2296.2 X 100 = 0.04 % which is reported as 0.0% and is within the 0.2 percent requirement

Report

Results shall be reported on standard forms approved for use by the agency. Depending on the agency, this may include:

- Mass retained on each sieve
- Percent retained on each sieve
- Cumulative mass retained on each sieve
- Cumulative percent retained on each sieve
- Calculated Percent passing each sieve to 0.1%
- Aggregate Correction Factor for each sieve from AASHTO T 308
- Reported Percent passing

Report percentages to the nearest 1 percent except for the percent passing the 75 µm (No. 200) sieve, which shall be reported to the nearest 0.1 percent.

Addendum WAQTC FOP for AASHTO T 30

Following are guidelines for the use of WAQTC FOP for AASHTO T 30 by the State of Alaska DOT&PF.

1. Calculate the minus 0.075 mm (No. 200) by dividing the sum of the loss from washing plus the mass of the material in the pan by the initial sample weight.

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THEORETICAL MAXIMUM SPECIFIC GRAVITY AND DENSITY OF BITUMINOUS PAVING MIXTURES (See Addendum for DOT&PF Guidelines)
FOP FOR AASHTO T 209

Scope

This procedure covers the determination of the maximum specific gravity (G_{mm}) of uncompacted Hot Mix Asphalt (HMA) paving mixtures in accordance with AASHTO T 209. Two methods using two different containers – bowl and flask – are covered.

Specimens prepared in the laboratory shall be cured according to agency standards.

Apparatus

- Balance or scale: 10,000 g capacity, readable to 0.1 g
- Container: A glass, metal, or plastic bowl or volumetric flask capable of holding a 2,000 g sample and withstanding a partial vacuum
- Container cover: A glass plate or a metal or plastic cover with a vented opening.
- Vacuum Lid: A transparent lid with a suitable vacuum connection. The vacuum opening to be covered with a fine wire mesh
- Vacuum pump or water aspirator: Capable of evacuating air from the container to a residual pressure of 4.0 kPa (30 mm Hg).
- Manometer or Vacuum gauge: Traceable to NIST and capable of measuring residual pressure down to 4.0 kPa (30 mm Hg) or less.
- Water bath: A constant-temperature water bath (optional)
- Thermometers: Calibrated liquid-in-glass, or electronic digital total immersion type, accurate to 0.5°C (0.9°F)
- Bleeder valve to adjust vacuum.
- Timer

Calibration of Flask

Use a volumetric flask that is calibrated to accurately determine the mass of water, at 25 ±0.5°C (77 ±0.9°F), in the flask. The volumetric flask shall be calibrated periodically in conformance with procedures established by the agency.

Test Sample Preparation

1. Obtain samples in accordance with the FOP for AASHTO T 168 and reduce according to the FOP for WAQTC TM 5.
2. Test sample size shall conform to the requirements of Table 1. Samples larger than the capacity of the container may be tested in two or more increments. Results will be combined and averaged. If the increments have a specific gravity difference greater than 0.018 for the bowl method and 0.011 for the flask method the test must be re-run.

Table 1
Test Sample Size for G_{mm}

Size of Largest Particle of Aggregate in Mixture mm (in.)	Minimum Mass g
50.0 (2)	6000
37.5 (1 ½)	4000
25 (1)	2500
19 (3/4)	2000
12.5 (1/2)	1500
9.5 (3/8)	1000
4.75 (No. 4)	500

Procedure – General

Two procedures – bowl and flask – are covered. The first 11 steps are the same for both.

1. Separate the particles of the sample, taking care not to fracture the mineral particles, so that the particles of the fine aggregate portion are not larger than 6.3 mm (1/4 in.). If the mixture is not sufficiently soft to be separated manually, place it in a large flat pan and warm in an oven only until it is pliable enough for separation.
2. Cool the sample to room temperature.
3. Determine and record the mass of the dry bowl or flask, including the cover, to the nearest 0.1 g.
4. Place the sample in the bowl or flask.
5. Determine and record the mass of the dry bowl or flask, cover, and sample to the nearest 0.1 g.
6. Determine and record the mass of the sample by subtracting the mass determined in Step 3 from the mass determined in Step 5. Designate this mass as “A”.
7. Add sufficient water at approximately 25° ±1°C (77° ±1.8°F) to cover the sample by about 25 mm (1 in.).

   Note 1: The release of entrapped air may be facilitated by the addition of a wetting agent. Check with the agency to see if this is permitted and, if it is, for a recommended agent.

8. Place the lid on the bowl or flask and attach the vacuum line. To ensure a proper seal between the flask and the lid, wet the O-ring or use a petroleum gel.
9. Remove entrapped air by subjecting the contents to a partial vacuum of 3.7 ±0.3 kPa (27.5 ±2.5 mm Hg) residual pressure for 15 ±2 minutes.
10. Agitate the container and contents, either continuously by mechanical device or manually by vigorous shaking, at 2-minute intervals. This agitation facilitates the removal of air.
11. Slowly open the release valve, turn off the vacuum pump and remove the lid.

Procedure – Bowl

12A. Suspend and immerse the bowl and contents in water at 25 ±1.0°C (77 ±1.8°F) for 10 ±1 minutes. The holder shall be immersed sufficiently to cover it and the bowl.

13A. Determine and record the submerged weight of the bowl and contents to the nearest 0.1 g.

14A. Empty and re-submerge the bowl following step 12A to determine the submerged weight of the bowl to the nearest 0.1 g.

15A. Determine and record the submerged weight of the sample the nearest 0.1 g by subtracting the submerged weight of the bowl from the submerged weight determined in Step 13A. Designate this submerged weight as "C".

Procedure – Flask

> ***Note 2:*** Stabilize the temperature of the flask and contents to 25 ±1°C (77 ±1.8°F) and determine final mass of the flask, cover, de-aired water, and sample within 10 ±1 minutes of completing Step 11.

12B. Fill the flask with water and adjust the temperature to 25 ±1°C (77 ±1.8°F).

13B. Stabilize the temperature of the flask and contents in a water bath so that final temperature is within 25 ±1°C (77 ±1.8°F).

> ***Note 3:*** In lieu of placing the flask in the water bath, determine the temperature of the water in the flask and make the appropriate density correction using Table 2 when the temperature is outside 25 ±1°C (77 ±1.8°F).

14B. Finish filling the flask, place the cover or a glass plate on the flask, and eliminate all air from the flask.

> ***Note 4:*** When using the metal flask and cover, place the cover on the flask and push down slowly, forcing excess water out of the hole in the center of the cover. Use care when filling flask to avoid reintroducing air into the water.

15B. Towel dry the outside of the flask and cover.

16B. Determine and record the mass of the flask, cover, de-aired water, and sample to the nearest 0.1 g. within 10 ±1 minutes of completion of Step 11. Designate this mass as "E".

17B. Mass "D", the mass of the flask and water, is determined during the Calibration of Flask procedure.

Procedure – Mixtures Containing Uncoated Porous Aggregate

If the pores of the aggregates are not thoroughly sealed by a bituminous film, they may become saturated with water during the vacuuming procedure, resulting in an error in maximum density. To determine if this has occurred, complete the general procedure and then:

1. Drain water from sample through a towel held over top of container to prevent loss of material.
2. Spread sample before an electric fan to remove surface moisture.
3. Determine the mass of the sample when the surface moisture appears to be gone.
4. Continue drying and determine the mass of the sample at 15-minute intervals until less than a 0.5 g loss is found between determinations.
5. Record the mass as the saturated surface-dry mass to the nearest 0.1 g. Designate this mass as "A_{SSD}".

6. Calculate, as indicated below, G_{mm}, using "A" and "A_{SSD}", and compare the two values.

Calculation

Calculate the G_{mm} to three decimal places as follows.

Bowl Procedure

$$G_{mm} = \frac{A}{A - C}$$

where:

A = mass of dry sample in air, g
C = submerged weight of sample in water, g

Example:

A = 1432.7 g
C = 848.6 g

$$G_{mm} = \frac{1432.7\,g}{1432.7\,g - 848.6\,g} = 2.453$$

Flask Procedure

$$G_{mm} = \frac{A}{A + D - E} \times R$$

or

$$G_{mm} = \frac{A}{A_{SSD} + D - E} \times R$$

(for mixtures containing uncoated aggregate materials)

where:

A = Mass of dry sample in air, g
A_{SSD} = Mass of saturated surface-dry sample in air, g
D = Mass of flask filled with water at 25°C (77°F), g
E = Mass of flask filled with water and the test sample at test temperature, g
R = Factor from Table 2 to correct the density of water – use when a test temperature is outside 25 ±1°C (77 ±1.8°F).

Example (in which two increments are averaged):

Test 1	Test 2
A = 1200.3 g	A = 960.2 g
D = 7502.5 g	D = 7525.5 g
E = 8217.1 g	E = 8096.3 g
Temperature = 26.2°C	Temperature = 25.0°C

$$G_{mm_1} = \frac{1200.3 \text{ g}}{1200.3 \text{ g} + 7502.5 \text{ g} - 8217.1 \text{ g}} \times 0.99968 = 2.470$$

$$G_{mm_2} = \frac{960.2 \text{ g}}{960.2 \text{ g} + 7525.5 \text{ g} - 8096.3 \text{ g}} \times 1.00000 = 2.466$$

Average

2.470 - 2.466 = 0.004 which is < 0.011 so they can be averaged.

Average

2.470 - 2.466 = 0.004   0.004 ÷ 2 = 0.002   0.002 + 2.466 = **2.468**

Or 2.470 + 2.466 = 4.936   4.936 ÷ 2 = 2.468

Table 2
Temperature Correction Factor

°C	°F	"R"		°C	°F	"R"
20.0	68.0	1.00117		23.3	74.9	1.00042
20.1	68.2	1.00114		23.4	74.1	1.00040
20.2	68.4	1.00112		23.5	74.3	1.00037
20.3	68.5	1.00110		23.6	74.5	1.00035
20.4	68.7	1.00108		23.7	74.7	1.00033
20.5	68.9	1.00106		23.8	74.8	1.00030
20.6	69.1	1.00104		23.9	75.0	1.00028
20.7	69.3	1.00102		24.0	75.2	1.00025
20.8	69.4	1.00100		24.1	75.4	1.00023
20.9	69.6	1.00097		24.2	75.6	1.00020
21.0	69.8	1.00095		24.3	75.7	1.00018
21.1	70.0	1.00093		24.4	75.9	1.00015
21.2	70.2	1.00091		24.5	76.1	1.00013
21.3	70.3	1.00089		24.6	76.3	1.00010
21.4	70.5	1.00086		24.7	76.5	1.00007
21.5	70.7	1.00084		24.8	76.6	1.00005
21.6	70.9	1.00082		24.9	76.8	1.00002
21.7	71.1	1.00080		25.0	77.0	1.00000
21.8	71.2	1.00077		25.1	77.2	0.99997
21.9	71.4	1.00075		25.2	77.4	0.99995
22.0	71.6	1.00073		25.3	77.5	0.99992
22.1	71.8	1.00030		25.4	77.7	0.99989
22.2	72.0	1.00068		25.5	77.9	0.99987
22.3	72.1	1.00066		25.6	78.1	0.99984
22.4	72.3	1.00064		25.7	78.3	0.99981
22.5	72.5	1.00061		25.8	78.4	0.99979
22.6	72.7	1.00059		25.9	78.6	0.99976
22.7	72.9	1.00057		26.0	78.8	0.99973
22.8	73.0	1.00054		26.1	79.0	0.99971
22.9	73.2	1.00052		26.2	79.2	0.99968
23.0	73.4	1.00050		26.3	79.3	0.99965
23.1	73.6	1.00047		26.4	79.5	0.99963
23.2	73.8	1.00045		26.5	79.7	0.99960

Theoretical Maximum Density

To calculate the theoretical maximum density at 25°C (77°F) use one of the following formulas. The density of water at 25°C (77°F) = 997.1 in Metric units or 62.245 in English units.

Theoretical maximum density kg/m^3 = G_{mm} x 997.1 kg/ m^3

2.468 x 997.1 kg/ m^3 = 2461 kg/ m^3

or

Theoretical maximum density lb/ft^3 = G_{mm} x 62.245 lb/ft^3

2.468 x 62.245 lb/ft^3 = 153.6 lb/ft^3

Report

Results shall be reported on standard forms approved for use by the agency. Report G_{mm} to three decimal places. Report the theoretical maximum density to1 kg/m^3 (0.1 lb/ft^3).

Addendum WAQTC FOP for AASHTO T 209

Following are guidelines for the use of WAQTC FOP for AASHTO T 209 by the State of Alaska DOT&PF.

1. The flask method is to be used in all Theoretical Maximum Specific Gravity determinations.

BULK SPECIFIC GRAVITY OF COMPACTED BITUMINOUS MIXTURES USING SATURATED SURFACE-DRY SPECIMENS (See Addendum for DOT&PF Guidelines)
FOP FOR AASHTO T 166

BULK SPECIFIC GRAVITY OF COMPACTED BITUMINOUS MIXTURES USING PARAFFIN-COATED SPECIMENS
FOP FOR AASHTO T 275

Scope

This procedure covers the determination of bulk specific gravity (G_{mb}) of compacted Hot Mix Asphalt (HMA) using three methods – A, B, and C – in accordance with AASHTO T 166. These three methods are for use on specimens not having open or inter-connecting voids and/or absorbing more than 2.0 percent water by volume. A fourth and fifth method – D & E – in accordance with AASHTO T 275 and covering specimens having open or interconnecting voids and/or absorbing more than 2.0 percent water by volume is also included.

Overview

- Method A Suspension
- Method B Volumeter
- Method C Rapid test for A or B

- Method D Suspension for coated specimen
- Method E Volumeter for coated specimen

Test Specimens

Test specimens may be either laboratory-molded or from HMA pavement. For specimens it is recommended that the diameter be equal to four times the maximum size of the aggregate and the thickness be at least one and one half times the maximum size.

Apparatus – Method A (Suspension)

- Balance or scale: 5 kg capacity, readable to 0.1 g, fitted with a suitable suspension apparatus and holder to permit weighing the specimen while suspended in water and conforming to AASHTO M 231.
- Suspension apparatus: Wire of the smallest practical size and constructed to permit the container to be fully immersed.
- Water bath: For immersing the specimen in water while suspended under the balance or scale, and equipped with an overflow outlet for maintaining a constant water level.
- Towel: Damp towel used for surface drying specimens.
- Oven: Capable of maintaining a temperature of 110 ±5°C (230 ±9°F) for drying the specimens to a constant mass.

> ***Note 1:*** AASHTO T 166 defines constant mass as the mass that further drying at 52 ±3°C (125 ±5°F) does not alter the mass by more than 0.05 percent. It also states that samples shall initially be dried overnight and that mass determinations shall be made at 2-hour drying intervals. AASHTO T 166 also states that recently molded laboratory samples that have not been exposed to moisture do not need drying.

- Pan: Pan or other suitable container of known mass, large enough to hold a sample for drying in oven.
- Thermometer: Having a range of 19 to27° C(66 to 80°F), graduated in 0.1° C(0.2°F) subdivisions.

Procedure - Method A (Suspension)

1. Dry the specimen to constant mass, if required. See note #1.

   Note 2: To expedite the procedure steps 1 and 2 may be performed last. To further expedite the process see Method C.

2. Cool the specimen in air to 25 ±5°C (77±9°F), and determine and record the dry mass to the nearest 0.1 g. Designate this mass as "A".
3. Fill the water bath to overflow level with water at 25 ±1°C (77 ±1.8°F).
4. Immerse the specimen for 4 ±1 minutes.
5. Determine and record the submerged weight to the nearest 0.1 g. Designate this submerged weight as "C".
6. Remove the sample from the water and quickly (not to exceed 5 seconds) surface dry with a damp towel.
7. Determine and record the mass of the SSD specimen to nearest 0.1 g. Designate this mass as "B". Any water that seeps from the specimen during the mass determination is considered part of the saturated specimen.

Calculations - Method A (Suspension)

$$G_{mb} = \frac{A}{B - C}$$

where:

A = Mass of dry specimen in air, g

B = Mass of SSD specimen in air, g

C = Weight of specimen in water at 25 ±1°C (77 ±1.8°F), g

$$\text{Percent Water Absorbed (by volume)} = \frac{B - A}{B - C} \times 100$$

Apparatus – Method B (Volumeter)

- Balance or scale: 5 kg capacity, readable to 0.1 g and conforming to AASHTO M 231.
- Water bath: thermostatically controlled to 25 ±0.5°C (77±0.9°F).
- Thermometer: Range of 19 to 27°C (66 to 80°F), and graduated in 0.1°C (0.2°F) subdivisions.

- Volumeter: Calibrated to 1200 mL or appropriate capacity for test sample and having a tapered lid with a capillary bore.
- Oven: Capable of maintaining a temperature of 110 ±5°C (230 ±9°F) for drying the specimens to a constant mass.
- Pan: Pan or other suitable container of known mass, large enough to hold a sample for drying in oven.
- Towel: Damp towel used for surface drying specimens.

Procedure - Method B (Volumeter)

1. Dry the specimen to constant mass, if required. See note 1.

   Note 2: To expedite the procedure steps 1 and 2 may be performed last. To further expedite the process see Method C.

2. Cool the specimen in air to 25 ±5°C (77±9°F), and determine and record the dry mass to the nearest 0.1 g. Designate this mass as "A".
3. Immerse the specimen in the temperature controlled water bath for at least 10 minutes.
4. Fill the volumeter with distilled water at 25 ±1°C (77 ±1.8°F) making sure some water escapes through the capillary bore of the tapered lid. Wipe the volumeter dry. Determine the mass of the volumeter to the nearest 0.1 g. Designate this mass as "D".
5. Remove the specimen from the water bath and quickly surface dry with a damp towel.
6. Determine and record the mass of the SSD specimen to the nearest 0.1 g. Designate this mass as "B". Any water that seeps from the specimen during the mass determination is considered part of the saturated specimen.
7. Place the specimen in the volumeter and let stand 60 seconds.
8. Bring the temperature of the water to 25 ±1°C (77 ±1.8°F), and cover the volumeter making sure some water escapes through the capillary bore of the tapered lid.
9. Wipe the volumeter dry.
10. Determine and record the mass of the volumeter and specimen to the nearest 0.1 g. Designate this mass as "E".

    Note 3: Method B is not acceptable for use with specimens that have more than 6 % air voids.

Calculations - Method B (Volumeter)

$$G_{mb} = \frac{A}{B + D - E}$$

where:

A = Mass of dry specimen in air, g

B = Mass of SSD specimen in air, g

D = Mass of volumeter filled with water at 25 ±1°C (77 ±1.8°F), g

E = Mass of volumeter filled with specimen and water, g

$$\text{Percent Water Absorbed (by volume)} = \frac{\text{B - A}}{\text{B + D − E}} \times 100$$

Apparatus - Method C (Rapid Test for Method A or B)

See Methods A or B.

Note 4: This procedure can be used for specimens not required to be saved and containing substantial amounts of moisture. Cores can be tested the same day as obtained by this method.

Procedure – Method C (Rapid Test for Method A or B)

1. Determine which method to perform, A or B. Proceed with Method A or B, except that the dry mass, A, is determined last. In method A and B, start on step 3, complete that procedure then continue as follows to determine mass "A".
2. Place the specimen on a large, flat bottom pan of known mass.
3. Heat at a minimum of 105°C (221°F), until the specimen can be easily separated to the point where the fine aggregate particles are not larger than 6.3 mm (1/4 in.). In no case should the Job Mix Formula mixing temperature be exceeded.
4. Dry to constant mass. Constant mass is defined as the mass at which further drying at the temperature in step 3 does not change by more than 0.05% after an additional 2 hour drying time.
5. Cool in air to 25 ±5°C (77 ±9°F).
6. Determine and record the mass of the pan and specimen to the nearest 0.1 g.
7. Determine and record the mass of the dry specimen to the nearest 0.1 g by subtracting the mass of the pan from the mass determined in Step 6. Designate this mass as "A".

Calculations – Method C (Rapid Test for Method A or B)

Complete the calculations as outlined in Methods A or B, as appropriate.

Materials – Method D Suspension (Coated Specimens/AASHTO T 275)

- Paraffin or parafilm: Used to coat test specimens.

Apparatus – Method D Suspension (Coated Specimens/AASHTO T 275)

- Balance or scale: 5 kg capacity, readable to 0.1 g, fitted with a suitable suspension apparatus and holder to permit weighing the specimen while suspended in water and conforming to AASHTO M 231.
- Suspension apparatus: Wire of the smallest practical size and constructed to permit the container to be fully immersed.
- Water bath: For immersing the specimen in water while suspended under the balance or scale, and equipped with an overflow outlet for maintaining a constant water level.
- Oven: Capable of maintaining a temperature of 110 ±5°C (230 ±9°F) for drying the specimens to a constant mass.
- Pan: Pan or other suitable container of known mass, large enough to hold a sample for drying in oven.

Procedure - Method D Suspension (Coated Specimens/AASHTO T 275)

1. Dry the specimen to constant mass, if required. See note 1.
2. Cool the specimen in air to 25 ±5°C (77 ±9°F), and determine and record the dry mass to the nearest 0.1 g. Designate this mass as “A”.
3. Coat specimen on all surfaces with melted paraffin, or parafilm coating, sufficiently thick to seal all voids.
4. Allow coating to cool in air at 25 ±5°C (77 ±9°F) for 30 minutes.
5. Determine and record the mass of the coated specimen to the nearest 0.1 g. Designate this mass as “D”.
6. Fill the water bath to overflow level with water at 25 ±1°C (77 ±1.8°F).
7. Immerse the specimen in water at 25 ±1°C (77 ±1.8°F) for 4 ±1 minutes.
8. Determine and record the submerged weight to the nearest 0.1 g. Designate this submerged weight as “E”.
9. Determine the specific gravity of paraffin or parafilm at 25 ±1°C (77 ±1.8°F) from the manufacturer’s literature or other suitable source. Designate this specific gravity as “F”.

Calculations - Method D Suspension (Coated Specimens/AASHTO T 275)

$$G_{mb} = \frac{A}{D - E - \left[\frac{D - A}{F}\right]}$$

where:

A = Mass of dry specimen in air, g

D = Mass of specimen with paraffin coating in air, g

E = Weight of specimen with paraffin coating in water, g

F = Specific gravity of paraffin or parafilm at 25 ±1°C (77 ±1.8°F)

Apparatus – Method E Volumeter (Coated Specimens/AASHTO T 275)

- Balance or scale: 5 kg capacity, readable to 0.1 g and conforming to AASHTO M 231.
- Water bath: thermostatically controlled to 25 ±0.5°C (77±0.9°F).
- Thermometer: Range of 19 to 27°C (66 to 80°F), and graduated in 0.1°C (0.2°F) subdivisions.
- Volumeter: Calibrated to 1200 mL or appropriate capacity for test sample and having a tapered lid with a capillary bore.
- Oven: Capable of maintaining a temperature of 110 ±5°C (230 ±9°F) for drying the specimens to a constant mass.
- Pan: Pan or other suitable container of known mass, large enough to hold a sample for drying in oven.
- Towel: Damp towel used for surface drying specimens.

Procedure - Method E Volumeter (Coated Specimens/AASHTO T 275)

1. Dry the specimen to constant mass, if required. See note 1.
2. Cool the specimen in air to 25 ±5°C (77±9°F), and determine and record the dry mass to the nearest 0.1 g. Designate this mass as "A".
3. Coat the specimen all surfaces with paraffin, or parafilm coating, sufficiently thick to seal all voids.
4. Allow coating to cool in air at 25 ±5°C (77 ±9°F) for 30 minutes.
5. Determine and record the mass of the coated specimen to the nearest 0.1g. Designate this mass as "C".
6. Fill the volumeter with distilled water at 25 ±1°C (77 ±1.8°F) and place the coated specimen in the volumeter.
7. Bring the temperature of the water to 25 ±1°C (77 ±1.8°F), and cover the volumeter making sure some water escapes through the capillary bore of the tapered lid.
8. Wipe the volumeter dry.
9. Determine and record the mass of the volumeter and specimen to the nearest 0.1 g. Designate this mass as "E".

10. Determine the specific gravity of paraffin or parafilm at 25 ±1°C (77 ±1.8°F) from the manufacturer's literature or other suitable source. Designate this specific gravity as "F".

Calculations - Method E Volumeter (Coated Specimens/AASHTO T 275)

$$G_{mb} = \frac{A}{D - \left[E - C + \left(\frac{C - A}{F}\right) \right]}$$

where:

A = Mass of dry specimen in air, g

C = Mass of specimen with paraffin coating in air, g

D = Mass of volumeter filled water at 25 ±1°C (77 ±1.8°F), g

E = Mass of volumeter filled with specimen with paraffin coating and in water25 ±1°C (77 ±1.8°F), g

F = Specific gravity of paraffin or parafilm at 25 ±1°C (77 ±1.8°F)

Report

Results shall be reported on standard forms approved for use by the agency. Report the G_{mb} to 3 decimal places and absorption to 2 decimal places. Report the method performed.

Addendum WAQTC FOP for AASHTO T 166/T 275

Following are guidelines for the use of WAQTC FOP for AASHTO T 166/T 275 by the State of Alaska DOT&PF.

1. Report compaction to the 1%. Calculate as follows:

$$C_p = \left(\frac{G_{mb}}{G_{mm}}\right) \times 100$$

   Where:
   C_p = Percent Compaction
   G_{mm} = Theoretical Maximum Specific Gravity
   G_{mb} = Bulk Specific Gravity

2. Method C/A is the only accepted method for AKDOT&PF projects, irregardless of the absorption calculated.

3. Report absorption to 0.1%.

IN-PLACE DENSITY OF BITUMINOUS MIXES USING THE NUCLEAR MOISTURE-DENSITY GAUGE (See Addendum for DOT&PF Guidelines)
FOP FOR WAQTC TM 8

Scope

This test method describes a test procedure for determining the density of bituminous mixes by means of a nuclear gauge employing either direct transmission or backscatter methods. Correlation with densities determined under the FOP for AASHTO T 166 is required by some agencies.

Apparatus

- Nuclear density gauge with the factory matched standard reference block.
- Drive pin, guide/scraper plate, and hammer for testing in direct transmission mode.
- Transport case for properly shipping and housing the gauge and tools.
- Instruction manual for the specific make and model of gauge.
- Radioactive materials information and calibration packet containing:
  - Daily Standard Count Log
  - Factory and Laboratory Calibration Data Sheet
  - Leak Test Certificate
  - Shippers Declaration for Dangerous Goods
  - Procedure Memo for Storing, Transporting and Handling Nuclear Testing Equipment
  - Other radioactive materials documentation as required by local regulatory requirements.

Material

- Filler material: Fine graded sand from the source used to produce the asphalt pavement or other agency approved materials.

Radiation Safety

This method does not purport to address all of the safety problems associated with its use. This test method involves potentially hazardous materials. The gauge utilizes radioactive materials that may be hazardous to the health of the user unless proper precautions are taken. Users of this gauge must become familiar with the applicable safety procedures and governmental regulations. All operators will be trained in radiation safety prior to operating nuclear density gauges. Some agencies require the use of personal monitoring devices such as a thermoluminescent dosimeter or film badge. Effective instructions together with routine safety procedures such as source leak tests, recording and evaluation of personal monitoring device data, etc., are a recommended part of the operation and storage of this gauge.

Calibration

Calibrate the nuclear gauge as required by the agency. This calibration may be performed by the agency using manufacturer's recommended procedures or by other facilities approved by the agency. Verify or re-establish calibration curves, tables, or equivalent coefficients every 12 months.

Standardization

1. Turn the gauge on and allow it to stabilize (approximately 10 to 20 minutes) prior to standardization. Leave the power on during the day's testing.
2. Standardize the nuclear gauge at the construction site at the start of each day's work and as often as deemed necessary by the operator or agency. Daily variations in standard count shall not exceed the daily variations established by the manufacturer of the gauge. If the daily variations are exceeded after repeating the standardization procedure, the gauge should be repaired and or recalibrated.
3. Record the standard count for both density and moisture in the Daily Standard Count Log. The exact procedure for standard count is listed in the manufacturer's Operators Manual.

***Note 1*:** New standard counts may be necessary more than once a day. See agency requirements.

Test Site Location

1. Select a test location(s) randomly and in accordance with agency requirements. Test sites should be relatively smooth and flat and meet the following conditions:
    a. At least 10 m (30 ft) away from other sources of radioactivity
    b. At least 3 m (10 ft) away from large objects
    c. If the gauge will be closer than 600 mm (24 in.) to any vertical mass, or less than 300 mm (12 in.) from a vertical pavement edge, use the gauge manufacturer's correction procedure.

Overview

There are two methods for determining in-place density of HMA. See agency requirements for method selection.

- Direct Transmission
- Backscatter

Procedure

Direct Transmission

1. Maximum contact between the base of the gauge and the surface of the material under test is critical.
2. Use the guide and scraper plate as a template and drill a hole to a depth of at least 1/4 in. (7 mm) deeper than the measurement depth required for the gauge.
3. Place the gauge on the prepared surface so the source rod can enter the hole. Insert the probe in the hole and lower the source rod to the desired test depth using the handle and trigger mechanism. Position the gauge with the long axis of the gauge parallel to the direction of paving. Pull the gauge so that the probe is firmly against the side of the hole.
4. Take two one-minute tests and record the wet density (WD) readings. If the two density readings are not within 3 lbs/ft^3 (50 kg/m^3) rotate the gauge 180 degrees and repeat the test in the same hole until they do agree.

Backscatter

1. Maintain maximum contact between the base of the gauge and the surface of the material under test. Use filler material to fill surface voids. Spread a small amount of filler material over the test site surface and distribute it evenly. Strike off the surface with a straight edge to remove excess material.
2. Place the gauge on the test site. Using a crayon, (not spray paint) mark the outline or footprint of the gauge. Extend the probe to the backscatter position.
3. Take a one-minute test and record the wet density reading.
4. Rotate the gauge 90 degrees about the probe. Mark the outline or footprint of the gauge.
5. Take another one-minute test and record the wet density reading.
6. If the difference between the two one minute tests is greater than 40 kg/m^3 (2.5 lb/ft^3), retest in both directions.

Calculation of Results

The density reported for each test site shall be the average of the two individual one-minute wet density readings.

Percent compaction is determined by comparing the in-place wet density as determined by this method to the appropriate agency density standard. See appropriate agency policy for use of density standards.

Example:

Reading #1: 141.5 lb/ft^3

Reading #2: 140.1 lb/ft^3 Are the two readings within the tolerance? (YES)

Reading Average: 140.8 lb/ft^3

Core correction : +2.1 lb/ft^3

Corrected Reading: 142.9 lb/ft^3

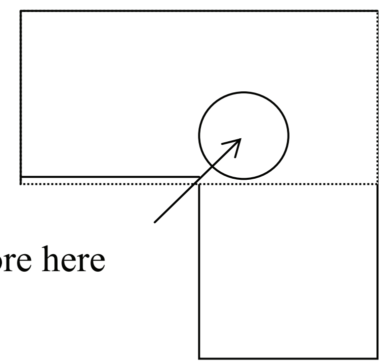
G_{mm} and Maximum Density from the FOP for AASHTO T 209: G_{mm} 2.466 153.5 lb/ft^3

$$\frac{\text{Corrected Reading}}{\text{Maximum Density}} X100 = \%\ \text{compaction} \qquad \frac{142.9}{153.5} X100 = 93.1\%$$

Correlation with Cores

Note 2: When density correlation with test method AASHTO T 166 is required, correlation of the nuclear gauge with pavement cores shall be made on the first day's paving (within 24 hours) or from a test strip constructed prior to the start of paving. Cores must be taken before traffic is allowed on the pavement.

1. Determine the number of cores required for correlation from the agency's specifications. Cores shall be located on the first day's paving or on the test strip. Locate the test sites in accordance with the agency's specifications. Follow the "Procedure" section above to establish test sites and obtain densities using the nuclear gauge.
2. Obtain a pavement core from each of the test sites. The core should be taken from the center of the nuclear gauge footprint. If direct transmission was used, locate the core at least 25 mm (1 in.) away from the edge of the drive pin hole.



3. Determine the density of the cores by AASHTO T 166, Bulk Specific Gravity of Compacted Bituminous Mixtures Using Saturated Surface-Dry Specimens.
4. Calculate a correlation factor for the nuclear gauge reading as follows.

   a. Calculate the difference between the core density and nuclear gauge density at each test site to the nearest 1 kg/m^3 (0.1 lb/ft^3). Calculate the average difference and standard deviation of the differences for the entire data set to the nearest 1 kg/m^3 (0.1 lb/ft^3).

   b. If the standard deviation of the differences is equal to or less than 40 kg/m^3 (2.5 lb/ft^3), the correlation factor applied to the nuclear density gauge reading shall be the average difference calculated above in 4.a.

   c. If the standard deviation of the differences is greater than 40 kg/m^3 (2.5 lb/ft^3), the test site with the greatest variation from the average difference shall be eliminated from the data set and the data set properties and correlation factor recalculated following 4.a and 4.b.

   d. If the standard deviation of the modified data set still exceeds the maximum specified in 4.b, additional test sites will be eliminated from the data set and the data set properties and correlation factor recalculated following 4.a and 4.b. If the data set consists of less than five test sites, additional test sites shall be established.

Note 3: The exact method used in calculating the Nuclear Gauge Correlation Factor shall be defined by agency policy.

Note 4: The above correlation procedure must be repeated if there is a new job mix formula. Adjustments to the job mix formula beyond tolerances established in the contract documents will constitute a new job mix formula. A correlation factor established using this procedure is only valid for the particular gauge and in the mode and at the probe depth used in the correlation procedure. If another gauge is brought onto the project, it shall be correlated using the same procedure. Multiple gauges may be correlated from the same series of cores if done at the same time.

Note 5: For the purpose of this procedure, a job mix formula is defined as the percent and grade of paving asphalt used with a specified gradation of aggregate from a designated aggregate source. A new job mix formula may be required whenever compaction of the wearing surface exceeds the agency's specified maximum density or minimum air voids.

Core Correlation Example:

Core results from T166:		Density results TM-8:		Difference:	
2338 kg/m^3	144.9 lb/ft^3	2295 kg/m^3	142.1 lb/ft^3	43 kg/m^3	2.8 lb/ft^3
2306 kg/m^3	142.8 lb/ft^3	2275 kg/m^3	140.9 lb/ft^3	31 kg/m^3	1.9 lb/ft^3
2314 kg/m^3	143.1 lb/ft^3	2274 kg/m^3	140.7 lb/ft^3	40 kg/m^3	2.4 lb/ft^3
2274 kg/m^3	140.7 lb/ft^3	2243 kg/m^3	138.9 lb/ft^3	31 kg/m^3	1.8 lb/ft^3
2343 kg/m^3	145.1 lb/ft^3	2319 kg/m^3	143.6 lb/ft^3	24 kg/m^3	1.5 lb/ft^3
2329 kg/m^3	144.2 lb/ft^3	2300 kg/m^3	142.4 lb/ft^3	29 kg/m^3	1.8 lb/ft^3
2322 kg/m^3	143.8 lb/ft^3	2282 kg/m^3	141.3 lb/ft^3	40 kg/m^3	2.5 lb/ft^3

Average Difference: 34 kg/m^3 2.1 lb/ft^3

Standard Deviation: 6.5 kg/m^3 0.43 lb/ft^3

Report

Results shall be reported on standard forms approved by the agency. Include the following information:

- Location of test and thickness of layer tested
- Mixture type
- Make, model and serial number of the nuclear moisture-density gauge
- Mode of measurement, depth, calculated wet density of each measurement and any adjustment data
- Standard density
- Percent compaction and/or percent air voids
- Name and signature of operator

Addendum WAQTC TM 8

Following are guidelines for the use of WAQTC TM 8 by the State of Alaska DOT&PF.

1. Testing under this method shall be used for quality control and when specified, acceptance testing.
2. All density testing on HMA done under this method shall be done in Backscatter only.

Relative Standard Density by the Control Strip Method ATM 412

1. Scope

This method describes a procedure for determining the relative standard density of a material by the control strip testing method. This is applicable to Hot Mix Asphalt (HMA).

> **Note 1**: While ATM 412 is specifically for HMA, it may be used for other types of materials as specified.

2. Significance and Use

In testing some HMA's, determining the standard density may be difficult with conventional test methods used in the laboratory. When these problems occur a method that allows the determination of a relative standard density in the field can facilitate the verification of compaction efforts. This method describes a procedure to determine the relative standard density to be used in these circumstances.

3. Apparatus

- Nuclear Moisture/Density Gauge—Calibrate and standardize in accordance with WAQTC TM 8.
- Compaction equipment that meets the requirements of the contract and of sufficient size and compaction energy to compact the material.

4. Site Preparation

1. The Engineer will designate the location and the size of the control strip, as well as minimum compaction equipment to be used.
2. The subgrade will be compacted to a minimum density equal to that required for the material being tested. When the compaction is complete, the Engineer will approve the surface.
3. A representative lift of the material being evaluated will be placed and prepared for compaction.

5. Procedure

1. Attention should be paid to the requirements of the product being placed so that temperature and/or moisture requirements are maintained in an acceptable range.
2. A minimum of 3 test locations will be selected with-in the control strip. The locations will be in the middle 1/3 of the control strip and at least 600 mm (12 in) from the edge of the control strip. The Engineer will select test locations.
3. The locations will be marked in such a way as not to be lost during the compaction of the control strip. This can be accomplished by marking the side of the strip with stakes or surveyors tape, or by marking with paint beside the location on the control strip.
4. A test will consist of a 15 second (fast mode) wet density determination at each location unless otherwise stated in the project specifications.
5. Care should be taken when preparing the test location so that it is flat and the surface voids filled. If necessary, use a small quantity of dry sand for HMA or fines for other products to fill the voids. This layer will in no case be more than 3 mm (1/8 in) in depth.
6. After the first pass with the compaction equipment, an initial density test is taken and recorded.

   Note 1: One pass of the roller will be defined as one roll over the location.

7. After each subsequent pass, a test is taken at each location and recorded.
8. Continue the compaction and testing cycle until either of these conditions are met.

a. There is less than 16 kg/m^3 (1 lb/ft^3) increase in the wet density of the averaged density tests for each location on two consecutive passes.

b. There is less than 16 kg/m^3 (1 lb/ft^3) increase in the wet density of the average of all three locations for two consecutive passes.

9. Select ten random locations on the completed control strip and test using two one minute counts at each location. Average the results from the ten locations and this value will be the relative standard density for this material.

Note 2: It may be necessary to repeat the procedure for additional roller types depending on the material to be tested and the requirements of sequencing for the finished surface.

Note 3: It may be useful to record the moisture readings from the gauge for comparison with the acceptance tests.

10. Additional control strips may be required if there are changes in the material or lift thickness.

6. Calculations

1. The Relative Standard Density value will be calculated as follows:

$$D_S = \frac{(A_1 + A_2 + A_3 + A_4 + A_5 + A_6 + A_7 + A_8 + A_9 + A_{10})}{10}$$

Where:
D_S = Relative Standard Density for the material.
A_n = Average Density for random test location *n*.

7. Report

- Report the average density for each pass
- Report the standard density to the nearest 1 kg/m^3 (0.1 lb/ft^3)

SAMPLING BITUMINOUS MATERIAL AFTER COMPACTION (OBTAINING CORES)
WAQTC TM 11 (See Addendum for DOT&PF Guidelines)

Scope

- This method describes the process for removal of a sample of compacted bituminous material from a pavement for laboratory testing by obtaining test cores after compaction has been completed. Core diameter(s) may range in size from 2 in. to 12 in.

- The values stated in SI units are to be regarded as the standard. The values given in parentheses are for information only.

Significance And Use

- Samples obtained in accordance with the procedure given in this practice may be used for measuring pavement thickness, density, and acceptance testing.

- When cores are used to determine nuclear gauge correlation, see WAQTC TM 8.

- When cores are used to determine pavement density, the Bulk Specific Gravity (**G_{mb}**) is determined according to WAQTC FOP for AASHTO T 166 / T 275.

Apparatus

- Coring Machine – To minimize distortion of the compacted bituminous cores, a motor driver core machine shall be used to secure the sample that is capable of obtaining a core the full depth of the bituminous material.

- Core Bit – The cutting edge of the core drill bit shall be of hardened steel or other suitable material with diamond chips embedded in the metal cutting edge.

- Separation Equipment – Cores shall be separated with a saw or other method(s) that provides a clean smooth plane representing the layer to be measured, or tested.

- Retrieval Device – A retrieval device for removing core samples from holes that will preserve the integrity of the core. The device may be a steel rod of suitable length and with a diameter that will fit into the space between the core and the pavement material. There shall be a 90 degree bend at the top to form a handle and a 90 degree bend at the bottom, approximately 50 mm (2 in.) long, forming a hook to assist in the retrieval of the core.

Material

- Water, ice, dry ice, liquid nitrogen, or other cooling material.

Safety

- This method does not purport to address all of the safety problems associated with its use. This test method involves potentially hazardous conditions.

Test Site Location

- The quantity of cores to be obtained shall be determined by the test procedure to be performed or agency requirements.

- Determine the location of the core(s) as required by the agency.

Procedure

- For freshly placed bituminous materials, the core shall be taken when the material has had sufficient amount of time to cool to prevent damage to the core.

- Cores may be taken by cooling the pavement to allow for immediate removal. Cooling may be expedited with the use of water, ice water, ice, or dry ice.

- Place the coring machine and core bit over the selected location.

- Start the flow of coolant to ensure removal of the cuttings and to minimize the generation of heat caused by friction.

- Keep the core bit perpendicular to the bituminous surface during the coring process. If any portion of the coring machine shifts during the operation, the core may break or distort.

- Constant downward pressure should be applied on the core bit. Failure to apply constant pressure, or too much pressure, may cause the bit to bind or distort the core.

- Continue the coring operation until the desired depth is achieved.

- If necessary, use a retrieval device to remove the core.

- If the core is damaged to a point that it can not be utilized for its intended purpose, a new core shall be obtained within 12 in. of the original location.

- Clearly identify the core without damaging it.

Filling Core Holes

- The hole made from the coring operation shall be filled with a material that will not become dislodged. If a bituminous material is available and used, it shall be compacted into the hole. A fast set concrete product may be used in lieu of a bituminous material.

Transporting Cores

- Transport cores on a smooth surface, top side down in a container(s) that prevents damage from jarring, rolling, hitting together, and/or impact with any object.

- Prevent cores from freezing or from excessive heat, 54° C (130º F), during transport.

Note #1: In extreme ambient temperature conditions, an insulated container should be used during transport.

- If the core is damaged to a point that it can not be utilized for its intended purpose the core will not be used for acceptance tests.

Separate the Layers

- When necessary to separate two or more pavement courses, lifts, or layers; separate by using a saw to cut the core on the designated lift line. Water must be sprayed on the saw blade to minimize the generation of excessive heat.

Note #2: Lift lines are often more visible by rolling the core on a flat surface.

Length Determination

- Measure the thickness of the designated lift to 3 mm. (0.1 in). Three or more measurements shall be taken around the lift and averaged.

Report

- Core information shall be reported on standard agency forms. Include the following information:

  - The date the cores were obtained
  - Location of test and thickness of layer tested
  - The lift being evaluated
  - Type of material being evaluated
  - Mix Design Lab Number
  - Average thickness of each core (to the nearest 3 mm or 0.1 in.)

Addendum WAQTC TM 11

Following are guidelines for the use of WAQTC TM 11 by the State of Alaska DOT&PF.

1. While saw cutting is the preferred method, the different layers in a core may be separated by freezing and use of a chisel and hammer or by use of a hammer and chisel alone if a saw is not available. Care must be taken to protect the core from deformation or damage during the separation. If the core is deformed or damaged, it must be discarded and a new core taken.
2. Core locations – Joint cores shall be centered on the longitudinal joint.
3. Determine and record the length of the core to 5 mm (¼″).

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Anti-Strip Requirements of Hot Mix Asphalt ATM 414

1. Scope

This method, an adaptation of AASHTO T 182, describes a procedure for determining the retention of a bituminous film by aggregate in the presence of water. It is applicable to asphalt cements, cutback asphalts and emulsified asphalts.

2. Apparatus

- Balance or scale: Capacity sufficient for the principle sample mass, readable to 0.1 percent of the total sample mass and meeting the requirements of AASHTO M 231.
- Thermostatically controlled oven capable of maintaining any required constant temperature between 49-150 ± 1ºC (120-300 ± 1°F).
- A 9.5 mm (⅜") and a 4.75 mm (No. 4) mm sieve conforming to AASHTO M 92.
- 600 ml beakers, low form glass or plastic type.
- Thermostatically controlled water bath capable of maintaining a temperature of 49º ± 1ºC (120° ± 2°F).
- Miscellaneous equipment including a steel spatula with stiff blade (approximately ½" wide x 4" long (25 mm x 100 mm), glass or plastic containers for mixing samples, and air-tight containers of suitable size for storing bitumen and anti-strip mixtures.

3. Sample Preparation

1. Aggregate:
   a. The test aggregate shall be processed in the same manner as that which would be used during the construction process.
   b. Dry the aggregate to a constant weight in accordance with WAQTC FOP for AASHTO T 255.
   c. Separate the aggregate by sieving to obtain the minus 9.5 mm (⅜") plus (No.4) material. Reduce this material, in accordance with WAQTC FOP for AASHTO T 248, Method A, to obtain approximately 1200 g.
2. Anti-stripping additive used in testing will be the same brand and type proposed for use on the project.
3. Bitumen and/or emulsified asphalts will be the same type and grade proposed for use in mix design.

4. Procedure

1. For asphalt cement and/or cutback asphalt samples:
   a. Thoroughly mix the bitumen samples with the anti-strip additive in the proportions of 0.25 percent, 0.50 percent, and 0.75 percent or as required. If necessary to store this mixture, use airtight containers.

      Note 1: After the additive is added to the bitumen standards they shall not be reheated in excess of preheat temperatures as outlined in (1) and (2) below.

   b. Make up 1 or more aggregate specimens per additive content by placing 100 ± 1 gram of the aggregate to be tested into individual mixing containers.
   c. Preheat aggregate specimens to the temperature of the respective bitumen below:

      (1) Asphalt cements: Preheat in oven at a temperature within the binders mixing temperature range for no longer than 30 minutes.

      (2) Cut-back asphalts:

      Grades 30 to 250. No preheat required.

Grades 800 to 3000: Preheat at 60-90ºC (140-195 °F) for no longer than 30 minutes.

d. Preheat the bitumen at the respective temperatures above until it can be poured.

e. Add 5.5 ± 0.5 g of bitumen-additive mixture to the aggregate specimen(s).

f. Mix the bitumen and aggregate thoroughly until uniformly coated.

g. The bitumen-aggregate specimen(s) shall be oven-cured at a temperature 60 ± 1ºC (140 ± 2°F) for a minimum of 18 hours but no more than 24 hours.

h. Remove the sample(s) from the oven and re-mix to obtain a uniform coating. Allow the specimen(s) to cool to a temperature of 49ºC (120°F) or less.

i. Place 50 ± 1 g of each of the coated aggregates into individual 600 ml. beakers.

j. Add 400 ml distilled water, cover and place in an oven or water bath maintained at 49º ± 1ºC (120 ± 2°F) for 24 hours. If a water bath is used, the container(s) shall not be submerged so as to allow bath water into the beakers.

2. For emulsified asphalts (anionic/cationic):

IMPORTANT: ANTI-STRIPPING ADDITIVE WILL NOT BE USED WITH EMULSIFIED ASPHALTS.

a. Preheat the emulsified asphalt to 38 ± 1°C (100 ± 2°F). Mix the asphalt thoroughly.

b. Make up 3 aggregate samples by placing 100 ± 1 g of the aggregate into individual containers.

c. Preheat aggregate specimens to the emulsified asphalt preheat temperature listed in Step 1.c (2).

d. Add 8.0 ± 0.5 g of each emulsion to the 100 g samples of aggregate and mix until the stones are uniformly coated.

e. The emulsion-coated aggregate shall be cured at 132º ± 3ºC (270 ± 5°F) for a minimum of 18 hours but no more than 24 hours.

f. Follow Steps 1.h thru 1.j.

5. Observations

1. Without disturbing or agitating the coated aggregate, remove any film floating on the water surface.
2. By observation through the water from above, estimate to the nearest 10 percent of the total visible surface area the aggregate coated with bitumen. Any thin brownish translucent areas are to be considered fully coated.
3. Average the results if more than one specimen was prepared for each additive content.

6. Report

Report the results on Department forms. The results will include the following:

- The visible bitumen/emulsion-covered area estimated to the nearest 10 percent for each additive content tested.
- The lowest percentage of additive required to obtain a 70 percent bitumen coating on the aggregate.
- Type and grade of bitumen/emulsion used.
- Brand of anti-stripping agent use.

Hot Mix Asphalt Design by the Marshall Method ATM 417

1. Scope

This method describes the Marshall Mix Design procedure for determining the optimum asphalt content, stability, flow and void properties of hot bituminous mixtures containing aggregates with maximum sizes of (1") or less. As recommended by AASHTO R 12, this method is adapted from the Asphalt Institute "Mix Design Methods for Asphalt Concrete and Other Hot Mix Types", Manual Series No. 2 (MS-2). It also includes information and procedures from AASHTO T 245 and AASHTO R 30.

2. Apparatus

- Ovens and hot plates thermostatically controlled to maintain the various required temperatures within ± 3°C (5°F).
- Temperature measuring devices:

  For asphalt binder and mixes: having a range of 10-200°C (50-400°F) and sensitive to 3°C (5°F).

  For the water bath: readable and sensitive to ± 0.2°C (0.5°F) at 60°C (140°F).

- Balance or scale: Capacity sufficient for the principal sample mass, readable to 0.1 percent or 0.1 g of the total sample mass and meeting the requirements of AASHTO M 231.
- Sieve shaker meeting the requirements of WAQTC FOP for AASHTO T27.
- Mechanical mixer with a wire whip mixing blade capable of producing a well-coated, homogeneous mixture and mixing bowls. Means of maintaining the mixture at mixing temperature, such as a heat lamp mounted below the mixer.

  Note 1: The Hobart Kitchen Aid Model K-5A with wire whip Model K5A-WW has been found satisfactory.

- The mold assemblies, compaction pedestal, mold holder, extruder, breaking head and flow meter or stress-strain recorder shall conform to AASHTO T 245.
- Mechanical compaction device conforming to AASHTO T 245. The device shall be equipped with a counter that will automatically shut off the machine at the required number of blows. The device will be calibrated annually in accordance with ASTM D 2168.
- Paper discs of heavy weight non-absorbent paper stock, 100 mm (4") diameter.

  Note 2: The Humboldt H-1341P paper disc has been found satisfactory.

- The water bath shall be at least 150 mm (6") deep and shall be thermostatically controlled so as to maintain a temperature of 60 ± 1°C (140 ± 1.8°F). The bath shall be equipped with an agitator to keep the water in constant circulation. It shall have a perforated false bottom or shelf for supporting the specimens a minimum of 2" (50 mm) above the bottom of the bath. The bath shall have a flat surface area large enough to allow the specimens to set singly with water flowing freely around each specimen. Stacking specimens is prohibited.
- Loading jack consisting of either a motor-driven screw jack, a hydraulic or other mechanical loading device which shall produce a uniform loading-head movement rate of 50 mm (2") per minute, independent of the load being applied. The loading frame shall have a minimum load capacity of 25 KN (5000 lb).
- Load-measuring device of 25 KN (5000 lb) minimum capacity, sensitive to 50 N (10 lb) or less, and capable of measuring displacement to 0.0025 mm (0.0001"). This device may be a load-cell or a ring dynamometer assembly.

- Flowmeter—The flowmeter shall consist of a guide sleeve and a gage. The activation pin of the gage shall slide inside the guide sleeve with a slight amount of frictional resistance. The guide sleeve shall slide freely over the guide rod of the breaking head. The flowmeter gage shall be adjusted to zero when placed in position on the breaking head when each individual test specimen is inserted between the breaking head segments. Graduations of the flowmeter gauge shall be in 0.25 mm (0.01") divisions.
- Data measuring/recording/display devices capable of the capacity and sensitivity of the load-measuring device and or flowmeter.
- Miscellaneous equipment including scale or caliper readable to 0.25 mm (0.01"), sample containers (metal pans, bowls or beakers), spatulas, spoons, marking crayons, heat-resistant gloves, straight-edge, etc.
- Bituminous Mix Design Worksheet, Bituminous Mix Design Report, and 0.45 Gradation Chart paper.

3. Synopsis

Aggregate properties important to bituminous mixes shall be determined as required. For Asphalt Concrete Pavement (ACP) mixes this will include: gradation of each submitted aggregate and, after combining according to the proposed Job Mix Formula (JMF), the plasticity index, fracture, flat & elongated, and bulk specific gravity of the coarse & fine aggregate. For Stone Mastic Asphalt (SMA) mixes, in addition to the tests listed for ACP mixes, the unit mass of the combined coarse aggregate and the apparent specific gravity of the mineral filler will be required.

A minimum of four (4) sets of three (3) specimens each, shall be prepared, mixed and compacted at different asphalt contents. These asphalt contents shall be by mass of total mix and will be at 0.5 percent increments. These specimens will be tested for Unit Mass, Marshall Stability & Flow, Percent Air Voids in Total Mix (VTM), Percent Voids in Mineral Aggregate (VMA), Percent Voids Filled with Asphalt (VF), and (for SMA mixes) Voids in Coarse Aggregate (VCA). The final results will define the VTM over that parameters specification range and should define the maximum values of the Stability and Unit Mass of the mix and the minimum value for VMA.

Three (3) specimens shall be prepared, mixed and tested to determine the maximum specific gravity in accordance with WAQTC FOP for AASHTO T 209.

Calibration specimens will be prepared as required by the Acceptance testing program for the project. The calibrations may include any of the following:

- JMF Calibration Points for the Nuclear Asphalt Content Gauge for ATM 405.
- Ignition Furnace Calibration Points for each Ignition Furnace System for WAQTC FOP for AASHTO T 308.

4. Determination of Asphalt Cement Properties

If not provided by the supplier, determine the following:

4.1 Verify compliance of the asphalt cement plus additives to specifications; in addition, determine the specific gravity at 25°C (77°F) of the asphalt binder in accordance with AASHTO T 228/ASTM D 70.

4.2 Establish the temperature-viscosity properties of the binder in accordance with ASTM D 2493 with the viscosities determined in accordance with the following as required by the project specifications:

AASHTO T 201 & T 202 ASTM D 2170 & D 2171	Or	AASHTO T 315 & T316

4.3 Select the mixing and compaction temperatures using the temperature-viscosity data. Determine, unless otherwise specified, the mixing temperature at 170 ± 20 centistokes and the compaction temperature at 280 ± 30 centistokes.

Note 3: Modified asphalts may not adhere to the equiviscosity requirements noted; the manufacturer's recommendations should be requested and used to determine mixing and compaction temperatures. Practically the mixing temperature should not exceed 165°C (330°F) and the compaction temperature should not be lower than 115°C (240°F).

5. Preparation of Aggregate

The aggregates used for the mix design will represent the aggregates in the contractor's stockpiles. The laboratory will use the aggregate as presented by the contractor and prepare the aggregate in the same manner as it will be handled during production. In no event will the aggregate be washed in the preparation of any test specimens other than the dust correction procedure.

5.1 Obtain samples from each individual aggregate in accordance with WAQTC FOP for AASHTO T 248 for the determination of the:

- Gradation in accordance with WAQTC FOP for AASHTO T 27/T 11
- Plastic Index in accordance with WAQTC FOP for AASHTO T 89 and WAQTC FOP for AASHTO T 90
- Sand Equivalent in accordance with WAQTC FOP for AASHTO T 176, if required.

5.2 Mix the aggregates from the individual stockpiles at the blend ratio specified by the contractor.

Separate the combined aggregates by dry sieving into individual specification sieve sizes including the minus 75 µm (No. 200) material. As the material is being dry sieved, separation will not be as efficient as when using washed samples. Therefore sieving time must be increased to separate as efficiently as possible. Sieving times should be increased to 15 minutes for coarse aggregate separation and 15-20 minutes for fine aggregate. The increased sieving time may be determined in accordance with WAQTC FOP for AASHTO T 27 (see Note 5).

Separate sufficient aggregate to perform all required tests (i.e. Marshall Stability, Calibration Points for Nuclear Content Gauge, Ignition Furnace, and aggregate Quality as required).

5.3 Using the contractor-proposed gradation, calculate the initial cumulative masses for each specification sieve size by the following:

$$X = \frac{(100 - P_N)}{100} \times E_i$$

where:
X = Cumulative aggregate batch masses for sieve size N,
P_N = Percent passing from proposed gradation for sieve size N, and
E_i = Initial total aggregate mass for a Marshall specimen.

Note 4: The initial aggregate mass may be chosen based on experience or a mass such as 1200 g may be assumed at this point. If a mass is assumed, a trial specimen to determine if height adjustment in accordance with the methodology of Preparation of Test Specimens, Step 1 a thru c will be required.

5.4 Aggregate Batching Correction:

As the JMF gradation was determined in accordance with WAQTC FOP for AASHTO T 27/T 11, which washed the sample in some manner, and the material for the mix design has been separated by dry sieving which will not completely separate the aggregate, a correction must be made to the material separated for the mix design to ensure that the proper amount of aggregate but especially the minus 75 µm (No. 200) material is included in the test specimens. If this is not done, batching material in accordance with the methodology outlined in this method will result in the mix design having a higher percentage of aggregate, fine sand and/or silt than the contractor's JMF proposes.

a. Prepare a wash gradation sample.

   Calculate the initial batch masses for the wash gradation.

b. Perform a wash gradation in accordance with WAQTC FOP for AASHTO T 27/T 11.

c. Compute the adjusted cumulative batch masses for each of the sieve sizes by the following formula:

$$Z_{Ni} = \frac{X^2}{Y}$$

where:

Z_{Ni} = corrected cumulative batch mass for sieve size N,
X = pre-wash cumulative batch mass for sieve size N,
Y = post-wash cumulative batch mass for sieve size N.

Note 5: In some cases, the adjusted cumulative batch masses will result in decreasing batch masses instead of increasing batch masses. This indicates that the dry sieving operation did not efficiently separate the fine aggregate, leaving too much 75 µm (No. 200) and minus 75 µm (No. 200) material in the larger aggregate sizes. If this occurs, resieve the sizes showing the decreasing batch masses, combining the separated material with the material already separated and perform Step 4 a thru c again.

d. Tabulate the overall adjusted cumulative batch.

6. Estimate Projected Optimum Asphalt Content

6.1 Estimate the projected optimum asphalt content. This value can be based on any or all of these sources:

a. Experience. This is the most important method of estimating projected optimum asphalt content. The projected optimum asphalt content will be estimated to the nearest 0.5 percent with four (4) sets of three (3) specimens prepared to bracket the projected optimum at 0.5 percent intervals.

   The following methods may be used where no experience exists for the proposed material and/or JMF target values.

b. Computational formula:

$$P = 0.035a + 0.045b + Kc + F$$

where:

P = projected optimum asphalt content of mix, percent by mass of mix,
a = percent retained on the 2.36 mm (No. 8) sieve, expressed as a whole number
b = percent passing the 2.36 mm (No. 8) sieve and retained on the 75 µm (No. 200) sieve, expressed as a whole number
c = percent passing the 75 µm (No. 200) sieve, expressed to the 0.1 percent
K = 0.15 for 11 to 15 percent passing the 75 µm (No. 200) sieve, or
0.18 for 6 to 10 percent passing the 75 µm (No. 200) sieve, or
0.20 for 5 percent or less passing the 75 µm (No. 200) sieve, and
F = asphalt absorption. In the absence of other data, use 0.7 percent.

   The projected optimum asphalt content will be rounded to the nearest 0.5 percent with specimens prepared as indicated under step 1.a.

c. Dust-Asphalt Ratio: Since the Dust-Asphalt Ratio specification is typically 0.6 to 1.2, using the larger of the D/A limits will give the projected minimum *effective* asphalt content for the JMF p200 target. Solving the Dust-Asphalt ratio formula for the projected minimum asphalt content percent (effective asphalt content plus absorbed asphalt):

Max. $D/A = \left(\frac{p200}{P}\right)$

for P results in $P = \left(\frac{\text{p200}}{Max.D/A}\right)$

where:
P = projected minimum *effective* asphalt content of mix, percent by mass of mix,
p200 = percent passing the 75 µm (No. 200) sieve, and
Max. D/A = dust-to-asphalt ratio.

The total projected asphalt content may be estimated by:

$P_m = P + F$

where:
P_m = projected minimum asphalt content, percent
P = projected minimum effective asphalt content of mix, percent
F = asphalt absorption, percent. In the absence of other data use 0.7 percent.

This projected minimum asphalt content will be rounded to the nearest 0.5 percent with specimens prepared for at this projected minimum value and at least three (3) more above this value at 0.5 percent intervals.

7. Preparation of Test Specimens

7.1 Marshall Stability and Flow: Batch a minimum of four (4) sets of three (3) aggregate specimens each. However, if the initial total aggregate mass for the Marshall specimen was estimated without prior experience, a single Marshall specimen will be batched, mixed at the projected optimum asphalt content, compacted and the thickness of the compacted specimen measured to determine if the aggregate mass must be adjusted.

a. Thickness Adjustment

1) The height of the compacted specimen must be within the specimen thickness limitations of 62-65 mm (2.45-2.55"). If it is not, adjust the total mass of the aggregate as shown below and recalculate the individual sieve masses to bring the specimens within this range.

2) Prepare an aggregate batch to the masses calculated above and calculate the mass of asphalt required for the estimated optimum asphalt content as shown below. Mix and compact the trial specimen in accordance with the requirements of sections **9** and **11.**

3) If thickness adjustment is necessary, adjust E_i, the initial total aggregate mass, by the following:

$$E_a = \frac{2.5 \times E_i}{H} \text{ (USC) or } \frac{63.5 \times E_i}{H} \text{ (SI)}$$

where:
E_a = adjusted total aggregate mass,
E_i = initial total aggregate mass, and
H = specimen thickness 0.1 mm (0.01") actually obtained.

4) If necessary, adjust each Z_{Ni} from Step 4c by:

$$Z_{Na} = \frac{E_a}{E_i} \times Z_{Ni}$$

where:
Z_{Na} = adjusted cumulative batch mass for sieve size N,
E_a = adjusted total aggregate mass,

E_i = initial total aggregate mass,
Z_{Ni} = corrected cumulative batch mass for sieve size N.

5) Using either the corrected cumulative sieve masses (Z_{Ni}) determined in **Preparation of Aggregate**, Step 4c or the adjusted cumulative sieve masses (Z_{Na}) determined in Step 1a, above, prepare three (3) aggregate specimens for each asphalt content. The aggregate for each specimen will be batched and placed in a container and dry-mixed thoroughly.

b. Calculate the mass of the asphalt cement for each set of specimens by:

$$AW = \frac{E_i \text{ (or } E_a) \times P_{bN}}{100 - P_{bN}}$$

where:
AW = mass of asphalt cement, to the nearest 0.1 g,
E_i (or E_a) = initial (or adjusted, see below) aggregate mass, and
P_{bN} = asphalt content for set N, to the nearest 0.1 percent.

7.2 Maximum Specific Gravity of Mixture.

a. For each sieve size, calculate the cumulative masses for a maximum specific gravity test specimen by the following formula:

$$R_N = \frac{Q}{E_i} \times Z_{Ni}$$

where:
R_N = cumulative batch mass for the maximum specific gravity specimen for sieve size N,
E_i = initial total aggregate mass,
Z_{Ni} = adjusted cumulative batch mass for sieve size N, and
Q = minimum sample mass required by WAQTC FOP for AASHTO T 209.

b. Prepare three (3) test specimens to these masses for performance of WAQTC FOP for AASHTO T 209.

7.3 Coarse Aggregate Properties.

a. For each coarse aggregate sieve size, calculate the cumulative masses for the required test specimens of coarse aggregate for the required test procedures by the following formula:

$$C_N = \frac{Q}{\text{No. 4 } E_i} \times Z_{Ni}$$

where: C_N = cumulative batch mass for the maximum specific gravity specimen for sieve size N, for the 4.75 mm (No. 4) and larger sieves only,
Q = minimum sample mass required for the required tests.
No. 4 Z_i = initial total aggregate mass of 4.75 mm (No. 4), and
Z_{Ni} = adjusted cumulative batch mass for sieve size N.

b. Prepare the required number of test specimens to the minimum sample size required by the test procedure for the performance of the following or other specified tests as required:

Test Procedure Designation	Title	Number of Specimens
WAQTC FOP for AASHTO T 85	Specific Gravity	1
WAQTC FOP for AASHTO TP 61	Fracture	1

ATM 306	Flat-Elongated	1
AASHTO T 19 (SMA only)	Bulk Density	3

7.4 Fine Aggregate Properties.

a. For each fine aggregate sieve size, calculate the cumulative masses for the specific fine aggregate property test by the following formula:

$$F_N = \left(\frac{Q}{E_i - Z_{4i}} \right) x \left(Z_{Ni} - Z_{4i} \right)$$

where:

F_N = cumulative batch mass for the fine aggregate specific gravity specimen for sieve size N, for the minus 4.75 mm (No. 4) sieves only,

Q = sample mass required for the specified test,

E_i = initial total aggregate mass,

Z_{Ni} = initial cumulative batch mass for sieve size N, and

Z_{4i} = initial cumulative batch mass for the 4.75 mm (No. 4) sieve. b. Prepare the required number of test specimens to the minimum sample size required by the test procedure for the performance of the following or other specified tests as required:

Test Procedure Designation	Title	Number of Specimens
AASHTO T 84	Specific Gravity	3
WAQTC FOP for AASHTO T 176	Sand Equivalent	1

7.5 Mineral Filler Specific Gravity.

If the JMF p200 is greater than 6 percent, the minus 75 µm (No. 200) material will be treated as mineral filler and the apparent specific gravity of this material will be determined in accordance with AASHTO T 100.

8. Preparation of Asphalt Cement

Heat a minimum of 1 L (1 qt) of asphalt cement to the mid-point of the mixing temperature range.

It is best to use the asphalt cement as soon as it reaches mixing temperature. If this is not possible, maintain the asphalt cement at this temperature in a covered container rather than reheat it.

9. Preparation of Mixtures and Mixture Conditioning

9.1 Place the aggregate specimens for Marshall Stability & Flow and Maximum Specific Gravity in the oven and heat to the mid-point of the asphalt cement mixing temperature range.

9.2 "Butter" the mixing bowl with an asphalt and fine aggregate mixture that will coat the mixing area of the bowl. Remove any excess material.

9.3 Place the heated specimen into the mixing bowl.

9.4 Form a crater in the dry blended aggregate large enough to hold the asphalt cement, place the mixing bowl on the scale and weigh into the aggregate crater, to the nearest 0.1 g, the required amount of pre-heated asphalt cement.

9.5 Mechanically mix the aggregate and asphalt cement rapidly until thoroughly coating the aggregate and return to the oven.

9.6 After mixing, spread the mixture in a pan to an even thickness of 25-50 mm (1-2 inches). Place the mixture and pan in a forced-draft oven at the midpoint of the compaction temperature range for 120 ± 5 minutes. Stir the mixture after 60 ± 5 minutes to maintain uniform conditioning. Highly absorptive aggregates may require a longer conditioning time.

10. Equipment Preparation

10.1 Thoroughly clean the mold assemblies (molds, bases and collars) and heat in an oven to the mid-point of the asphalt cements compaction temperature range.

10.2 Thoroughly clean the face of the compaction hammer and heat on a hot plate to a temperature within the asphalt cements compaction temperature range.

11. Compaction of Specimens

11.1 Place the pre-heated mold assembly into the mold holder on the compaction pedestal. Place a paper disc in the bottom of the mold.

11.2 Stir the specimen thoroughly and place in the mold. Spade the mixture vigorously with a heated spatula 15 times around the perimeter and 10 times over the interior, remove the collar and smooth the surface of the mix to a slightly rounded shape.

11.3 Place a paper disc on top of the specimen, position the compaction hammer, and apply the required number of blows with the compaction hammer.

11.4 Remove the base plate and collar, invert and re-assemble the mold, and apply the same number of blows to the face of the inverted specimen.

11.5 Remove the collar, base plate and paper discs, mark each biscuit for individual identification, and allow them to cool until the specimen can be extruded without damage or distortion.

11.6 Extrude the specimen from the mold; transfer to a smooth, flat surface; allow it to stand and cool to room temperature.

12. Mix Sample Test Procedures

12.1 Measure and record the thickness of each compacted specimen and record to the nearest 0.25 mm (0.01"). Use either a device that will measure the average height or measure the height with a caliper at three (3) locations spaced evenly around the circumference of the specimen and average these results.

12.2 Determine the bulk specific gravity of each compacted specimen in accordance with WAQTC FOP for AASHTO T 166.

12.3 Stability and Flow.

a. Bring the specimens to the specified temperature of 60 ± 1°C (140 ± 1.8°F) by immersing in the water bath for 30 to 40 minutes. Stacking specimens on top of each other is prohibited.

b. Thoroughly clean and lubricate the guide rods, and clean the inside surfaces of the breaking heads before performing the stability and flow tests. Maintain the breaking head at a temperature of 21 to 38°C (70 to 100 °F).

c. Remove the specimens one at a time from the water bath and place in the lower segment of the breaking head.

d. Place the upper segment of the breaking head on the specimen, firmly seat the head on the specimen, and place the complete assembly in position on the loading jack.

The elapsed time for the test from the removal of the test specimen from the water bath to the maximum load determination shall not exceed 30 seconds.

e. For machines using proving ring & flow meter:

1) Place the flow meter over one of the guide rods and adjust the flow meter to zero; hold the sleeve firmly against the upper segment of the breaking head while the test load is applied.

2) When the load to the specimen at a constant rate of 50.8 mm (2") per minute until the maximum load is reached. The maximum load is indicated when the proving ring dial value decreases.

3) Simultaneously read the proving ring dial to the nearest 0.0025 mm (0.0001") and the flow meter to the nearest 0.25 mm (0.01"). Record the readings as whole numbers (no decimal points) from the proving ring dial flow meter.

f. For machines using load cell and chart recorder/display:

1) Turn on the recorder, adjust the pen to the zero position according to the manufacture's instructions, turn the range selector to the appropriate range (use the smallest range possible) and set the chart speed at 10" per minute (250 mm per minute).

2) Apply the load to the specimen by means of the constant rate movement of the loading jack at 50 mm per minute (2" per minute) until the maximum is reached and the load, as indicated by the chart recorder, decreases.

12.4 Maximum Specific Gravity.

Determine the maximum specific gravity of the prepared specimens at or near the optimum asphalt content in accordance with WAQTC FOP for AASHTO T 209 as follows:

a. Choose a projected optimum asphalt content as described in **Estimate Projected Optimum Asphalt Content**.

b. Mix and condition the specimens in accordance with the provisions of **Preparation of Mixtures and Mixture Conditioning**.

c. Determine the maximum specific gravity in accordance with WAQTC FOP for AASHTO T 209 on the prepared specimens at the projected optimum asphalt content.

d. If the projected optimum asphalt content differs from the final optimum asphalt content, determined below in **Determination of Optimum Asphalt Content, Selection of Final Optimum Asphalt Content**, by 1 percent or more, prepare and determine a new maximum specific gravity at the final optimum asphalt content and recalculate the maximum specific gravities at the other asphalt contents, the voids total mix and the optimum asphalt content.

13. Calculations

13.1 Calculate the bulk specific gravity of each compacted specimen in accordance with WAQTC FOP for AASHTO T 166. Average the bulk specific gravities (G_{mb}) of all compacted specimens for each asphalt cement content.

Record the result to the nearest 0.001.

13.2 Calculate the unit mass for each asphalt content by:

$$W_N = G_{mbN} \times 997.1 \text{ kg/m}^3 \ (62.245 \text{ lb/ft}^3)$$

where:
W_N = unit mass of set N,
G_{mbN} = average bulk specific gravity of set N, and
997.1 kg/m^3 (62.245 lb/ft^3=density of water at 25°C (77°F).

Record the result to the nearest 1 kg/m^3 (0.1 lb/ft^3).

13.3 Calculate the maximum specific gravity of the mix at the selected asphalt content in accordance with WAQTC FOP for AASHTO T 209. Average the results and record the average to the nearest 0.001.

13.4 Calculate the maximum specific gravity for each asphalt content as follows:

a. Calculate the effective specific gravity of the aggregate by:

$$G_{se} = \frac{100 - P_b}{\frac{100}{G_{mm}} - \frac{P_b}{G_b}}$$

where:

G_{se} = effective specific gravity of the aggregate,
P_b = asphalt content at which G_{mm} was determined,
G_{mm}= maximum specific gravity at P_b,
G_b = specific gravity of the asphalt at 25 °C (77°F).

Record the result to the nearest 0.001.

b. Calculate the maximum specific gravity for each asphalt content by:

$$G_{mm} = \frac{100}{\frac{100 - P_{bN}}{G_{se}} + \frac{P_{bN}}{G_b}}$$

where:

G_{mm} = maximum specific gravity for asphalt content P_{bN},
G_{se} = effective specific gravity of the aggregate,
P_{bN} = percent asphalt for set N, and
G_b = specific gravity of the asphalt at 25 °C (77°F).

Record the result to the nearest 0.001.

13.5 Calculate the percent air voids in total mix (VTM) for each asphalt content by:

$$\text{VTM} = \frac{G_{mm} - G_{mb}}{\text{G}_{\text{mm}}} \times 100$$

where:

VTM = percent voids total mix,
G_{mb} = average specific gravity of each content, and
G_{mm} = maximum specific gravity of each content.

Record the result to the nearest 0.1 percent.

13.6 Calculate the percent voids in mineral aggregate (VMA) for each asphalt content by:

a. Calculate the blended aggregate bulk specific gravity by:

$$\text{G}_{\text{sb}} = \frac{100}{\frac{\text{P}_1}{\text{G}_1} + \frac{\text{P}_2}{\text{G}_2} + \ldots \frac{\text{P}_\text{N}}{\text{G}_\text{N}}}$$

where:

G_{sb} = blended aggregate bulk specific gravity,
P_1, P_2 ...& P_N = percent of individual aggregate,
G_1, G_2…&G_N = bulk specific gravity individual aggregate.

Record the result to the nearest 0.001.

b. Calculate the percent voids in mineral aggregate for each asphalt content by:

$$VMA = 100 - \frac{G_{mb}\ (100 - P_b)}{G_{sb}}$$

where:

VMA = percent voids in mineral aggregate for each content,
G_{sb} = blended aggregate bulk specific gravity,
G_{mb} = average bulk specific gravity for each content, and
P_b = percent asphalt of each content.

Record the result to the nearest 0.1 percent.

13.7 Calculate the percent voids filled with asphalt for each asphalt content by:

$$\text{VFA} = 100 \times \frac{\text{VMA} - \text{VTM}}{\text{VMA}}$$

where:

VFA = percent voids filled with asphalt for each content,
VMA = percent Voids in mineral aggregate for each content, and
VTM = percent voids total mix for each content.

Record the result to the nearest whole percent.

13.8 Calculate the dust/asphalt ration for each asphalt content by:

a. Calculate the asphalt absorption by:

$$P_{ba} = 100\left(\frac{G_{se} - G_{sb}}{G_{sb} \times G_{se}}\right)G_b$$

where:

P_{ba} = absorbed asphalt, percent by mass of aggregate,
G_{se} = effective specific gravity of aggregate,
G_{sb} = bulk specific gravity of aggregate, and
G_b = specific gravity of asphalt.

b. Calculate the effective asphalt content for each asphalt content by:

$$P_{be} = P_b - \left(\left(\frac{P_{ba}}{100}\right) \times (100 - P_b)\right)$$

where:

P_{be} = effective asphalt content, percent by total mass of mix,
P_b = asphalt content, percent by total mass of mix, and
P_{ba} = absorbed asphalt, percent by mass of aggregate.

c. Calculate the dust/asphalt ratio by:

$$\text{D/A} = \frac{\text{p200}}{P_{be}}$$

where:

D/A = dust/asphalt ratio,
p200 = percent passing the 75 µm (No. 200) sieve, and

P_{be} = effective asphalt content, percent by total mass of mix.

13.10 Stability:

a. For machines using proving ring and flow meter, calculate the uncorrected stability from the dial readings by the following:

$$S = (D \times m) + C$$

where:

S = uncorrected stability load, in pounds,
D = dial reading as a whole number
m = slope from proving ring calibration, and
C = constant from proving ring calibration.

Record the result to the nearest whole pound.

b. For machines using load cell and chart recorder/display, read and record the uncorrected stability to the accuracy allowed by the chart scale.

c. Stability values for each specimen that differ from the standard 63.5 mm (2.5") thickness will be corrected to the equivalent 63.5 mm (2.5") value by the following:

$$CS = S \times t$$

where:

CS = corrected stability,
S = uncorrected stability, and
t = thickness correction factor = 4.2992 ($x^{-1.5901}$) for USC units or 531 ($x^{-1.5118}$) for SI units.

Table 1
Thickness Correction Factors

USC		SI			
Thickness, 0.01"	t	Thickness, 0.1 mm	t	Thickness, 0.1 mm	t
		62.0	1.036	63.5	0.999
2.45	1.034	62.1	1.033	63.6	0.997
2.46	1.027	62.2	1.031	63.7	0.994
2.47	1.021	62.3	1.028	63.8	0.992
2.48	1.014	62.4	1.026	63.9	0.990
2.49	1.008	62.5	1.023	64.0	0.987
2.50	1.000	62.6	1.021	64.1	0.985
2.51	0.995	62.7	1.019	64.2	0.983
2.52	0.989	62.8	1.016	64.3	0.980
2.53	0.983	62.9	1.014	64.4	0.978
2.54	0.973	63.0	1.011	64.5	0.976
2.55	0.970	63.1	1.009	64.6	0.974
		63.2	1.006	64.7	0.971
		63.3	1.004	64.8	0.969
		63.4	1.002	64.9	0967
				65.0	0.965

d. Corrected stability values for each asphalt content averaged and recorded to the nearest 50 N (10 lb) 10. Flow:

a. For machines using the proving ring and flow meter, average the flow values for each asphalt content and record as a whole number (e.g. flow reading of 0.12 will be recorded as 12).

b. For machines using load cell and chart recorder:

1) Extend the constant rate slope line to intersect the horizontal axis.

2) Determine the maximum load point and draw a line perpendicular to the horizontal axis through this point to intersect the horizontal axis.

3) From the point determined in (1) to the point determined in (2), read and record the flow as a whole number in 0.01" increments.

4) Average the flow values for each asphalt content set and record to the nearest whole number.

14. Determination of Optimum Asphalt Content

A mix that will satisfy a specific project. There are some considerations for adjustment that should be evaluated prior to 1. Graphical Presentation:

Prepare a graphical plot of Asphalt Content vs. Unit Mass, Stability, Flow, Percent Voids Total Mix, Percent Voids in Mineral Aggregate, and Percent Voids Filled with a smooth curve that represents a best-fit for all values.

14.1 Determination of Optimum Asphalt Content:

a. Determination of Preliminary Optimum Asphalt Content: Choose the preliminary optimum asphalt content at the median of the Voids in Total Mix specification. All of the calculated and measured mix properties should then be evaluated by comparing them to the project mix design specifications. If all of the specifications are met, then this is the preliminary optimum asphalt content. If all of the specifications are not met, then some adjustment or compromise is necessary or the mix may need to be redesigned. Even if all of the specifications are met, a number of considerations should be weighed before choosing the final optimum asphalt content.

b. Selection of Final Mix Optimum Asphalt Content: The final optimum asphalt content should be a compromise selected to balance all of the mix properties. Normally, the mix design specifications will produce a narrow range of acceptable asphalt contents that will pass all specifications. The asphalt content selection can be adjusted within this narrow range to achieve establishing the final optimum asphalt content. These are covered in detail in Asphalt Institute Manual MS-2, 6th Edition, Mix Design Methods, Chapter 5, Marshall Mix Design Method, Section D-5.15, Selection of Final Mix Design, pages 69 thru 77.

If this evaluation reveals no asphalt content which meets all project specifications or such a narrow range of asphalt contents meeting all project specifications as to be unfeasible and/or uneconomical to produce, the Materials Engineer may reject the proposed job mix design and require a new proposal from the contractor.

15. Report

The report shall include the following:

- Project identification, Source/Supplier of mix and General Contractor Name.
- Aggregate quality identification(s), target gradation, blend ratio of individual stockpiles, blended bulk specific and effective specific gravities. Other properties that may be specified in the Contract such as: fineness modulus of the blended fine aggregate; percent fracture; percent flat and elongated; and the plasticity index of the blended fine aggregate.
- Asphalt binder quality identification, specific gravity at 77°F, the maximum mixing temperature, and the compaction temperature range.
- Anti-strip additive brand/type and the minimum percent required.
- Asphalt content at the median of the percent voids in total mix specification and the approved optimum asphalt content.
- The following properties at the optimum asphalt content: maximum specific gravity, percent voids in total mix, percent voids in mineral aggregate, percent voids filled, stability, flow, unit mass and the dust-asphalt ratio.
- Graphical representation on a 0.45 power graph of the target gradation with the LSL-USL.
- Graphical representation of asphalt content versus the following properties: unit mass, stability, flow, percent voids in total mix, percent voids in mineral aggregate and voids filled.
- Identification and address of the laboratory that performed the mix design, that laboratories mix design identification number and the signature/title of the professional engineer who reviewed and approved/disapproved the mix design.

Attachment ATM 417

Example Calculations

(See Example Worksheets)

Contractor Proposed JMF for a Type IIA ACP Mix Design

Sieve	Percent Pass.
3/4"	100
1/2"	83
3/8"	69
#4	50
#8	36
#16	26
#30	18
#50	11
#100	7
#200	4.7

Note: Nominal Maximum Size of this material is 3/4 inch.

1. Preparation of Aggregate

1.1 Initial total aggregate mass: $E_i = 1175.0$ g

Calculate cumulative aggregate batch mass by:

$$\text{for No. 4} = \frac{100 - 50}{100} \text{ x } 1175.0 = 587.5 \text{ g}$$

$$x = \frac{100 - \text{Percent PASS}}{100} \times E_i \qquad \text{for No. 8} = \frac{100 - 36}{100} \text{ x } 1175.0 = 752.0 \text{ g}$$

$$\text{for No. 200} = \frac{100 - 4.7}{100} \text{ x } 1175.0 = 1119.8 \text{ g}$$

Repeat for the other required sieve sizes.

1.2 Aggregate Dust Correction

a. Determine the masses for the dust correction gradation by subtracting the initial cumulative mass for the No. 4 sieve from each of the minus No. 4 sieve sizes initial cumulative mass.

X_N Initial Cumulative Mass - No. 4 Initial Cumulative Mass

= X_N Dust Correction Gradation Initial Cumulative Mass

For No. 8: 752.0 - 587.5 = 164.5 g

For No. 200: 1119.8 -587.5 = 532.3 g

Repeat for the other required sieve sizes.

c. Compute the adjusted cumulative batch masses for each of the fine aggregate sieves by:

Pre-wash cumulative batch mass, g		Post-wash cumulative batch mass, g
No. 8	164.5	160.6
No. 200	532.3	521.9

Adjusted cumulative batch masses of each of the fine aggregate sieve calculations:

$$Z_{ni} = \frac{X^2}{Y} + M_4 \quad \text{or}$$

$$Z_{8i} = \frac{164.5^2}{160.6} + 587.5 = 756.0 \text{ g}$$

$$Z_{200i} = \frac{532.3^2}{521.9} + 587.5 = 1130.4 \text{ g}$$

Repeat for the other required sieve sizes.

2. Estimate Projected Optimum Asphalt Content

2.1 Assuming that no experience with the current sources or contractor is available, the projected optimum and minimum asphalt content will be estimated by both the computational formula and dust/asphalt methods.

b. Computational Formula

P = 0.035a + 0.045b +Kc + F

= 0.035 (100 - 36) + 0.045 (36 - 5) + (0.20 x 4.7) + 0.7

= 5.3, round to 5.5%

Test specimens will be prepared and tested at 4.5 to 6.5 percent binder contents.

c. Dust/Asphalt Ratio

$$P = \left(\frac{\text{p200}}{\text{max . D / A}} \right) = 4.7 / 1.2 = 3.9, \text{ round to 4.0 percent}$$

Test specimens will be prepared and tested at 4.0 to 6.0 percent binder contents.

Since the two methods give slightly different ranges, specimens should be prepared and tested at 4.0 to 6.5 percent binder contents.

3. Preparation of Test Specimens

3.1 Thickness Adjustment

The thickness of the trial specimen is 2.48 inches, thus requiring adjustment of the initial aggregate mass by:

$$E_a = \frac{2.5 \times E_i}{H} = \frac{2.5 \text{ x } 1175}{2.48} = 1184.5 \text{ g}$$

3.2 Adjust the final batch mass for each sieve by:

$$\text{For No. 4} = \frac{1184.5}{1175.0} \text{ x } 587.5 = 592.2 \text{ g}$$

$$Z_{Na} = \frac{E_a}{E_i} \times Z_{Ni}$$

$$\text{For No. 8} = \frac{1184.5}{1175.0} \text{ x } 756.0 = 762.1 \text{ g}$$

Repeat for the other required sieve sizes.

3.3 Calculate the mass of the asphalt cement for each set of specimens by:

$$\text{for 4.0 percent} = \frac{1184.5 \text{ x } 4.0}{100 - 4.0} = 49.4 \text{ g}$$

$$AW = \frac{E_i \text{ (or } E_a) \times P_{bN}}{100 - P_{bN}}$$

$$\text{for 6.5 percent} = \frac{1184.5 \text{ x } 6.5}{100 - 6.5} = 82.3 \text{ g}$$

Repeat for the other asphalt contents.

3.4 Calculate the cumulative masses for a maximum specific gravity test specimen by:

$$\text{For No. 4} = \frac{2000}{1175.0} \text{ x } 587.5 = 1000.0 \text{ g}$$

$$R_N = \frac{Q}{E_i} \times Z_{Ni}$$

$$\text{For No. 8} = \frac{2000}{1175.0} \text{ x } 756.0 = 1286.8 \text{ g}$$

Repeat for the other required sieve sizes.

3.5 Coarse Aggregate Properties (such as Specific Gravity, Fracture, Flat-Elongated, Unit Weight, et al)

For each coarse aggregate sieve size, calculate the cumulative mass for the required test specimen(s) of coarse aggregate for the required test procedures by the following formula:

$$C_N = \frac{Q}{\text{No.4 } E_i} \times Z_{Ni}$$

For CA Specific Gravity for No. 4 = 3000 g

$$\text{for 1/2"} = \frac{3000}{587.5} \text{ x } 364.3 = 1860.3 \text{ g}$$

Repeat for the other required sieve sizes.

For Other CA Property Tests substitute the appropriate Q.

3.6 Fine Aggregate Properties (such as Specific Gravity, Sand Equivalent, et al)

For each fine aggregate sieve size, calculate the cumulative masses for the required specimens of fine aggregate specific gravity by the following formula:

$$F_N = \left(\frac{Q}{E_i - Z_{4i}}\right) x \left(Z_{Ni} - Z_{4i}\right)$$

$$\text{No. } 8 = \left(\frac{1000}{1175.0 - 587.5}\right) x \quad (756.0 - 587.5) = 286.8 \text{ g}$$

For FA Specific Gravity for

$$\text{No. } 200 = \left(\frac{1000}{1175.0 - 587.5}\right) x \quad (1130.4 - 587.5) = 924.1 \text{ g}$$

Repeat for the other required sieve sizes.

For Other FA Property Tests substitute the appropriate Q.

4. Calculations

4.1 Calculate the maximum specific gravity for each asphalt content as follows:

a. Calculate the effective specific gravity of the aggregate by:

$$G_{se} = \frac{100 - P_b}{\frac{100}{G_{mm}} - \frac{P_b}{G_b}} = \frac{100 - 5.0}{\frac{100}{2.528} - \frac{5.0}{1.009}} = 2.745$$

b. Calculate the maximum specific gravity for each asphalt content by:

$$G_{mm} = \frac{100}{\frac{100 - P_{bN}}{G_{se}} + \frac{P_{bN}}{G_b}} \qquad \text{For } 4.0\% = \frac{100}{\frac{100 - 4.0}{2.745} + \frac{4.0}{1.009}} = 2.568$$

Repeat for other asphalt contents.

4.2 Calculate the percent air voids in total mix (VTM) for each asphalt content by:

$$VTM = \frac{G_{mm} - G_{mb}}{G_{mm}} x100 \qquad \text{For } 4.0\% = \frac{2.568 - 2.403}{2.568} x100 = 6.4$$

4.3 Calculate the percent voids in mineral aggregate (VMA) for each asphalt content by:

a. Calculate the blended aggregate bulk specific gravity by:

$$G_{sb} = \frac{100}{\frac{P_1}{G_1} + \frac{P_2}{G_2} + \ldots \frac{P_N}{G_N}} = \frac{100}{\frac{50}{2.727} + \frac{50}{2.653}} = 2.689$$

b. Calculate the percent voids in mineral aggregate for each asphalt content by:

$$VMA = 100 - \frac{G_{mb}\ (100 - P_b)}{G_{sb}} \qquad \text{For } 4.0\% = 100 - \frac{2.403\,(100 - 4.0)}{2.689} = 14.2$$

4.4 Calculate the percent voids filled (VFA) with asphalt for each asphalt content by:

$$VFA = 100 \times \frac{VMA - VTM}{VMA} \qquad \text{For } 4.0\% = 100 \text{ x } \frac{14.2 - 6.4}{14.2} = 55$$

4.5 Calculate the dust/asphalt ration for each asphalt content by:

a. Calculate the asphalt absorption by:

$$P_{ba} = 100\left(\frac{G_{se} - G_{sb}}{G_{sb} \times G_{se}}\right)G_b \qquad \text{For } 4.0\% = 100\left(\frac{2.745 - 2.689}{2.689 \text{ x } 2.745}\right)1.009 = 0.77$$

b. Calculate the effective asphalt content for each asphalt content by:

$$P_{be} = P_b - \left(\left(\frac{P_{ba}}{100}\right) \times \left(100 - P_b\right)\right) \qquad \text{For } 4.0\% = 4.0 - \left(\left(\frac{0.77}{100}\right) \times \left(100 - 4.0\right)\right) = 3.3$$

c. Calculate the dust/asphalt ratio by:

$$D/A = \frac{p200}{P_{be}} \qquad \text{For } 4.0\% = \frac{4.7}{3.3} = 1.4$$

4.6 Stability:

c. Correct Stability values for each specimen that differ from the standard 63.5 mm (2.5") thickness by the following:

CS = S x t For Set 1, Specimen 1 = 3145 x 0.976 = 3070

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Rutting Susceptibility using an Asphalt Pavement Analyzer ATM 419

1. Scope

This method describes a procedure for determining the rut susceptibility of hot mix asphalt using an Asphalt Pavement Analyzer (APA).

2. Apparatus

- Asphalt Pavement Analyzer (APA) – A thermostatically controlled device designed to test the rutting susceptibility of hot mix asphalt by applying repetitive linear loads to compacted test specimens through pressurized hoses.
  - The APA shall be thermostatically controlled to maintain the test temperature and conditioning chamber at any set point between 30-60 ± 1°C (85-140 ± 1°F).
  - The APA shall be capable of independently applying loads up to 450 N (100 lbf) to the three wheels. The loads shall be calibrated to the desired test load by a suitable device such as an external force transducer or proving ring.
  - The pressure in the test hoses shall be adjustable and capable of maintaining pressure up to 830 kPa (120 psi).
  - The APA shall be capable of testing six cylindrical specimens simultaneously.
  - The APA shall have a programmable master cycle counter that can be preset to the desired number of cycles for a test. The APA shall be capable to automatically stopping the test at the completion of the programmed number of cycles.
- Balance or scale: Capacity sufficient for the principle sample mass, readable to 0.1 percent or 0.1 g of the total sample mass and meeting the requirements of AASHTO M 231.
- Mixing utensils (bowls, spoon, spatula)
- Ovens and hot plates thermostatically controlled to maintain the various required temperatures within ± 3°C (5°F).
- Compaction device and molds

3. Test Specimens

Number of test specimens – A sample will consist of six 150 mm diameter x 75 mm (6" diameter x 3") cylindrical specimens.

Production Mix

Samples of plant-produced mixtures shall be obtained in accordance with WAQTC FOP for AASHTO T 168. Samples shall be reduced to the appropriate test size in accordance with WAQTC TM 5 and compacted while the mixture is still hot. Reheating of loose plant mixture should be avoided.

Laboratory Prepared Mixtures

Mixture proportions will be batched in accordance to the desired Job Mix Formula. The required batch sizes are determined in accordance to ATM 417, **Preparation of Aggregate and Preparation of Asphalt**. The voids in total mix (VTM) target for the compacted specimens shall be 6.0 + 1.0 percent unless otherwise directed.

The temperature to which the asphalt binder must be heated to achieve a viscosity of 170 ± 20 cSt (0.170 + 0.020 Pa·s) or the mix design mixing temperature shall be the mixing temperature.

Prepare the mixture in accordance with ATM T 417, Preparation of Mixtures and Mixture conditioning. The temperature to which the asphalt binder must be heated to achieve a viscosity of 290 ± 30 cSt (0.290 + 0.030 Pa·s) or the mix design compaction temperature shall be the compaction temperature.

Roadway Core Specimens

Roadway core specimens shall be 150 mm (6") outside diameter with all surfaces of the perimeter perpendicular to the surface of the core within 5 mm (3/16"). Cores shall be trimmed with a wet masonry saw to a height of 75 ± 3 mm (3 ± 1/8"). Final adjustment of the core to the top of the testing molds shall be done with Plaster of Paris.

4. Compaction of Specimens

1 Superpave Gyratory Compaction

- Apparatus (see AASHTO T 312).

a. Compaction of the cylindrical specimens with the Superpave Gyratory Compactor will be performed in such a manner so that the target air void content of 6.0 ± 1.0% is obtained at the specified height of 75 ± 3 mm.

b. Remove the mold and base plate from the oven set at the compaction temperature. Place a paper disc in the bottom of the mold assembly.

c. Transfer the mixture to the mold with care to avoid segregation of the mixture.

d. Place the mold and mixture in the Superpave Gyratory Compactor and begin compaction as described in the compactor's operation manual.

e. When the compaction procedure is completed, remove the mold and compacted specimen from the compactor. Extrude the specimen from the mold with care to avoid distorting the specimen until it is cooled.

f. Compacted specimens should be left at room temperature (about 25°C or 77°F) and allowed to cool overnight.

5. Determining the Voids Total Mix

1. Determine the bulk specific gravity of the test specimens in accordance with WAQTC FOP for AASHTO T 166, Method A.
2. Determine the maximum specific gravity of the test mixture in accordance with WAQTC FOP for AASHTO T 209.
3. Determine the air void contents of the test specimens in accordance with AASHTO T 269.

6. Test Temperature

The test temperature shall be 105°F unless otherwise directed.

7. Initial Measurements

2 Place the rut depth measurement template over the specimen. Take initial measurements on three locations of each specimen. Record the measurement for each location to the nearest 0.01 mm.

8. Specimen Conditioning

1. Stabilize the testing chamber temperature at 105°F or as directed.

2. Place the test specimens into the testing molds and secure in the APA.

3 Push the sample holding tray in and secure. Close chamber doors.

4 Allow specimens to condition at the test temperature for 90 minutes.

5 Set PRESET COUNTER to 8000 cycles.

6 Start the testing. A complete test will take approximately 3.5 hours. At the end of the test cycle, the APA will stop.

7 Open the chamber doors, unlock and pull out the sample holding tray.

8 Remove specimens from the testing molds and take rut-depth measurements in the same manner as the **Initial Measurements**.

9. Calculations

The rut depth at each location is determined by subtracting the final measurement from the initial measurement.

Determine the average rut depth for each specimen, use the average of all measurements to calculate the average rut depth.

The APA rut depth for the mixture is the average of six cylindrical specimens unless otherwise directed.

10. Report

The test report shall include the following information:

- The laboratory name and date of test.
- The mixture type and description.
- The average rut depth to the nearest 0.1 mm.

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SAMPLING FRESHLY MIXED CONCRETE
WAQTC TM 2

Scope

This method covers procedures for obtaining representative samples of fresh concrete delivered to the project site and on which tests are to be performed to determine compliance with quality requirements of the specifications under which concrete is furnished. The method includes sampling from stationary, paving and truck mixers, and from agitating and non-agitating equipment used to transport central mixed concrete. Sampling concrete may involve hazardous materials, operations, and equipment. This standard does not purport to address all of the safety problems associated with its use. It is the responsibility of the user of this standard to establish appropriate safety and health practices.

This method also covers the procedure for preparing a sample of concrete for further testing where it is necessary to remove aggregate larger than the designated size for the test method being performed. The removal of large aggregate particles is accomplished by wet sieving.

Apparatus

- Wheelbarrow
- Cover for wheelbarrow (plastic, canvas, or burlap)
- Buckets
- Shovel
- Cleaning equipment: including scrub brush, rubber gloves, water
- Apparatus for wet sieving including a sieve or sieves conforming to AASHTO M92 of suitable size and conveniently arranged and supported so that the sieve can be shaken rapidly by hand.

Procedure

1. Use every precaution in order to obtain samples representative of the true nature and condition of the concrete being placed being careful not to obtain samples from the very first or very last portions of the batch. The size of the sample will be 1.5 times the volume of concrete required for the specified testing, but not less than 0.03 m^3 (1 ft^3).
   Note 1: Sampling should normally be performed as the concrete is delivered from the mixer to the conveying vehicle used to transport the concrete to the forms; however, specifications may require other points of sampling, such as at the discharge of a concrete pump.

- **Sampling from stationary mixers, except paving mixers**

  Sample the concrete after a minimum of 1/2 m^3 (1/2 yd^3) of concrete has been discharged. Perform sampling by passing a receptacle completely through the discharge stream, or by completely diverting the discharge into a sample container. Take care not to restrict the flow of concrete from the mixer, container, or transportation unit so as to cause segregation. These requirements apply to both tilting and nontilting mixers.

- **Sampling from paving mixers**

Sample after the contents of the paving mixer have been discharged. Obtain material from at least five different locations in the pile and combine into one test sample. Avoid contamination with subgrade material or prolonged contact with absorptive subgrade. To preclude contamination or absorption by the subgrade, the concrete may be sampled by placing a shallow container on the subgrade and discharging the concrete across the container.

- **Sampling from revolving drum truck mixers or agitators**

  Sample the concrete after a minimum of 1/2 m^3 (1/2 yd^3) of concrete has been discharged. Do not obtain samples until after all of the water has been added to the mixer. Do not obtain samples from the very first or last portions of the batch discharge. Sample by repeatedly passing a receptacle through the entire discharge stream or by completely diverting the discharge into a sample container. Regulate the rate of discharge of the batch by the rate of revolution of the drum and not by the size of the gate opening.

- **Sampling from open-top truck mixers, agitators, non-agitating equipment or other types of open-top containers**

  Sample by whichever of the procedures described above is most applicable under the given conditions.

- **Sampling from pump or conveyor placement systems**

  Sample after a minimum of 1/2 m^3 (1/2 yd^3) of concrete has been discharged. Do not obtain samples until after all of the pump slurry has been eliminated. Sample by repeatedly passing a receptacle through the entire discharge system or by completely diverting the discharge into a sample container. Do not lower the pump arm from the placement position to ground level for ease of sampling, as it may modify the air content of the concrete being sampled. Do not obtain samples from the very first or last portions of the batch discharge.

2. Transport samples to the place where fresh concrete tests are to be performed and specimens are to be molded. They shall then be combined and remixed with a shovel the minimum amount necessary to ensure uniformity. Protect the sample from direct sunlight, wind, rain, and sources of contamination.
3. Complete test for temperature and start tests for slump and air content within 5 minutes of obtaining the sample. Complete tests as expeditiously as possible. Start molding specimens for strength tests within 15 minutes of obtaining the sample.

Wet Sieving

When required for slump testing, air content testing or molding test specimens the concrete sample shall be wet-sieved, after transporting but prior to remixing, by the following.

1. Place the sieve designated by the test procedure over dampened sample container.
2. Pass the concrete over the designated sieve. Do not overload the sieve (one particle thick).
3. Shake or vibrate the sieve until no more material passes the sieve. A horizontal back and forth motion is preferred.
4. Discard oversize material including all adherent mortar.
5. Repeat until sample of sufficient size is obtained. Mortar adhering to the wet-sieving equipment shall be included with the sample.

6. Remix the sample with a shovel the minimum amount necessary to ensure uniformity.

Note 2: Wet-sieving is not allowed for samples being utilized for density determinations according to the FOP for AASHTO T 121.

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TEMPERATURE OF FRESHLY MIXED PORTLAND CEMENT CONCRETE
WAQTC FOP FOR AASHTO T 309

Scope

This procedure covers the determination of the temperature of freshly mixed portland cement concrete in accordance with AASHTO T 309.

Apparatus

- Container — The container shall be made of nonabsorptive material and large enough to provide at least 75 mm (3 in.) of concrete in all directions around the sensor; concrete cover must also be a least three times the nominal maximum size of the coarse aggregate.
- Temperature Measuring Device — The temperature measuring device shall be calibrated and capable of measuring the temperature of the freshly mixed concrete to ±0.5°C (±1°F) throughout the temperature range likely to be encountered. Partial immersion liquid-in-glass thermometers (and possibly other types) shall have a permanent mark to which the device must be immersed without applying a correction factor.
- Reference Temperature Measuring Device — The reference temperature measuring device shall be a liquid-in-glass thermometer readable to 0.2°C (0.5°F) that has been verified and calibrated. The calibration certificate or report indicating conformance to the requirements of ASTM E 77 shall be available for inspection.

Calibration of Temperature Measuring Device

Each temperature measuring device shall be verified for accuracy annually and whenever there is a question of accuracy. Calibration shall be performed by comparing readings on the temperature measuring device with another calibrated instrument at two temperatures at least 15°C or 27°F apart.

Sample Locations and Times

The temperature of freshly mixed concrete may be measured in the transporting equipment, in forms, or in sample containers, provided the sensor of the temperature measuring device has at least 75 mm (3 in.) of concrete cover in all direction around it.

Complete the temperature measurement of the freshly mixed concrete within 5 minutes of obtaining the sample.

Concrete containing aggregate of a nominal maximum size greater than 75 mm (3 in.) may require up to 20 minutes for the transfer of heat from the aggregate to the mortar after batching.

Procedure

1. Dampen the sample container.

2. Obtain the sample in accordance with the FOP for WAQTC TM 2.

3. Place sensor of the temperature measuring device in the freshly mixed concrete so that it has at least 75 mm (3 in.) of concrete cover in all directions around it.

4. Gently press the concrete in around the sensor of the temperature measuring device at the surface of the concrete so that air cannot reach the sensor.

5. Leave the sensor of the temperature measuring device in the freshly mixed concrete for a minimum of two minutes, or until the temperature reading stabilizes.

6. Complete the temperature measurement of the freshly mixed concrete within 5 minutes of obtaining the sample.

7. Read and record the temperature to the nearest 0.5°C (1°F).

Report

Results shall be reported on standard forms approved for use by the agency. Record the measured temperature of the freshly mixed concrete to the nearest 0.5°C (1°F).

SLUMP OF HYDRAULIC CEMENT CONCRETE
WAQTC FOP FOR AASHTO T 119

Scope

This procedure provides instructions for determining the slump of hydraulic cement concrete in accordance with AASHTO T 119. It is not applicable to non-plastic and non-cohesive concrete. With concrete using 37.5mm (1½ in.) or larger aggregate, the +37.5mm (1½ in.) aggregate must be removed in accordance with the FOP for WAQTC TM 2.

Apparatus

- Mold: The metal mold shall be provided with foot pieces and handles. The mold must be constructed without a seam. The interior of the mold shall be relatively smooth and free from projections such as protruding rivets. The mold shall be free from dents. A mold that clamps to a rigid nonabsorbent base plate is acceptable provided the clamping arrangement is such that it can be fully released without movement of the mold.
- Mold: Other than metal must conform to AASHTO T 119 Sections 5.1.1.1 & 5.1.1.2.
- Tamping rod: 16 mm (5/8 in.) diameter and approximately 600 mm (24 in.) long, having a hemispherical tip. (Hemispherical means "half a sphere"; the tip is rounded like half of a ball.)
- Scoop
- Tape measure or ruler with at least 5 mm or 1/8 in. graduations
- Base: Flat, rigid, non-absorbent moistened surface on which to set the slump cone

Procedure

1. Obtain the sample in accordance with FOP for WAQTC TM 2. If any aggregate 37.5mm (1½ in.) or larger aggregate is present, aggregate must be removed in accordance with the Wet Sieving portion of the FOP for WAQTC TM 2.

   Note 1: Testing shall begin within five minutes of obtaining the sample.

2. Dampen the inside of the cone and place it on a dampened, rigid, nonabsorbent surface that is level and firm.
3. Stand on both foot pieces in order to hold the mold firmly in place.
4. Fill the cone 1/3 full by volume, to a depth of approximately 67 mm (2 5/8 in.) by depth.
5. Consolidate the layer with 25 strokes of the tamping rod, using the rounded end. Distribute the strokes evenly over the entire cross section of the concrete. For this bottom layer, incline the rod slightly and make approximately half the strokes near the perimeter, and then progress with vertical strokes, spiraling toward the center.
6. Fill the cone 2/3 full by volume, to a depth of approximately 155 mm (6 1/8 in.) by depth.
7. Consolidate this layer with 25 strokes of the tamping rod, just penetrating into the bottom layer. Distribute the strokes evenly.
8. Fill the cone to overflowing.

9. Consolidate this layer with 25 strokes of the tamping rod, just penetrating into the second layer. Distribute the strokes evenly. If the concrete falls below the top of the cone, stop, add more concrete, and continue rodding for a total of 25 strokes. Keep an excess of concrete above the top of the mold at all times. Distribute strokes evenly as before.
10. Strike off the top surface of concrete with a screeding and rolling motion of the tamping rod.
11. Clean overflow concrete away from the base of the mold.
12. Remove the mold from the concrete by raising it carefully in a vertical direction. Raise the mold 300 mm (12 in.) in 5 ±2 seconds by a steady upward lift with no lateral or torsional motion being imparted to the concrete.

    The entire operation from the start of the filling through removal of the mold shall be carried out without interruption and shall be completed within an elapsed time of 2 1/2 minutes. Immediately measure the slump by:
13. Invert the slump cone and set it next to the specimen.
14. Lay the tamping rod across the mold so that it is over the test specimen.
15. Measure the distance between the bottom of the rod and the displaced original center of the top of the specimen to the nearest 5 mm (1/4 in.).

    Note 2: If a decided falling away or shearing off of concrete from one side or portion of the mass occurs, disregard the test and make a new test on another portion of the sample. If two consecutive tests on a sample of concrete show a falling away or shearing off of a portion of the concrete from the mass of the specimen, the concrete probably lacks the plasticity and cohesiveness necessary for the slump test to be applicable.

Report

Results shall be reported on standard forms approved for use by the agency. Record the slump to the nearest 5 mm (1/4 in.).

DENSITY (UNIT WEIGHT), YIELD, AND AIR CONTENT (GRAVIMETRIC) OF CONCRETE

(See Addendum for DOT&PF Guidelines)

WAQTC FOP FOR AASHTO T 121

Scope

This procedure covers the determination of density, or unit weight, of freshly mixed concrete in accordance with AASHTO T 121. It also provides formulas for calculating the volume of concrete produced from a mixture of known quantities of component materials, and provides a method for calculating cement content& cementitious material content – the mass of cement or cementitious material per unit volume of concrete. A procedure for calculating water/cement ratio is also covered.

Apparatus

- Measure: May be the bowl portion of the air meter used for determining air content under the FOP for AASHTO T 152. Otherwise, it shall be a metal cylindrical container meeting the requirements of AASHTO T 121. The capacity and dimensions of the measure shall conform to those specified in Table 1.
- Balance or scale: Accurate to 0.3 percent of the test load at any point within the range of use.
- Tamping Rod: 16 mm (5/8 in.) diameter and approximately 600 mm (24 in.) long, having a hemispherical tip. (Hemispherical means "half a sphere"; the tip is rounded like half of a ball.)
- Vibrator: 7000 vibrations per minute, 19 to 38 mm (3/4 to 1 1/2 in.) in diameter, and the length of the shaft shall be at least 610 mm (24in).
- Scoop
- Strike-off Plate: A flat rectangular metal plate at least 6 mm (1/4 in.) thick or a glass or acrylic plate at least 12 mm (1/2 in.) thick, with a length and width at least 50 mm (2 in.) greater than the diameter of the measure with which it is to be used. The edges of the plate shall be straight and smooth within tolerance of 1.5 mm (1/16 in.).
- Mallet: With a rubber or rawhide head having a mass of 0.57 ±0.23 kg (1.25 ±0.5 lb) for use with measures of 0.014 m^3 (1/2 ft^3) or less, or having a mass of 1.02 ±0.23 kg (2.25 ±0.5 lb) for use with measures of 0.028 m^3 (1 ft^3).

Table 1
Dimensions of Measures

Capacity m^3 (ft^3)	Inside Diameter mm (in.)	Inside Height mm (in.)	Minimum Thicknesses mm(in.) Bottom	Wall	Nominal Maximum Size of Coarse Aggregate** mm (in.)
0.0071	203 ±2.54	213 ±2.54	5.1	3.0	25
(1/4)*	(8.0 ±0.1)	(8.4 ±0.1)	(0.20)	(0.12)	(1)
0.0142	254 ±2.54	279 ±2.54	5.1	3.0	50
(1/2)	(10.0 ±0.1)	(11.0 ±0.1)	(0.20)	(0.12)	(2)
0.0283	356 ±2.54	284 ±2.54	5.1	3.0	76
(1)	(14.0 ±0.1)	(11.2 ±0.1)	(0.20)	(0.12)	(3)

* Note: Measure may be the base of the air meter used in the FOP for AASHTO T 152.
** Nominal Maximum size: One sieve larger than the first sieve to retain more than 10 percent of the material using an agency specified set of sieves based on cumulative percent retained. Where large gaps in specification sieves exist, intermediate sieve(s) may be inserted to determine nominal maximum size.

Calibration of Measure

1. Determine the mass of the dry measure and strike-off plate.
2. Fill the measure with water at a temperature between 16°C and 29°C (60°F and 85°F) and cover with the strike-off plate in such a way as to eliminate bubbles and excess water.
3. Wipe the outside of the measure and cover plate dry, being careful not to lose any water from the measure.
4. Determine the mass of the measure, strike-off plate, and water in the measure.
5. Determine the mass of the water in the measure by subtracting the mass in Step 1 from the mass in Step 4.
6. Measure the temperature of the water and determine its density from Table 2, interpolating as necessary.
7. Calculate the volume of the measure, V_m, by dividing the mass of the water in the measure by the density of the water at the measured temperature, from Table 2.

   Example: at 23°C (73.4°F)

$$V_m = \frac{7.062\,\text{kg}}{997.54\,\text{kg/m}^3} = 0.007079\,\text{m}^3$$

$$V_m = \frac{15.53\,lb}{62.274\,lb/\text{ft}^3} = 0.2494\,ft^3$$

Table 2
Unit Mass of Water
15°C to 30°C

°C	(°F)	kg/m^3	(lb/ft^3)	°C	(°F)	kg/m^3	(lb/ft^3)
15	(59.0)	999.10	(62.372)	23	(73.4)	997.54	(62.274)
15.6	(60.0)	999.01	(62.366)	23.9	(75.0)	997.32	(62.261)
16	(60.8)	998.94	(62.361)	24	(75.2)	997.29	(62.259)
17	(62.6)	998.77	(62.350)	25	(77.0)	997.03	(62.243)
18	(64.4)	998.60	(62.340)	26	(78.8)	996.77	(62.227)
18.3	(65.0)	998.54	(62.336)	26.7	(80.0)	996.59	(62.216)
19	(66.2)	998.40	(62.328)	27	(80.6)	996.50	(62.209)
20	(68.0)	998.20	(62.315)	28	(82.4)	996.23	(62.192)
21	(69.8)	997.99	(62.302)	29	(84.2)	995.95	(62.175)
21.1	(70.0)	997.97	(62.301)	29.4	(85.0)	995.83	(62.166)
22	(71.6)	997.77	(62.288)	30	(86.0)	995.65	(62.156)

Procedure Selection

There are two methods of consolidating the concrete – rodding and vibration. If the slump is greater than 75 mm (3 in.), consolidation is by rodding. When the slump is 25 to 75 mm (1 to 3 in.), internal vibration or rodding can be used to consolidate the sample, but the method used must be that required by the agency in order to obtain consistent, comparable results. For slumps less than 25 mm (1 in.), consolidate the sample by internal vibration.

Procedure – Rodding

1. Obtain the sample in accordance with the FOP for WAQTC TM 2. Testing may be performed in conjunction with the FOP for AASHTO T 152. When doing so, this FOP should be performed prior to the FOP for AASHTO T 152.

   Note 1: If the two tests are being performed using the same sample, this test shall begin within five minutes of obtaining the sample.

2. Determine the mass of the dry empty measure.
3. Dampen the inside of the measure.
4. Fill the measure approximately 1/3 full with concrete.
5. Consolidate the layer with 25 strokes of the tamping rod, using the rounded end. Distribute the strokes evenly over the entire cross section of the concrete. Rod throughout its depth without hitting the bottom too hard.
6. Tap the sides of the measure smartly 10 to 15 times with the mallet to close voids and release trapped air.
7. Add the second layer, filling the measure about 2/3 full.
8. Consolidate this layer with 25 strokes of the tamping rod, penetrating about 25 mm (1 in.) into the bottom layer.
9. Tap the sides of the measure smartly 10 to 15 times with the mallet.
10. Add the final layer, slightly overfilling the measure.

11. Consolidate this layer with 25 strokes of the tamping rod, penetrating about 25 mm (1 in.) into the second layer.
12. Tap the sides of the measure smartly 10 to 15 times with the mallet.

    Note 2: The measure should be slightly over full, about 3 mm (1/8 in.) above the rim. If there is a great excess of concrete, remove a portion with the scoop. If the measure is under full, add a small quantity. This adjustment may be done only after consolidating the final layer and before striking off the surface of the concrete.

13. Strike off by pressing the strike-off plate flat against the top surface covering approximately 2/3 of the measure. Withdraw the strike-off plate with a sawing motion to finish the 2/3 originally covered. Cover the original 2/3 again with the plate; finishing the remaining 1/3 with a sawing motion (do not lift the plate, continue the sawing motion until the plate has cleared the surface of the measure). Final finishing may be accomplished with several strokes with the inclined edge of the strike-off plate. The surface should be smooth and free of voids.
14. Clean off all excess concrete from the exterior of the measure including the rim.
15. Determine and record the mass of the measure and the concrete to the nearest 0.3%.
16. If the air content of the concrete is to be determined, proceed to Rodding Procedure Step 13 of the FOP for AASHTO T 152.

Procedure - Internal Vibration

1. Perform Steps 1 through 3 of the rodding procedure.
2. Fill the measure approximately half full.
3. Insert the vibrator at four different points in each layer when a 0.0283 m^3 (1 ft^3) measure is used, and three different points in each layer when a 0.0142 m^3 (1/2 ft^3), or smaller, measure is used. Do not let the vibrator touch the bottom or sides of the measure.

    Note 3: Remove the vibrator slowly, so that no air pockets are left in the material.

    Note 4: Continue vibration only long enough to achieve proper consolidation of the concrete. Over vibration may cause segregation and loss of appreciable quantities of intentionally entrained air.

4. Fill the measure a bit over full.
5. Insert the vibrator as in Step 3. Do not let the vibrator touch the sides of the measure, but do penetrate the first layer approximately 25 mm (1 in.).
6. Return to Step 13 of the rodding procedure and continue.

Calculations

- **Density** – Calculate the net mass, M_m, of the concrete in the measure by subtracting the mass of the measure from the gross mass of the measure plus the concrete. Calculate the density, W, by dividing the net mass, M_m, by the volume, V_m, of the measure as shown below.

$$W = \frac{M_m}{V_m} \quad \text{Example: } W = \frac{16.920\,\text{kg}}{0.007079\,\text{m}^3} = 2390\,\text{kg/m}^3 \qquad W = \frac{36.06\,lb}{0.2494\,ft^3} = 144.6\,lb/\text{ft}^3$$

- **Yield** – Calculate the yield, Y, or volume of concrete produced per batch, by dividing the total mass of the batch, W_1, by the density , W, of the concrete as shown below.

$$Y = \frac{W_1}{W} \quad \text{Example: } Y = \frac{2436\,\text{kg}}{2390\,\text{kg/m}^3} = 1.02\,\text{m}^3 \qquad Y = \frac{3978\,lb}{(27)(144.6\,\text{lb/ft}^3)} = 1.02\,yd^3$$

Note 5: The total mass, W_1, includes the masses of the cement, water, and aggregates in the concrete.

- **Cement Content** – Calculate the actual cement content, N, by dividing the mass of the cement, N_t, by the yield, Y, as shown below.

Note 6: Specifications may require Portland cement content and cementitious materials content

$$N = \frac{N_t}{Y} \quad \text{Example: } N = \frac{261\,\text{kg}}{1.02\,\text{m}^3} = 256\,\text{kg/m}^3 \qquad N = \frac{602\,lb}{1.02\,\text{yd}^3} = 590\,lb/\text{yd}^3$$

- **Water Content** – Calculate the mass of water in a batch of concrete by summing the:
  - water added at batch plant
  - water added in transit
  - water added at jobsite
  - free water on coarse aggregate
  - free water on fine aggregate
  - liquid admixtures (if the agency requires this to be included).

This information is obtained from concrete batch tickets collected from the driver. Use the following conversion factors.

Table 3

To Convert From	To	Multiply By
Liters, L	Kilograms, kg	1.0
Gallons, gal	Kilograms, kg	3.785
Gallons, gal	Pounds, lb	8.34
Milliliters, mL	Kilograms, kg	0.001
Ounces, oz	Milliliters, mL	28.4
Ounces, oz	Kilograms, kg	0.0284
Ounces, oz	Pounds, lb	0.0625
Pounds, lb	Kilograms, kg	0.4536

Calculate the mass of free water on aggregate as follows.

$$\text{Free Water Mass} = \text{Total Aggregate Mass} - \frac{\text{Total Aggregate Mass}}{1 + (\text{Free Water Percentage}/100)}$$

Example:

Total Aggregate Mass = 3540 kg(7804 lb)
Free Water Percentage = 1.7*

* To determine Free Water percentage
Total moisture content of the aggregates – absorbed moisture = Free Water

$$\text{Free Water Mass} = 3540\,\text{kg} - \frac{3540\,\text{kg}}{1+(1.7/100)} = 59\,\text{kg} \qquad 7804\,lb - \frac{7804\,lb}{1+(1.7/100)} = 130\,lb$$

Example for actual water content:

Water added at batch plant =	300 L	79 gal	
Water added in transit =	0 L		
Water added at jobsite =	40 L	11 gal	
	340 L = 340 kg	90 gal =	751 lbs

Coarse aggregate: 3540 kg (7804 lbs) @ 1.7% free water
Fine aggregate: 2490 kg (5489 lb) @ 5.9% free water

CA free water = $3540\ \text{kg} - \frac{3540\ \text{kg}}{1 + (1.7/100)} = 59\ \text{kg}$ $\quad 7804\,lb - \frac{7804\ lb}{1 + (1.7/100)} = 130\ \text{lbs}$

FA free water = $2490\ \text{kg} - \frac{2490\ \text{kg}}{1 + (5.9/100)} = \underline{139\ \text{kg}}$ $\quad 5489\,lb - \frac{5489\,lb}{1 + (5.9/100)} = \underline{306\ \text{lbs}}$

Mass of water in batch = 538 kg 1187 lbs

- **Water/Cement Ratio** – Calculate the water/cement ratio by dividing the mass of water in a batch of concrete by the mass of cementitious material in the batch. The masses of the cementitious materials are obtained from concrete batch tickets collected from the driver.

  Example:

Cement:	950 kg	2094 lb
Fly Ash:	180 kg	397 lb
Water:	538 kg (from previous example)	1187 lb

$$W/C = \frac{538\,\text{kg}}{(950+180\,\text{kg})} = 0.476\text{, say } 0.48 \qquad W/C = \frac{1187\,lb}{(2094+397\,lb)} = 0.48$$

Report

Results shall be reported on standard forms approved for use by the agency and should include the following:

Density (unit weight) to 1 kg/m^3 (0.1 lb/ft^3)

Yield to 0.01 m^3 (0.01 yd^3),

Cement content to 1 kg/m^3 (1 lb/yd^3)

Cementitious material content to 1 kg/m^3 (1 lb/yd^3)

Water/Cement ratio to 0.01

Addendum WAQTC FOP for AASHTO T 121

Following are guidelines for the use of WAQTC FOP for AASHTO T 121 by the State of Alaska DOT&PF.

1. Calibration shall be done in accordance with Standard Practice 9.
2. Under the Heading of Procedure – Rodding, reverse steps 2 and 3.
3. Report the volume of the measure to 0.000001 m^3 (0.0001 ft^3).

AIR CONTENT OF FRESHLY MIXED CONCRETE BY THE PRESSURE METHOD WAQTC FOP FOR AASHTO T 152 (See Addendum for DOT&PF Guidelines)

Scope

This procedure covers determination of the air content in freshly mixed Portland Cement Concrete containing dense aggregates in accordance with AASHTO T 152, Type B meter. It is not for use with lightweight or highly porous aggregates. This procedure includes calibration of the Type B air meter gauge, and two methods for calibrating the gauge are presented.

Concrete containing aggregate that is 37.5 mm (1 ½") or larger must be wet sieved. Sieve a sufficient amount of the sample over the 37.5 mm (1 ½") sieve in accordance with the wet sieving portion of the FOP for WAQTC TM 2.

Apparatus

- Air meter: Type B, as described in AASHTO T 152
- Balance or scale: Accurate to 0.3 percent of the test load at any point within the range of use (for Method 1 calibration only)
- Tamping rod: 16 mm (5/8 in.) diameter and approximately 600 mm (24 in.) long, having a hemispherical tip. (Hemispherical means "half a sphere"; the tip is rounded like half of a ball.)
- Vibrator: 7000 vibrations per minute, 19 to 38 mm (0.75 to 1.50 in.) in diameter, at least 75 mm (3 in.) longer than the section being vibrated for use with low slump concrete
- Scoop
- Container for water: rubber syringe (may also be a squeeze bottle)
- Strike-off bar: Approximately 300 mm x 22 mm x 3 mm (12 in. x 3/4 in. x 1/8 in.)
- Strike-off Plate: A flat rectangular metal plate at least 6 mm (1/4 in.) thick or a glass or acrylic plate at least 12 mm (1/2 in.) thick, with a length and width at least 50 mm (2 in.) greater than the diameter of the measure with which it is to be used. The edges of the plate shall be straight and smooth within tolerance of 1.5 mm (1/16 in.).

  Note 1: Use either the strike-off bar or strike-off plate; both are not required.

- Mallet: With a rubber or rawhide head having a mass of 0.57 ±0.23 kg (1.25 ±0.5 lb)

Calibration of Air Meter Gauge

Note 2: There are two methods for calibrating the air meter, mass or volume.

1. Screw the short piece of straight tubing into the threaded petcock hole on the underside of the cover. Determine the mass of the dry, empty air meter bowl and cover assembly (Mass Method only).
2. Fill the bowl nearly full with water.
3. Clamp the cover on the bowl with the tube extending down into the water. Mark the petcock with the tube attached for future reference.
4. Add water through the petcock having the pipe extension below until all air is forced out the other petcock. Rock the meter slightly until all air is expelled through the petcock.

5. Wipe off the air meter bowl and cover assembly, and determine the mass of the filled unit (Mass Method only).
6. Pump up the air pressure to a little beyond the predetermined initial pressure indicated on the gauge. Wait a few seconds for the compressed air to cool, and then stabilize the gauge hand at the proper initial pressure by pumping up or relieving pressure, as needed.
7. Close both petcocks and immediately open the main air valve exhausting air into the bowl. Wait a few seconds until the meter needle stabilizes. The gauge should now read 0 percent. If two or more tests show a consistent variation from 0 percent in the result, change the initial pressure line to compensate for the variation, and use the newly established initial pressure line for subsequent tests.
8. Determine which petcock has the straight tube attached to it. Attach the curved tube to external portion of the same petcock.
9. Pump air into the air chamber. Open the petcock with the curved tube attached to it. Open the main air valve for short periods of time until 5 percent of water by mass or volume has been removed from the air meter. Remember to open both petcocks to release the pressure in the bowl and drain the water in the curved tube back into the bowl. To determine the mass of the water to be removed, subtract the mass found in Step 1 from the mass found in Step 5. Multiply this value by 0.05. This is the mass of the water that must be removed. To remove 5 percent by volume, remove water until the external calibration vessel is level full.

   Note3: Many air meters are supplied with a calibration vessel(s) of known volume that are used for this purpose. Calibration vessel(s) should be brass, not plastic, and must be protected from crushing or denting.
   If an external calibration vessel is used, confirm what percentage volume it represents for the air meter being used. Vessels commonly represent 5 percent volume, but they are for specific size meters. This should be confirmed by mass.

10. Remove the curved tube. Pump up the air pressure to a little beyond the predetermined initial pressure indicated on the gauge. Wait a few seconds for the compressed air to cool, and then stabilize the gauge hand at the proper initial pressure by pumping up or relieving pressure, as needed.
11. Close both petcocks and immediately open the main air valve exhausting air into the bowl. Wait a few seconds until the meter needle is stabilized. The gauge should now read 5.0 ±0.1 percent. If the gauge is outside that range, the meter needs adjustment. The adjustment could involve adjusting the starting point so that the gauge reads 5.0 ±0.1 percent when this calibration is run, or could involve moving the gauge needle to read 5.0 percent. Any adjustment should comply with the manufacturer’s recommendations.

Note 4: Calibration shall be performed at the frequency required by the agency. Record the date of the calibration, the calibration results, and the name of the technician performing the calibration in the log book kept with each air meter.

12. When the gauge hand reads correctly at 5.0 percent, additional water may be withdrawn in the same manner to check the results at other values such as 10 percent or 15 percent.
13. If an internal calibration vessel is used follow steps 1 thru 8 to set initial reading.
14. Release pressure from the bowl and remove cover. Place the internal calibration vessel into the bowl. This will displace 5 percent of the water in the bowl. (See AASHTO 152 for more information on internal calibration vessels.)
15. Place the cover back on the bowl and add water through the petcock until all the air has been expelled.

16. Pump up the air pressure chamber to the initial pressure. Wait a few seconds for the compressed air to cool, and then stabilize the gauge hand at the proper initial pressure by pumping up or relieving pressure, as needed.
17. Close both petcocks and immediately open the main air valve exhausting air into the bowl. Wait a few seconds until the meter needle stabilizes. The gauge should now read 5 percent.

Note 5: Remove the extension tubing from threaded petcock hole in the underside of the cover before starting the test procedure.

Procedure Selection

There are two methods of consolidating the concrete – rodding and vibration. If the slump is greater than 75 mm (3 in.), consolidation is by rodding. When the slump is 25 to 75 mm (1 to 3 in.), internal vibration or rodding can be used to consolidate the sample, but the method used must be that required by the agency in order to obtain consistent, comparable results. For slumps less than 25 mm (1 in.), consolidate the sample by internal vibration.

Procedure – Rodding

1. Obtain the sample in accordance with the FOP for WAQTC TM 2. If any aggregate 37.5mm (1½ in.) or larger is present, aggregate must be removed in accordance with the Wet Sieving portion of the FOP for WAQTC TM 2.

   Note 6: Testing shall begin within five minutes of obtaining the sample.
2. Dampen the inside of the air meter bowl and place on a firm level surface.
3. Fill the bowl approximately 1/3 full with concrete.
4. Consolidate the layer with 25 strokes of the tamping rod, using the rounded end. Distribute the strokes evenly over the entire cross section of the concrete. Rod throughout its depth without hitting the bottom too hard.
5. Tap the sides of the bowl smartly 10 to 15 times with the mallet to close voids and release trapped air.
6. Add the second layer, filling the bowl about 2/3 full.
7. Consolidate this layer with 25 strokes of the tamping rod, penetrating about 25 mm (1 in.) into the bottom layer.
8. Tap the sides of the bowl 10 to 15 times with the mallet.
9. Add the final layer, slightly overfilling the bowl.
10. Consolidate this layer with 25 strokes of the tamping rod, penetrating about 25 mm (1 in.) into the second layer.
11. Tap the sides of the bowl smartly 10 to 15 times with the mallet.

    Note 7: The bowl should be slightly over full, about 3 mm (1/8 in.) above the rim. If there is a great excess of concrete, remove a portion with the trowel or scoop. If the bowl is under full, add a small quantity. This adjustment may be done only after consolidating the final layer and before striking off the surface of the concrete.
12. Strike off the surface of the concrete and finish it smoothly with a sawing action of the strike-off bar or plate, using great care to leave the bowl just full. The surface should be smooth and free of voids.

13. Clean the top flange of the bowl to ensure a proper seal.
14. Moisten the inside of the cover and check to see that both petcocks are open and the main air valve is closed.
15. Clamp the cover on the bowl.
16. Inject water through a petcock on the cover until water emerges from the petcock on the other side.
17. Jar and or rock the air meter gently until no air bubbles appear to be coming out of the second petcock. The petcock expelling water should be higher than the petcock where water is being injected. Return the air meter to a level position and verify that water is present in both petcocks.
18. Close the air bleeder valve and pump air into the air chamber until the needle goes past the initial pressure determined for the gauge. Allow a few seconds for the compressed air to cool.
19. Tap the gauge gently with one hand while slowly opening the air bleeder valve until the needle rests on the initial pressure. Close the air bleeder valve.
20. Close both petcocks.
21. Open the main air valve.
22. Tap the sides of the bowl smartly with the mallet.
23. With the main air valve open, lightly tap the gauge to settle the needle, and then read the air content to the nearest 0.1 percent.
24. Release or close the main air valve.
25. Open both petcocks to release pressure, remove the concrete, and thoroughly clean the cover and bowl with clean water.
26. Open the main air valve to relieve the pressure in the air chamber.

Procedure - Internal Vibration

1. Obtain the sample in accordance with the FOP for WAQTC TM 2. If any aggregate 37.5mm (1½ in.) or larger is present, aggregate must be removed in accordance with the Wet Sieving portion of the FOP for WAQTC TM 2.
2. Dampen the inside of the air meter bowl and place on a firm level surface.
3. Fill the bowl approximately half full.
4. Insert the vibrator at three different points. Do not let the vibrator touch the bottom or sides of the bowl.

   Note 8: Remove the vibrator slowly, so that no air pockets are left in the material.

   Note 9: Continue vibration only long enough to achieve proper consolidation of the concrete. Over vibration may cause segregation and loss of appreciable quantities of intentionally entrained air.

5. Fill the bowl a bit over full.
6. Insert the vibrator as in Step 4. Do not let the vibrator touch the sides of the bowl, and penetrate the first layer approximately 25 mm (1 in.).
7. Return to Step 12 of the rodding procedure and continue.

Report

- Results shall be reported on standard forms approved for use by the agency.
- Record the percent of air to the nearest 0.1 percent.
- Some agencies require an aggregate correction factor in order to determine total % entrained air.

  Total % entrained air = Gauge reading – aggregate correction factor from mix design

  (See AASHTO T 152 for more information.)

Addendum WAQTC FOP for AASHTO T 152

Following are guidelines for the use of WAQTC FOP for AASHTO T 152 by the State of Alaska DOT&PF.

1. Calibration shall be done in accordance with Standard Practice 8.
2. Correction Factors should be checked for each new aggregate source and for sources that have a history of a correction factor in excess of 0.4%.
3. For concrete with a slump at or above 1”, the concrete shall be rodded.

METHOD OF MAKING AND CURING CONCRETE TEST SPECIMENS IN THE FIELD WAQTC FOP FOR AASHTO T 23 (See Addendum for DOT&PF Guidelines)

Scope

This procedure covers the method for making, initially curing, and transporting concrete test specimens in the field in accordance with AASHTO T 23.

Apparatus and Test Specimens

- Concrete cylinder molds: Conforming to AASHTO M 205 with a length equal to twice the diameter. Standard specimens shall be 150 mm (6 in.) by 300 mm (12 in.) cylinders. Mold diameter must be at least three times maximum aggregate size unless wet sieving is conducted according to the FOP for WAQTC TM 2. Agency specifications may allow cylinder molds of 100 mm (4 in.) by 200 mm (8 in.) size when the nominal maximum aggregate size does not exceed 25 mm (1 in.).
- Beam molds: Rectangular in shape with ends and sides at right angles to each other. Must be sufficiently rigid to resist warpage. Surfaces must be smooth. Molds shall produce length no more than 1.6 mm (1/16") shorter than that required (greater length is allowed). Maximum variation from nominal cross section shall not exceed 3.2 mm (1/8 in.). Ratio of width to depth may not exceed 1.5; the smaller dimension must be at least 3 times maximum aggregate size. Unless otherwise noted in specifications, beam molds for casting specimens in the field shall result in specimens having width and depth of not less than 150 mm (6 inches). Specimens shall be cast and hardened with the long axes horizontal.
- Standard tamping rod: 16 mm (5/8 in.) diameter and approximately 600 mm (24 in.) long, having a hemispherical tip for preparing 150mm (6 in.) x 300 mm (12 in.) cylinders.
- Small tamping rod: 10 mm (3/8 in.) diameter and approximately 305 mm (12 in.) long, having a hemispherical tip for preparing 100 mm (4 in.) x 200 mm (8 in.) cylinders.
- Vibrator: At least 7000 vibrations per minute, diameter no more than ¼ the diameter or width of the mold and at least 75 mm (3 in.) longer than the section being vibrated for use with low slump concrete.
- Scoop
- Trowel or Float
- Mallet: With a rubber or rawhide head having a mass of 0.57 ± 0.23 kg (1.25 ±0.5 lb.).
- Rigid base plates and cover plates: metal, glass, or plywood.
- Initial Curing Facilities: Temperature controlled curing box or enclosure capable of maintaining the required range of 16 to 27°C (60 to 80°F) during the entire initial curing period (for concrete with compressive strength of 40 Mpa (6000 psi) or more, the temperature shall be 20 to 26°C (68 to 78°F). As an alternative, sand or earth for initial cylinder protection may be used provided that the required temperature range is maintained and the specimens are not damaged.
- **Thermometer:** Capable of registering both maximum and minimum temperatures during the initial cure.

Procedure – Making Specimens – General

1. Obtain the sample according with the FOP for WAQTC TM 2. Wet Sieving per the FOP for WAQTC TM 2 is required when concrete contains aggregate with a nominal maximum size greater than 50 mm (2 in.) for specimens with a 150 mm (6 in.) diameter, or greater than 25 mm (1 in.) for specimen's with a 100 mm (4 in.) diameter. Sieve the sample for 150 mm (6 in.) diameter specimens over the 37.5mm (1½ in.) sieve and for 100 mm (4 in.) diameter specimens, sieve over the 25mm (1 in.).
2. Remix the sample after transporting to testing location.
3. Begin making specimens within 15 minutes of obtaining the sample.
4. Set molds upright on a level rigid base in a location free from vibration and relatively close to where they will be stored.
5. Fill molds in the required number of layers attempting to exactly fill the mold on the final layer. Add or remove concrete prior to completion of consolidation to avoid a deficiency or excess of concrete.
6. There are two methods of consolidating the concrete – rodding and internal vibration. If the slump is greater than 25 mm (1 in.), consolidation may be by rodding or vibration. When the slump is 25 mm (1 in.) or less, consolidate the sample by internal vibration. Agency specifications may dictate when rodding or vibration will be used.

Procedure – Making Cylinders – Rodding

1. For the standard 150 mm (6 in.) by 300 mm (12 in.) specimen, fill each mold in three approximately equal layers, moving the scoop or trowel around the perimeter of the mold to evenly distribute the concrete. For the 100 mm (4 in.) by 200 mm (8 in.) specimen, fill the mold in two layers. When filling the final layer, slightly overfill the mold.
2. Consolidate each layer with 25 strokes of the appropriate tamping rod, using the rounded end. Distribute strokes evenly over the cross section of the concrete. Rod the first layer throughout its depth without forcibly hitting the bottom. For subsequent layers, rod the layer throughout its depth penetrating approximately 25 mm (1 in.) into the underlying layer.
3. After rodding each layer, tap the sides of each mold 10 to 15 times with the mallet (reusable steel molds) or lightly with the open hand (single-use light-gauge molds).
4. Strike off the surface of the molds with tamping rod, or straightedge and begin initial curing.

Note 1: Floating or troweling is permitted instead of striking off with rod or straightedge

Procedure – Making Cylinders – Internal Vibration

1. Fill the mold in two layers.
2. Insert the vibrator at the required number of different points for each layer (two points for 150 mm (6 in.) diameter cylinders; one point for 100 mm (4 in.) diameter cylinders). When vibrating the bottom layer, do not let the vibrator touch the bottom or sides of the mold. When vibrating the top layer, the vibrator shall penetrate into the underlying layer approximately 25 mm (1 in.)
3. Remove the vibrator slowly, so that no air pockets are left in the material.

Note 2: Continue vibration only long enough to achieve proper consolidation of the concrete. Over vibration may cause segregation and loss of appreciable quantities of intentionally entrained air.

4. Strike off the surface of the molds with tamping rod, or straightedge and begin initial curing.

Procedure – Making Flexural Beams – Rodding

1. Fill the mold in two approximately equal layers with the second layer slightly overfilling the mold.
2. Consolidate each layer with the tamping rod once for every 1300 mm^2 (2 in^2) using the rounded end. Rod each layer throughout its depth taking care to not forcibly strike the bottom of the mold when compacting the first layer. Rod the second layer throughout its depth, penetrating approximately 25 mm (1") into the lower layer.
3. After rodding each layer, strike the mold 10 to 15 times with the mallet and spade along the sides and end using a trowel.
4. Strike off to a flat surface using a float or trowel and begin initial curing.

Procedure – Making Flexural Beams – Vibration

1. Fill the mold to overflowing in one layer.
2. Consolidate the concrete by inserting the vibrator vertically along the centerline at intervals not exceeding 150 mm (6 in.). Take care to not over vibrate, and withdraw the vibrator slowly to avoid large voids. Do not contact the bottom or sides of the mold with the vibrator.
3. After vibrating, strike the mold 10 to 15 times with the mallet.
4. Strike off to a flat surface using a float or trowel and begin initial curing.

Procedure – Initial Curing

- When moving cylinder specimens made with single use molds support the bottom of the mold with trowel, hand, or other device.
- For initial curing of cylinders, there are two methods, use of which depends on the agency. In both methods, the curing place must be firm, within ¼ in. of a level surface, and free from vibrations or other disturbances.
- Maintain initial curing temperature of 16 to 27° C (60 to 80°F) or 20 to 26°C (68 to 78°F) for concrete with strength of 40 Mpa (6000 psi) or more.
- Prevent loss of moisture.

Method 1 – Initial cure in a temperature controlled chest-type curing box

1. Finish the cylinder using the tamping rod, straightedge, float or trowel. The finished surface shall be flat with no projections or depressions greater than 6.3 mm (1/8 in.).
2. Place the mold in the curing box. When lifting light-gauge molds be careful to avoid distortion (support the bottom, avoid squeezing the sides).

3. Place the lid on the mold to prevent moisture loss.
4. Mark the necessary identification data on the cylinder mold and lid.

Method 2 – Initial cure by burying in earth or by using a curing box over the cylinder

Note 3: This procedure may not be the preferred method of initial curing due to problems in maintaining the required range of temperature.

1. Move the cylinder with excess concrete to the initial curing location.
2. Mark the necessary identification data on the cylinder mold and lid.
3. Place the cylinder on level sand or earth, or on a board, and pile sand or earth around the cylinder to within 50 mm (2 in.) of the top.
4. Finish the cylinder using the tamping rod, straightedge, float or trowel. Use a sawing motion across the top of the mold. The finished surface shall be flat with no projections or depressions greater than 6.3 mm (1/8 in.).
5. If required by the agency, place a cover plate on top of the cylinder and leave it in place for the duration of the curing period or place the lid on the mold to prevent moisture loss.

Procedure – Transporting Specimens

- After 24 to 48 hours of initial curing, the specimens will be transported to the laboratory for storing under standard conditions. Specimen identity will be noted along with the date / time the specimen was made and the maximum and minimum temperatures registered during the initial cure.
- While in transport, specimens shall be protected from jarring, extreme changes in temperature, freezing, or moisture loss.
- Cylinders shall be secured so that the axis is vertical.
- Transportation time shall not exceed 4 hours.

Final Curing

- For all specimens (cylinders or beams) final curing must be started within 30 minutes of mold removal. Temperature shall be maintained at 23° ±2°C (73 ±3°F). Free moisture must be present on the surfaces of the specimens during the entire curing period. Curing may be accomplished in a moist room or water tank conforming to M 201.
- For cylinders, during the final 3 hours prior to testing the temperature requirement may be waived, but free moisture must be maintained on specimen surfaces at all times until tested.
- Final curing of beams must include immersing in lime-saturated water for at least 20 hours prior to testing.

Report

- Report on standard agency forms.
- Pertinent placement information for identification of project, element(s) represented, etc.
- Date and Time molded.
- Test ages.
- Slump, Air Content, & Density
- Temperature (concrete, initial cure max. & min., and ambient).
- Method of initial curing.
- Other information as required by agency such as concrete supplier, truck number, invoice number, water added, etc.

Addendum WAQTC FOP for AASHTO T 23

Following are guidelines for the use of WAQTC FOP for AASHTO T 23 by the State of Alaska DOT&PF.

1. If the slump is 1” or less, consolidate by vibrator. If the slump is above 1” , consolidate by rodding. Concrete for curb and gutter shall be rodded regardless of slump.
2. When cylinders must be transported, transportation time shall not exceed 8 hours. If this transportation time requirement cannot be met, the transportation time must be approved by the Engineer in writing prior to transporting.
3. All acceptance testing will be performed using 150 mm by 300 mm (6 in by 12 in) cylinders.

Making and Curing Hydraulic-Cement Grout (Nonshrink) Test Specimens ATM 507

1. Scope

This procedure covers the method for sampling, making, initially curing, and transporting hydraulic-cement grout (Nonshrink) test specimens in the field based on AASHTO T 106.

2. Apparatus

- Specimen molds for the 50 mm (2″) cube specimens shall be brass. The molds shall have not more than three cube compartments and shall be separable into not more than three parts including the base. The parts of the mold when assembled shall be positively held together, tight fitting and watertight. The sides of the mold shall be sufficiently rigid to prevent spreading or warping. The interior faces of the mold shall conform to the requirements of Table 1 of AASHTO T 106.
- Metal cover plate conveniently sized to fit over top of the specimen mold with a clamping system (such as C-clamps or equivalent) to hold the plate tightly to provide confinement and to prevent moisture loss and contamination.
- Tamper for consolidating plastic mixes. The tamper shall be hard rubber with a tamping face cross-section of 13 x 25 mm (1/2″ x 1″) and a length of 120 to 150 mm (5″ to 6″). The tamping face shall be flat and at right angles to the length of the tamper.
- Rubber gloves for consolidating fluid mixes and general protection whenever handling hydraulic cement mixes.
- Trowel having a steel blade 100 to 150 mm (4″ to 6″) in length, with straight edges.
- Miscellaneous equipment such as scoops, concrete form release oil, small brush or lint-free cloth for applying and removing excess release oil, burlap or other wettable wrapping cloth, pans large enough to hold specimen molds and sand.

3. Terminology

- Plastic mix is defined as material viscous enough that an indentation will be left in the surface of the grout after tamping.
- Fluid mix is defined as material fluid enough that little or no indentation will be left in the surface of the grout after puddling.

4. Sampling

Obtain samples in accordance with WAQTC TM 2 if the batch equals or exceeds 1 m^3 (1 cy). If the batch is less than 1 m^3 (1 cy) sample directly from the mixer or from the batch after discharge and remixing. The minimum sample size is 1200 g (3 lb) for each set of three (3) cubes to be made. A minimum of three (3) cubes is required for each test age.

5. Molding Procedure

1. Place a layer of grout about 25 mm (1″) (approximately one-half of the depth of the mold) in all of the cube compartments. Consolidated according to the consistency of the mix.

   a. For plastic mixes, tamp each lift 32 times in 4 rounds. Each round to be at right angles to other and consisting of 8 adjoining strokes over the surface. See Figure 1 for the tamping sequence.

   b. For Fluid mixes: Puddle each lift 5 times with a gloved finger. See Figure 2 for the puddling sequence.

Figure 1
Tamping Sequence

First & Third Round

1	8
2	7
3	6
4	5

Second & Fourth Round

1	2	3	4
8	7	6	5

Figure 2
Puddling Sequence

1		4
	5	
3		2

3. When the tamping or puddling of the first lift in all of the compartments is completed, place the second lift in each of the compartments, slightly over-filling each compartment.

4. Consolidate the grout in each compartment as described in 2a or 2b with the additional requirement that during consolidation of the second lift any grout forced out onto the top of the mold after each round will be pushed back onto the compartment by means of the tamper and/or gloved fingers before the next consolidation round. When consolidation of the grout is completed, material should extend slightly above the top of the mold. Push any grout forced out onto the top of the mold after the last round back onto the compartment with the trowel.

5. Smooth off the cubes by a single stroke of the flat side of the trowel (with the leading edge slightly raised) across the top of each cube once at right angles to the length of the mold and once along the length of the mold.
6. Finish the grout to a plane finish by drawing the straightedge of the trowel (held nearly perpendicular to the mold) with a sawing motion over the length of the mold.

7. Immediately after finishing the tops, place and secure the cover plate over the top of the mold.

6. Curing

1. Place the covered molds in a secure location as close as possible to the structure for initial curing. These shall remain undisturbed and protected from freezing or overheating for a period of 24 ± 4 hours.

2. At the end of the initial curing period, disassemble the mold and carefully remove the cube specimens. Using a permanent marker, identify the specimens with the field number.

3. Handling the cubes very carefully, wrap them in wet burlap or towels and place them into a watertight container to prevent moisture loss.

7. Transporting and Identifying Specimens

Immediately after the initial curing period, transport the specimens to the laboratory for final curing and/or compressive strength testing under standard conditions in accordance with AASHTO T 106, Section 10.5 or 10.6.

A grout compressive strength submittal/worksheet form will be filled out with the required data and accompany the cylinders or beams to the testing laboratory.

While in transport, specimens shall be protected from jarring, freezing or moisture loss.

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Resistance of Grout to Freeze-Thaw Action ATM 520

1. Scope

This method describes the procedure for determining the resistance of the bond between a concrete surface and a grout patching material to repeated freezing and thawing.

2. Apparatus

- Mortar cubes made in accordance with ATM 507 and standard cured for a minimum of 28 days.
- Silicon carbide stone designated as C-30-Q ±VHD.
- Masking tape, 2" wide.
- General purpose balance conforming to AASHTO M 231.
- Mechanical mixer and mixing bowls meeting AASHTO T 162 requirements.
- Freezer capable of maintaining a temperature of minus 20°F.
- Watertight pan of sufficient dimensions to immerse cubes with patch.
- Moist curing room meeting the requirements of AASHTO T 106.
- Miscellaneous equipment including waterproof and cold resistant gloves, straight edge, towels, etc.

3. Specimen Preparation

1. Prepare three mortar cubes according to ATM 507. Clean any scale and loose material from one face of the cube with the carbide stone and scoring that face with two grooves (approximately 1/16") perpendicular to each other.
2. Wrap the edges of the prepared face of the cube with masking tape, creating a form approximately 1" deep.
3. To create as fluid a mix as possible, mix the patching grout with the maximum allowable water content in accordance with the manufacturer's instructions.
4. Pour the grout mixture into the form to a depth of 1/2".
5. Cure the specimens by allowing them to set in accordance with manufacturer's instructions and then placing in the moist curing room for seven days.

4. Procedure

1. Pre-cool the freezer to -29°C (-20°F).
2. Place the specimens, with the grout patch face up, into the freezer for a minimum of one hour.

   Note 1: If the specimens are to be left for extended periods (i.e. over a weekend), they should be left in the freezer.

3. Remove the specimens from the freezer and immerse the grout patch in room temperature water for a minimum of one hour. Use waterproof and cold-resistant gloves during this step.
4. Remove the specimens from the water and check the grout bond by holding the cube in one hand and twisting the grout patch with the other hand using moderate effort.
5. Repeat Steps 2-4 for 25 cycles. If any of the grout patches come loose from the cube, the sample has failed.

5. Report

Report the results of the test as either Pass or Fail.

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Terminology SP 1

1. Scope

This standard practice provides terminology as interpreted and defined by the State of Alaska. The definitions of the American Association of State Highway and Transportation Officials (AASHTO) are the ones most commonly followed by this Agency.

Absorption – The increase in the mass of aggregate due to water being absorbed into the pores of the material, but not including water adhering to the outside surface of the particles, expressed as a percentage of the dry mass.

Acceptance sampling and testing– sampling, testing, and the assessment of test results done to determine whether or not the quality of produced material or construction is acceptable in terms of the contract specifications.

Admixture – Material other than water, cement, and aggregates in portland cement concrete (PCC).

Aggregate – Hard granular material of mineral composition, including sand, gravel, slag or crushed stone, used in roadway base and in Portland Cement Concrete (PCC) and Asphalt concrete pavement.

- **Coarse aggregate** – Aggregate retained on or above the 4.75 mm (No. 4) sieve.
- **Coarse-graded aggregate** – Aggregate having a predominance of coarse sizes.
- **Dense-graded aggregate** – Aggregate having a particle size distribution such that voids occupy a relatively small percentage of the total volume.
- **Fine aggregate** – Aggregate passing the 4.75 mm (No. 4) sieve.
- **Fine-graded aggregate** – Aggregate having a predominance of fine sizes.
- **Mineral filler** – A fine mineral product at least 70 percent of which passes a 75 µm (No. 200) sieve.
- **Open-graded gap-graded aggregate** – Aggregate having a particle size distribution such that voids occupy a relatively large percentage of the total volume.
- **Well-Graded Aggregate** – Aggregate having an even distribution of particle sizes.

Aggregate storage bins – Bins that store aggregate for feeding material to the dryer in an asphalt concrete pavement plant in substantially the same proportion as required in the finished mix.

Agitation – Provision of gentle motion in Portland Cement Concrete (PCC) sufficient to prevent segregation and loss of plasticity.

Air voids – Total volume of the small air pockets between coated aggregate particles in asphalt concrete pavement; expressed as a percentage of the bulk volume of the compacted paving mixture.

Ambient temperature – Temperature of the surrounding air.

Angular aggregate – Aggregate possessing well-defined edges at the intersection of roughly planar faces.

Apparent specific gravity – The ratio of the mass, in air, of a volume of the impermeable portion of aggregate to the mass of an equal volume of water.

Asphalt – A dark brown to black cementitious material in which the predominate constituents are bitumens occurring in nature or obtained through petroleum processing. Asphalt is a constituent of most crude petroleum.

Asphalt cement – Asphalt specially prepared in quality and consistency for use in the manufacture of asphalt concrete pavement.

Asphalt concrete batch plant – A manufacturing facility for producing asphalt concrete that proportions aggregate by weight and asphalt by weight or volume.

Asphalt concrete continuous mix plant – A manufacturing facility for producing asphalt concrete that proportions aggregate and asphalt by a continuous volumetric proportioning system without specific batch intervals.

Automatic cycling control – A control system in which the opening and closing of the weigh hopper discharge gate, the bituminous discharge valve, and the pug mill discharge gate are actuated by means of automatic mechanical or electronic devices without manual control. The system includes preset timing of dry and wet mixing cycles.

Automatic dryer control – A control system that automatically maintains the temperature of aggregates discharged from the dryer.

Automatic proportioning control – A control system in which proportions of the aggregate and asphalt fractions are controlled by means of gates or valves that are opened and closed by means of automatic mechanical or electronic devices without manual control.

Bag (of cement) – 94 lb of portland cement. (Approximately 1 ft^3 of bulk cement.)

Base – A layer of selected material constructed on top of subgrade or subbase and below the paving on a roadway.

Bias – The offset or skewing of data or information away from its true or accurate position as the result of systematic error.

Binder – Asphalt cement or modified asphalt cement that binds the aggregate particles into a dense mass.

Boulders – Rock fragment, often rounded, with an average dimension larger than 300 mm (12 in.).

Bulk Density – The mass per volume of a material, including any voids that may occur within the volume.

Bulk specific gravity – The ratio of the mass, in air, of a volume of aggregate or compacted asphalt concrete mix (including the permeable and impermeable voids in the particles, but not including the voids between particles) to the mass of an equal volume of water.

Bulk specific gravity (SSD) – The ratio of the mass, in air, of a volume of aggregate or compacted asphalt concrete mix, including the mass of water within the voids (but not including the voids between particles), to the mass of an equal volume of water. (See saturated surface dry.)

Clay – Fine-grained soil that exhibits plasticity over a range of water contents, and that exhibits considerable strength when dry. Also, that portion of the soil finer than 2 μm.

Cobble – Rock fragment, often rounded, with an average dimension between 75 and 300 mm (3 and 12 in.).

Cohesionless soil – Soil with little or no strength when dry and unconfined or when submerged, such as sand.

Cohesive soil – Soil with considerable strength when dry and that has significant cohesion when unconfined or submerged.

Compaction – Densification of a soil or asphalt concrete pavement by mechanical means.

Compaction curve (Proctor curve or moisture-density curve) – The curve showing the relationship between the dry unit weight or density and the water content of a soil for a given compactive effort.

Compaction test (moisture-density test) – Laboratory compaction procedure in which a soil of known water content is placed in a specified manner into a mold of given dimensions, subjected to a compactive effort of controlled magnitude, and the resulting density determined.

Compressibility – Property of a soil or rock relating to susceptibility to decrease in volume when subject to load.

Consolidation – In the placement of portland cement concrete (PCC) it is the removal of entrapped air by either tamping or vibrating the material.

Constructor – The builder of a project. The individual or entity responsible for performing and completing the construction of a project required by the contract documents. Often called a contractor, since this individual or entity contracts with the owner.

Crusher-run – The total unscreened product of a stone crusher.

Delivery tolerances – Permissible variations from the desired proportions of aggregate and asphalt cement delivered to the pug mill.

Density – The ratio of mass to volume of a substance. Usually expressed in kg/m^3 (lb/ft^3).

Design professional – The designer of a project. This individual or entity may provide services relating to the planning, design, and construction of a project, possibly including materials testing and construction inspection. Sometimes called a “contractor”, since this individual or entity contracts with the owner.

Dryer – An apparatus that dries aggregate and heats it to specified temperatures.

Dry mix time – The time interval between introduction of aggregate into the pug mill and the addition of asphalt cement.

Durability – The property of concrete that describes its ability to resist disintegration by weathering and traffic. Included under weathering are changes in the pavement and aggregate due to the action of water, including freezing and thawing.

Effective diameter (effective size) – D_{10}, particle diameter corresponding to 10 percent finer or passing.

Embankment – Controlled, compacted material between the subgrade and subbase or base in a roadway.

Field Operating Procedure (FOP) – Procedure used in field testing on a construction site or in a field laboratory. (Based on AASHTO, ASTM or WAQTC test methods.)

Fineness modulus – A factor equal to the sum of the cumulative percentages of aggregate retained on certain sieves divided by 100; the sieves are 150 mm (6”), 75 mm (3”), 37.5 mm (1 ½”), 19.0 mm (3/4”), 9.5 mm (3/8”), 4.75 mm (No. 4), 2.36 mm (No. 8), 1.18 mm (No. 16), 0.60 mm (No. 30), 0.30 mm (No. 50), and 0.15 mm mm (No. 100). Used in the design of concrete mixes. The lower the fineness modulus, the more water/cement paste that is needed to coat the aggregate.

Fines – Portion of a soil or aggregate finer than a 75 µm (No. 200) sieve. Also silts and clays.

Free water – Water on aggregate available for reaction with hydraulic cement. Mathematically, the difference between total moisture content and absorbed moisture content.

Glacial till – Material deposited by glaciation, usually composed of a wide range of particle sizes, which has not been subjected to the sorting action of water.

Gradation (grain-size or particle-size distribution) – The proportions by mass of a soil or fragmented rock distributed by particle size.

Gradation analysis (grain size analysis, particle-size or sieve analysis) – The process of determining grain-size distribution by separation of sieves with different size openings.

Hot aggregate storage bins – Bins that store heated and separated aggregate prior to final proportioning into the mixer.

Hot mix asphalt (HMA) – High quality, thoroughly controlled hot mixture of asphalt cement and well-graded, high quality aggregate.

Hydraulic cement – Cement that sets and hardens by chemical reaction with water.

Independent assurance – A management tool not directly responsible for process control or acceptance, to provide an independent assessment of the product and/or the reliability of test results obtained from the process control and acceptance testing.

In situ – Rock or soil in its natural formation or deposit.

Liquid limit – Water content corresponding to the boundary between the liquid and plastic states.

Loam – A mixture of sand, silt and/or clay with organic matter.

Lot – A quantity of material to be controlled. It may represent a specified mass, a specified number of truckloads, a linear quantity, or a specified time period during production.

Manual proportioning control – A control system in which proportions of the aggregate and asphalt fractions are controlled by means of gates or valves that are opened and closed by manual means. The system may or may not include power assisted devices in the actuation of gate and valve opening and closing.

Materials and methods specifications – Also called prescriptive specifications. Specifications that direct the Constructor (Contractor) to use specified materials in definite proportions and specific types of equipment and methods to place the material.

Maximum size – One sieve larger than nominal maximum size.

Maximum particle size –First sieve to retain any material.

Mesh – The square opening of a sieve.

Moisture content (Soils and Aggregate)– The ratio, expressed as a percentage, of the mass of water in a material to the dry mass of the material.

Moisture content (Asphalt)– The ratio, expressed as a percentage, of the mass of water in a material to the wet mass of the material.

Nominal maximum size – One sieve larger than the first sieve to retain more than 10 percent of the material using an agency specified set of sieves based on cumulative percent retained. Where large gaps between specification sieves exist, intermediate sieve(s) may be inserted to determine nominal maximum size.

Nuclear gauge – Instruments used to measure in-place density, moisture content, or asphalt content through the measurement of nuclear emissions.

Optimum moisture content (optimum water content) – The water content at which a soil can be compacted to a maximum dry density by a given compactive effort.

Organic soil – Soil with a high organic content.

Paste – Mix of water and hydraulic cement that binds aggregate in portland cement concrete (PCC).

Penetration – The consistency of a bituminous material, expressed as the distance in tenths of a millimeter (0.1 mm) that a standard needle vertically penetrates a sample of the material under specified conditions of loading, time, and temperature.

Percent compaction – The ratio of density of a soil, aggregate, or asphalt concrete mix in the field to maximum density determined by a standard compaction test, expressed as a percentage.

Plant screens – Screens located between the dryer and hot aggregate storage bins that separate the heated aggregates by size.

Plastic limit – Water content corresponding to the boundary between the plastic and the semisolid states.

Plasticity – Property of a material to continue to deform indefinitely while sustaining a constant stress.

Plasticity index – Numerical difference between the liquid limit and the plastic limit and, thus, the range of water content over which the soil is plastic.

Portland cement – Hydraulic cement produced by pulverizing portland cement clinker.

Portland cement concrete (PCC) – A controlled mix of aggregate, portland cement, and water, and possibly other admixtures.

PCC batch plant – A manufacturing facility for producing portland cement concrete.

Proficiency samples – Homogeneous samples that are distributed and tested by two or more laboratories. The test results are compared to assure that the laboratories are obtaining the same results.

Pugmill – A shaft mixer designed to mix aggregate and cement.

Quality assurance (QA)– Planned and systematic actions necessary to provide confidence that a product or service will satisfy given requirements for quality. QA is the overall system for providing quality in a constructed project, including Quality Control (QC), Acceptance, and Independent Assurance (IA).

Quality assurance specifications – Also called QC/QA specifications. A combination of end-result (performance) specifications and materials and methods (prescriptive) specifications. The Constructor (Contractor) is responsible for quality control, and the Owner is responsible for acceptance of the product.

Quality control (QC) – Also called process control—those quality assurance actions and considerations necessary to assess production and construction processes so as to control the level of quality being produced in the end product. This concept of quality control includes sampling and testing to monitor the process but usually does not include acceptance sampling and testing.

Random sampling – Procedure for obtaining non-biased, representative samples.

Sand – Particles of rock passing the 4.75 mm (No. 4) sieve and retained on the 75 µm (No. 200) sieve.

Saturated surface dry (SSD) – Condition of an aggregate particle, asphalt concrete pavement or portland cement concrete (PCC) core, or other porous solid when the permeable voids are filled with water, but no water is present on exposed surfaces. (See bulk specific gravity.)

Segregation – The separation of aggregate by size resulting in a non-uniform material.

SHRP – The Strategic Highway Research Program (SHRP) established in 1987 as a five-year research program to improve the performance and durability of roads and to make those roads safe for both motorists and highway workers. SHRP research funds were partly used for the development of performance-based specifications to directly relate laboratory analysis with field performance.

Sieve – Laboratory apparatus consisting of wire mesh with square openings, usually in circular or rectangular frames.

Silt – Material passing the 75 µm (No. 200) sieve that is non-plastic or very slightly plastic, and that exhibits little or no strength when dry and unconfined. Also, that portion of the soil finer than 75 µm and coarser than 2 µm.

Slump – Measurement related to the workability of concrete.

Soil – Natural occurring sediments or unconsolidated accumulations of solid particles produced by the physical and chemical disintegration or rocks, and which may or may not contain organic matter.

Specific gravity – The ratio of the mass, in air, of a volume of a material to the mass of an equal volume of water.

Stability – The ability of an asphalt concrete to resist deformation from imposed loads. Stability is dependent upon internal friction, cohesion, temperature, and rate of loading.

Stratified random sampling – Procedure for obtaining non-biased, representative samples in which the established lot size is divided into equally-sized sublots.

Subbase – A layer of selected material constructed between the subgrade and the base coarse in a flexible asphalt concrete pavement roadway, or between the subgrade and Portland Cement Concrete (PCC) pavement in a rigid PCC roadway.

Subgrade – Natural soil prepared and compacted to support a structure or roadway pavement.

Sublot – A segment of a lot chosen to represent the total lot.

Superpave™ – Superpave™ (Superior Performing Asphalt Pavement) is a trademark of the Strategic Highway Research Program (SHRP). Superpave™ is a product of the SHRP asphalt research. The Superpave™ system incorporates performance-based asphalt materials characterization with design environmental conditions to improve performance by controlling rutting, low temperature cracking and fatigue cracking. The three major components of Superpave™ are the asphalt binder specification, the mix design and analysis system, and a computer software system.

Theoretical maximum specific gravity – The ratio of the mass of a given volume of asphalt concrete with no air voids to the mass of an equal volume of water, both at a stated temperature commonly referred to as the “Rice” value.

Topsoil – Surface soil, usually containing organic matter.

Uniformity coefficient – C_u, a value employed to quantify how uniform or well-graded an aggregate is: $C_u = D_{60}/D_{10}$. 60 percent of the aggregate, by mass, has a diameter smaller than D_{60} and 10 percent of the aggregate, by mass, has a diameter smaller than D_{10}.

Unit weight – The ratio of weight to volume of a substance. The term “density” is more commonly used.

µm – Micro millimeter (micron) Used as measurement for sieve size.

Viscosity – A measure of the resistance to flow; one method of measuring the consistency of asphalt.

- **Absolute viscosity** – A method of measuring viscosity using the “poise” as the basic measurement unit. This method is used at a temperature of 60°C, typical of hot pavement.
- **Kinematic viscosity** – A method of measuring viscosity using the stoke as the basic measurement unit. This method is used at a temperature of 135°C, typical of hot asphalt at a plant.

Void in the mineral aggregate (VMA) – The volume of inter-granular void space between aggregate particles of compacted asphalt concrete pavement that includes air and asphalt; expressed as a percentage of the bulk volume of the compacted paving mixture.

Voids filled with asphalt – The portion of the void in the mineral aggregate (VMA) that contains asphalt; expressed as a percentage of the bulk volume of mix or the VMA.

Wet mixing period – The time interval between the beginning of application of asphalt material and the opening of the mixer gate.

Zero air voids curve (saturation curve) – Curve showing the zero air voids density as a function of water content. Points that define the curve are calculated in accordance with the addendum of WAQTC FOP for AASHTO T 99/ T 180.

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Calibration of Mechanical Compaction Hammer/Rammer SP 2

1. Scope

This practice sets forth the apparatus, procedures, and materials necessary to calibrate a mechanical compaction hammer used in ATM 417, WAQTC FOP for AASHTO T 99/T 180, AASHTO T 245; and ASTM D 698/D 1557 in accordance with ASTM E 2168.

This test method involves potentially hazardous materials, operations and equipment. This method does not purport to address all of the safety problems associated with it use.

2. Apparatus

- Hand-operated compaction hammer and compaction pedestal conforming to the requirements of WAQTC FOP for AASHTO T 99/T 180, AASHTO T 245; and ASTM D 698/D 1557.
- Mechanical compaction hammer and pedestal conforming to the requirements of ATM 417, WAQTC FOP for AASHTO T 99/T 180, AASHTO T 245, and ASTM D 698/D 1557.
- Marshall and Proctor compaction molds, bases, collars and rubber plugs (roughly 50 mm (2") thick and cut to fit bottom of mold).
- Caliper capable of measuring 25 mm to an accuracy of 0.01 mm.
- Lead deformation apparatus, consisting of an anvil, guide collar and striking pin.
- Lead test cylinders having a maximum weight spread of 0.06 grams between the heaviest and the lightest cylinder, a length of 17.2 ± 0.1 mm and a diameter of 7.87 ± 0.05 mm. A minimum of ten test cylinders are required for the calibration of one compaction hammer (However as many as 100 test cylinders may be required.)

  Note 1: Calibration Kit CN-4242 and Lead Cylinders CN-4245 available from Soil Test have been found satisfactory.

3. Procedure--General

1. Inspect and adjust the mechanical and hand-operated compaction hammers to conform to the requirements of ATM T 17, AASHTO T 99, T 180 & T 245; and ASTM D 698 & D 1557.
2. Select a set of lead cylinders from the same lot or shipment. Remove any burrs from the ends of the cylinders using a fine grade of emery cloth.

   Note 2: Deformation of the test cylinders is affected by changes in temperature. Take precautions to maintain the temperature of the test cylinders within 3ºC of the temperature of the mechanical and hand-operated compaction hammers during the calibration procedure. All testing may be done at room temperature.

3. Measure and record, to the nearest 0.01 mm, the original length of the test cylinders.

4. Procedure—Hand Operated Manual Hammer

1. Place the compaction mold base plate on the compaction pedestal.
2. Assemble the deformation apparatus and place on the base plate.
3. Gently place a compaction mold with collar on the base plate.

4. Gently place the hand-operated hammer on top of the striking pin and, with the guide shaft held vertical; apply one drop of the hammer.

5. Measure and record, to the nearest 0.01 mm, the final length of the test cylinder.

6. Using new test cylinders each time, repeat steps 2 through 5 until five (5) deformation values are obtained that do not vary by more than ± 2.0 percent from the average value of all values within this range.

5. Procedure—Mechanically Operated Hammer

1. Assemble a compaction base, mold and collar. Place a rubber plug in the mold assembly and operate the compaction hammer for a minimum of 25 drops to allow friction in the parts to become constant. Remove the rubber plug.

2. Place the compaction mold base plate on the compaction pedestal.

3. Assemble the deformation apparatus and place on the base plate.

4. Gently place a compaction mold with collar on the base plate.

5. Gently place the mechanical hammer on top of the striking pin and, with the guide shaft held vertical; apply one drop of the hammer.

6. The mechanical compaction hammer shall operate automatically using the same technique that would be used in the actual test method. Raising and releasing the hammer manually or by any other procedure is not allowed.

7. Measure and record, to the nearest 0.01 mm, the final length of the test cylinder.

8. Using new test cylinders each time, repeat steps 3 through 7 until five (5) deformation values are obtained that do not vary by more than ± 2.0 percent from the average value of all values within this range.

6. Calibration Comparison and Adjustment

1. Calculate the percentage difference between the average deformation values of the mechanical and hand-operated compaction hammers. If the difference is less than or equal to 2.0 percent the mechanical compaction hammer is ready for use.

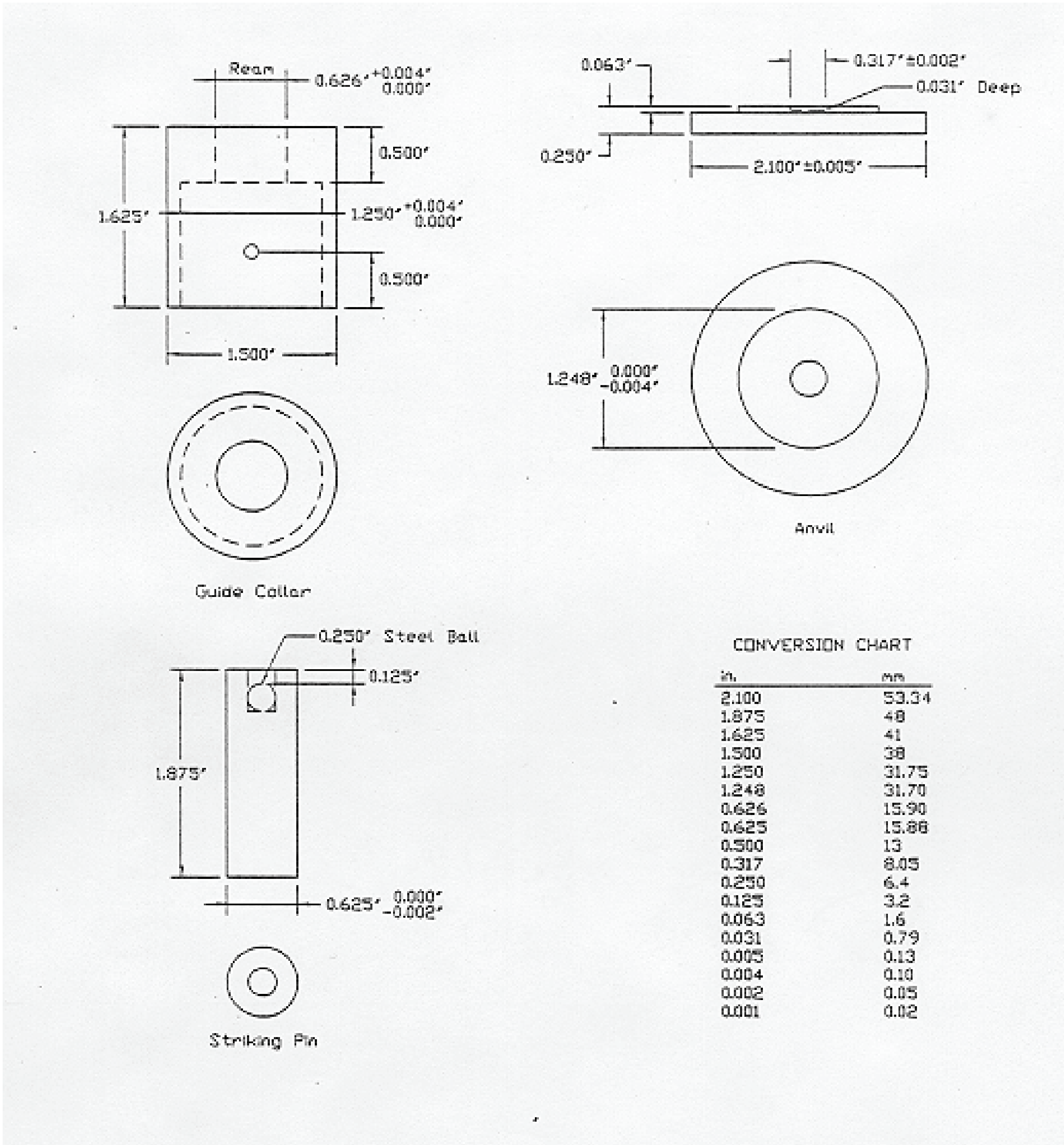
2. If the difference is greater than 2.0 percent, adjust the weight of the mechanical hammer and repeat steps 3 through 7 of the Mechanically Operated Hammer Procedure, until the mean value of 3 sets of data is equal to, or less than 2.0 percent.

7. Report

1. All compaction hammers shall be calibrated every 12 months or prior to use if the existing calibration is more than one (1) year old.

2. The original calibration certificate and test data shall be filed at the calibrating laboratory.

3. A copy of the calibration certificate shall be kept with the Compaction Hammer.



CONVERSION CHART

in.	mm
2.100	53.34
1.875	48
1.625	41
1.500	38
1.250	31.75
1.248	31.70
0.626	15.90
0.625	15.88
0.500	13
0.317	8.05
0.250	6.4
0.125	3.2
0.063	1.6
0.031	0.79
0.005	0.13
0.004	0.10
0.002	0.05
0.001	0.02

Figure 1.
LEAD DEFORMATION APPARATUS

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Hydrometer Calibration SP 3

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Rounding and Precision in Materials Test Reporting SP 6

1. Scope

This standard practice provides a procedure for rounding off numbers generated during the process of calculating materials testing results when a specific test method does not specify rounding procedures.

2. Calculation Procedures

2.1 All test results should be reported to a significant, practical, and accurate value. This can be achieved using the following procedures:

2.2 If the first digit to the right of the place to which the calculation is to be reported ends in 0, 1, 2, 3, or 4, the value of that place is not changed. If the rounded number ends in 0, the 0 should be written down. For example, if the result of a calculation is to be rounded to the tenth then 5.6489 rounds to 5.6.

2.3 If the first digit to the right of the place to which the calculation is to be reported ends in 5, 6, 7, 8, or 9, the value of that place is increased by one. For example, if the result of a calculation is to be rounded to the tenth, then 5.6543 rounds to 5.7; 7.9722 rounds to 8.0; 0.054 rounds to 0.1.

2.4 Intermediate calculations are carried out to one more decimal place than that required in the final result. For example, where the final answer is to be reported to the whole percent, intermediate calculations will be carried out to the tenth of a percent (0.1%).

2.5 Most calculators carry 8 digits internally regardless of how many digits are shown in the display. When it is directed to round to a certain level of precision, this means round that value immediately. If the calculator shows a result as 7.45, it may be carrying 7.44537901. If the directions call for this intermediate result to be given to the hundredth, the calculator must be cleared and 7.45 entered. This rounded value must be entered in the calculator in order to remove unusable figures. As another example, if the value 3.4675489 results from a calculation and the directions are to round that result to the tenth, then the calculator must be cleared and the value 3.5 entered.

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Determination of Outlier Test Results SP 7

1. Scope

This standard practice provides a mechanism for rejecting individual test values that may misrepresent the physical properties of a material lot. The method statistically identifies a non-representative "outlier" and justifies its removal from the remaining test data for the lot.

2. General

1. When a test result is clearly a result of a gross deviation from prescribed sampling or testing procedure, the test result should be discarded, without further analysis. When no direct evidence of sampling and/or testing errors exists, the lot data will be statistically evaluated for the presence of an outlier.
2. An outlying test result will be assumed to be non-characteristic of the overall quality of the material tested. Outlying test results will be excluded from the price adjustment calculation, by either documental evidence or through statistical analysis.

3. Basis of Statistical Criteria For Outliers

All test results in a lot are included in the calculation of the numerical value of a sample criterion (or statistic), which is then compared with a critical value based on the theory of random sampling from a normal distribution to determine whether the doubtful test result is to be retained or rejected. The critical value is that value of the sample criterion that would be exceeded by chance with 5% total probability. This 5% probability is the risk of erroneously rejecting a good observation and is the Department's defined outlier threshold limit.

4. Procedure

4.1 Calculate the arithmetic mean [$\bar{x}$] of all test results for the lot using the following formula:

$$\bar{x} = \frac{\sum X}{n}$$

Where:
- $\sum$ = summation of
- X = individual test value to x_n
- n = total number of test values

And where: $\bar{x}$ is rounded to the nearest 0.1 percent for density and all sieve sizes except the 0.075 mm (No. 200) sieve.

$\bar{x}$ is rounded to the nearest 0.01 percent for asphalt content and the 0.075 mm (No. 200) sieve.

4.2 Calculate sample standard deviation (s) of all test results for the lot using the following formula:

$$s = \sqrt{\frac{n\sum\left(x^2\right)-\left(\sum x\right)^2}{n(n-1)}}$$

Where:
- s = standard deviation of the lot
- $\sum(x^2)$ = summation of the squares of individual test values.

$(\sum x)^2$ = square of the summation of the individual test values.

n = total number of test values

4.3 The lot standard deviation (s) is rounded to the nearest 0.01 for density and all sieve sizes except the 0.075 mm (No. 200) sieve. The lot standard deviation(s) is rounded to the nearest 0.001 for asphalt content and the 0.075 mm (No. 200) sieve.

NOTE 1: This is the sample standard deviation and not the population (sigma) standard deviation. Many computer spreadsheet programs have formulas for population standard deviation and not sample standard deviation.

4.4 Calculate the difference between the arithmetic mean $(\bar{x})$ and the lowest test result (X_L); and between the highest test result (X_H) and the arithmetic mean $\bar{x}$

4.5 Calculate test criterion, T_L or T_H, of the test result with the greatest difference from the arithmetic mean $(\bar{x})$.

4.6 If the lowest test result (X_L) has the greatest difference from the arithmetic mean $\bar{x}$, then T_L is calculated as follows:

$$T_L = \frac{(X_L - \bar{x})}{s}$$

4.1 If the highest test result (X_H) has the greatest difference from the arithmetic mean $(\bar{x})$, then T_H is calculated as follows:

$$T_H = \frac{(X_H - \bar{x})}{s}$$

Determine critical T value from Table 1.

4.2 If T_L or T_H, whichever is larger, exceeds the critical T value from Table 1, then that test result is an outlier and will be excluded from the price adjustment calculations. If one or more additional test result(s) has the same value as the outlier, then none of the test results will be outliers and all test results will be included in the price adjustment calculations. If T_L and T_H are equal, then neither test result will be an outlier and all test results will be included in the price adjustment calculations.

NOTE 2: This test method will not be reapplied to identify additional "outliers" based on the new arithmetic mean and sample standard deviations calculated after the "outliers" have been excluded.

TABLE 1

Critical T Values for a Sample Standard Deviation

Number Of Samples, n	Critical T
3	1.155
4	1.481
5	1.715
6	1.887
7	2.020
8	2.126
9	2.215
10	2.290
11	2.355
12	2.412
13	2.462
14	2.507
15	2.549
16	2.585
17	2.620

5. Example 1

1. Consider the following test results on percent asphalt content:

   5.3, 5.6, 5.8, 5.8, 5.9, 5.9, 5.9, 6.0, 6.0 and 6.0

2. Calculate the arithmetic mean $(\bar{x})$:

   $$(\bar{x}) = \frac{5.3+5.6+5.8+5.8+5.9+5.9+5.9+6.0+6.0+6.0}{10}$$

   $(\bar{x})$ = 5.82%

3. Calculate the sample standard deviation:

   $$s = \sqrt{\frac{n\sum\left(x^2\right)-\left(\sum x\right)^2}{n(n-1)}}$$

   Where $\sum(x)^2$ = 339.16
   $(\sum x)^2$ = 3,387.24
   n = 10
   s = 0.220

4. The difference between the arithmetic mean $(\bar{x})$ and the lowest test result is:

   (5.82% - 5.3%) = 0.52%

5. The difference between the highest test result and the arithmetic mean $(\bar{x})$ is:

$(6.0\% - 5.82\%) = .18\%$

6. Calculate T_L or T_H. Since the lowest test result (5.3%) had the greatest difference from the arithmetic mean $(\bar{x})$ it is evaluated to determine if it is an outlier. T_L is calculated as follows:

$T_L = (5.82\% - 5.3\%) \div 0.220$
$T_L = 2.364$

7. Determine Critical T. From Table 1, the critical T for 10 samples is 2.290. Since $T_L = 2.364$ is greater than 2.290, the test result of 5.3% is an outlier and is excluded from the price adjustment calculations.

6. Example 2

1. Consider the following test result on percent asphalt content:

   5.3, 5.8, 5.8, 5.8, 5.9, 5.9, 6.0, 6.0, 6.0 and 6.5

2. Calculate arithmetic mean $(\bar{x})$:

$$x = \frac{5.3+5.8+5.8+5.8+5.9+5.9+6.0+6.0+6.0+6.5}{10}$$

$x = 5.90\%$

3. Calculate sample standard deviation:

$$s = \sqrt{\frac{n\sum(x^2) - (\sum x)^2}{n(n-1)}}$$

Where: $\sum(x)^2$ = 348.88
$(\sum x)^2$ = 3,481.00
n = 10
s = 0.294

4. The difference between the arithmetic mean x and the lowest test result is:

   $(5.90\% - 5.3\%) = 0.6\%$

5. The difference between the highest test result and the arithmetic mean $(\bar{x})$ is:

   $(6.5\% - 5.90\%) = 0.6\%$

6. Calculate T_L or T_H. Since the lowest test result (5.3%) and the highest test result (6.5%) have the same difference from the arithmetic mean $(\bar{x})$, both T_L and T_H are calculated.

$T_L = (5.90\% - 5.3\%) \div 0.294$
$T_H = (6.5\% - 5.90\%) \div 0.294$
$T_L = T_H = 2.041$

6.1.6 Since T_L and T_H are equal, neither test result is considered to be an outlier and all test results are included in the price adjustment calculation.

Standard Practice for Calibration of Pressure Type Air Meter SP 8

1. Scope

This practice covers the calibration of pressure type air meters used to determine the air content of freshly mixed concrete. Calibration procedures are developed to meet AASHTO T 152.

Note: This practice is equipment specific for two models of air meters currently in use by regional/field laboratories.

2. Apparatus

- Press-Ur-Meter (Charles R. Watts Company and Gilson)
- Appropriate calibration vessels for the air meters listed. Calibration vessels will have either be a vessel with an internal volume equal to 5 percent of the volume of the measuring bowl, or a vessel to place into the measuring bowl conforming to Note 1 in AASHTO T 152 and also equal to 5 percent. Regardless of type, the effective volume of the vessel should be checked.

3. Calibration Procedure for the Press-Ur-Meter:

3.1 Fill the measuring bowl with water.

3.2 Screw the straight tube into the threaded petcock hole on the underside of the cover. Clamp the cover assembly onto the measuring bowl with the tube extending down into the water.

3.3 With both petcocks open, add water through the petcock having the tubing extension, until all air is forced out the opposite petcock. Leave both petcocks open.

3.4 Pump air pressure to 0 percent or to the previous Initial Pressure line. Wait a few seconds for the compressed air to cool to ambient temperature, then stabilize the gauge needle at the assumed initial pressure by pumping up or bleeding off air, as necessary.

3.5 Close both petcocks and immediately press down on the air release lever exhausting the air into the measuring bowl. Wait a few seconds until the gauge needle is stabilized, tapping lightly on the gauge to keep gauge needle from sticking. If all the air was eliminated and the assumed Initial Pressure line was correct, the gauge should read 0 percent. If two or more tests show a consistent variation from 0 percent in the result, then change the Initial Pressure line to compensate for the variation, or remove the gauge glass and reset the gauge needle to 0 percent by turning the gauge's calibration screw. Use the newly established "Initial Pressure" line for subsequent tests.

3.6 Screw the curved tube into the outer end of the petcock with the straight tube below and, by pressing on the air release lever and controlling the flow with the petcock lever, fill the 5 percent calibrating vessel (345 ml) level full of water from the measuring bowl.

3.7 Release the air pressure at the free petcock. Open the other petcock and let the water in the curved pipe run back into the measuring bowl. There is now 5 percent air in the measuring bowl.

3.8 Pump air pressure to the Initial Pressure as determined in Step 5. Wait a few seconds for the compressed air to cool to ambient temperature and then stabilize the gauge needle at the assumed zero point by pumping up or bleeding off air, as necessary.

3.9 Close both petcocks and immediately press down on the air release lever exhausting the air into the measuring bowl. Wait a few seconds until the gauge needle is stabilized, tapping lightly on the gauge to keep gauge needle from sticking. If all the air was eliminated and the assumed Initial Pressure line was correct, the gauge should read 5 percent.

3.10 If two or more consistent tests show that the gauge at 5 percent air reads incorrectly in excess of 0.2

percent, then remove the gauge glass and reset the gauge needle to 5 percent by adjusting the gauge's calibration screw.

3.11 When the gauge reads correctly at 5 percent, additional water may be withdrawn in the same manner to check results at 10 percent.

4. Calibration Using Internal Calibration Vessel

4.1 Fill the measuring bowl with water.

4.2 Clamp the cover assembly onto the measuring bowl.

4.3 With both petcocks open, add water through one petcock, until all air is forced out the opposite petcock. Leave both petcocks open.

4.4 Pump air pressure to 0 percent or to the previous Initial Pressure Line. Wait a few seconds for the compressed air to cool to ambient temperature, then stabilize the gauge needle at the assumed zero point by pumping up or bleeding off air, as necessary.

4.5 Close both petcocks and immediately press down on the air release lever exhausting the air into the measuring bowl. Wait a few seconds until the gauge needle is stabilized, tapping lightly on the gauge to keep gauge needle from sticking. If all the air was eliminated and the assumed Initial Pressure line was correct, the gauge should read 0 percent. If two or more tests show a consistent variation from 0 percent in the result, then change the Initial Pressure line to compensate for the variation, or remove the gauge glass and reset the gauge needle to 0 percent by turning the gauge's calibration screw. Use the newly established "Initial Pressure" line for subsequent tests.

4.6 Release the pressure and remove the cover assembly.

4.7 Place the Internal Calibration Vessel into the measuring bowl, replace the cover assembly and refill as in step 3.

4.8 Pump the air pressure to the Initial Pressure Line allowing a few seconds for the gauge needle to stabilize.

4.9 Verify there is water standing in both petcocks and then close them.

4.10 Release to air into the measuring bowl by pressing down on the air release lever. Tap the gauge lightly and when stable, the meter should read 5 percent. If two or more consistent tests show that the gauge at 5 percent air reads incorrectly in excess of 0.2 percent, then remove the gauge glass and reset the gauge needle to 5 percent by adjusting the gauge's calibration screw and re-check.

5. Report

5.1 Report the results of the calibration as well as noting any adjustments or repairs made.

5.2 Label the meter with a sticker noting the month and year of the calibration.

Calibration of Unit Weight Measures SP 9

1. Scope

- This standard practice covers the calibration procedure for unit weight measures in accordance with AASHTO T 19 and ASTM C 29 to meet Department requirements.
- *This test method involves potentially hazardous materials, operations and equipment. This method does not purport to address all of the safety problems associated with it use.*

2. Apparatus

- Measure to be calibrated, meeting the requirements of the particular test method.
- Balance or scale: Accurate to 0.1 percent of the test load at any point within the range of use.
- Strike-off Plate: A glass 1/4-in. (6mm) thick and at least 2-in. (50 mm) greater than the diameter of the measure with which it is to be used. The plate shall be straight and smooth within tolerance of 0.01-in. (0.25 mm).
- Grease: Water pump, chassis, stopcock or similar grease.
- Water, at room temperature.
- Thermometer

3. Measure Identification, Calibration Frequency and Records

1. Each measure will be marked with a permanent and unique identification mark.
2. Measures shall be calibrated at least once per year or whenever there is reason to question the accuracy of the calibration.
3. Records of the calibration will be kept with the measure or by the laboratory conducting the calibration with the calibration volume being marked on the measure in a durable, removable medium.

4. Procedure

1. Grease the rim of the measure to form a seal with the strike-off plate preventing water leakage when measure is filled with water.
2. Determine and record (as M_m) the mass of the dry measure and strike-off plate.
3. Fill the measure with water at a temperature between 60°F and 85°F (16°C and 29°C) and cover with the strike-off plate in such a way as to eliminate bubbles and excess water.
4. Wipe dry the measure and cover plate, being careful not to lose any water from the measure.
5. Determine and record (as M_w) the mass of the measure, strike-off plate, and water in the measure.
6. Measure and record (as T) the temperature of the water and determine its density from Table 1 interpolating as necessary.

5. Calculation

1. Calculate the volume of the measure, V_m, by:

$$V_m = \frac{M_W - M_m}{D}$$

Where V_m = calibrated volume of measure

M_W = mass of measure, strike-off plate and water,

M_m = mass of measure and strike-off plate,

And D = density of water at temperature T from Table 1.

Note 1: From Table 1 use the units required by the particular test method and/or specification.

6. Report

Report the calibrated volume to the nearest 0.0001 cubic foot.

DENSITY of WATER

T °F	T °C	lbs/ft3	g/cm3	kg/m3	T °F	T °C	lbs/ft3	g/cm3	kg/m3	T °F	T °C	lbs/ft3	g/cm3	kg/m3	T °F	T °C	lbs/ft3	g/cm3	kg/m3
59.0	**15.0**	62.372	0.99910	999.10	**65.8**	**18.8**	62.330	0.99843	998.43	**72.7**	**22.6**	62.280	0.99762	997.62	**79.5**	**26.4**	62.220	0.99666	996.66
59.2	**15.1**	62.371	0.99908	999.08	**66.0**	**18.9**	62.329	0.99841	998.41	**72.9**	**22.7**	62.278	0.99760	997.60	**79.7**	**26.5**	62.218	0.99663	996.63
59.4	**15.2**	62.370	0.99907	999.07	**66.2**	**19.0**	62.328	0.99840	998.40	**73.0**	**22.8**	62.277	0.99757	997.57	**79.9**	**26.6**	62.216	0.99660	996.60
59.5	**15.3**	62.369	0.99905	999.05	**66.4**	**19.1**	62.327	0.99838	998.38	**73.2**	**22.9**	62.275	0.99755	997.55	**80.1**	**26.7**	62.214	0.99657	996.57
59.7	**15.4**	62.368	0.99904	999.04	**66.6**	**19.2**	62.326	0.99836	998.36	**73.4**	**23.0**	62.274	0.99753	997.53	**80.2**	**26.8**	62.213	0.99655	996.55
59.9	**15.5**	62.368	0.99903	999.03	**66.7**	**19.3**	62.325	0.99834	998.34	**73.6**	**23.1**	62.272	0.99750	997.50	**80.4**	**26.9**	62.211	0.99652	996.52
60.1	**15.6**	62.367	0.99901	999.01	**66.9**	**19.4**	62.323	0.99832	998.32	**73.8**	**23.2**	62.271	0.99748	997.48	**80.6**	**27.0**	62.209	0.99649	996.49
60.3	**15.7**	62.365	0.99899	998.99	**67.1**	**19.5**	62.322	0.99830	998.30	**73.9**	**23.3**	62.269	0.99745	997.45	**80.8**	**27.1**	62.208	0.99647	996.47
60.4	**15.8**	62.364	0.99897	998.97	**67.3**	**19.6**	62.321	0.99828	998.28	**74.1**	**23.4**	62.268	0.99743	997.43	**81.0**	**27.2**	62.206	0.99644	996.44
60.6	**15.9**	62.363	0.99896	998.96	**67.5**	**19.7**	62.320	0.99826	998.26	**74.3**	**23.5**	62.266	0.99740	997.40	**81.1**	**27.3**	62.204	0.99641	996.41
60.8	**16.0**	62.363	0.99894	998.94	**67.6**	**19.8**	62.318	0.99824	998.24	**74.5**	**23.6**	62.265	0.99738	997.38	**81.3**	**27.4**	62.203	0.99639	996.39
61.0	**16.1**	62.361	0.99891	998.91	**67.8**	**19.9**	62.317	0.99822	998.22	**74.7**	**23.7**	62.264	0.99736	997.36	**81.5**	**27.5**	62.201	0.99636	996.36
61.2	**16.2**	62.360	0.99890	998.90	**68.0**	**20.0**	62.316	0.99820	998.20	**74.8**	**23.8**	62.262	0.99733	997.33	**81.7**	**27.6**	62.199	0.99633	996.33
61.3	**16.3**	62.359	0.99888	998.88	**68.2**	**20.1**	62.314	0.99817	998.17	**75.0**	**23.9**	62.260	0.99731	997.31	**81.9**	**27.7**	62.198	0.99630	996.30
61.5	**16.4**	62.358	0.99887	998.87	**68.4**	**20.2**	62.313	0.99815	998.15	**75.2**	**24.0**	62.259	0.99728	997.28	**82.0**	**27.8**	62.196	0.99628	996.28
61.7	**16.5**	62.357	0.99885	998.85	**68.5**	**20.3**	62.311	0.99813	998.13	**75.4**	**24.1**	62.257	0.99726	997.26	**82.2**	**27.9**	62.194	0.99625	996.25
61.9	**16.6**	62.356	0.99884	998.84	**68.7**	**20.4**	62.310	0.99811	998.11	**75.6**	**24.2**	62.255	0.99723	997.23	**82.4**	**28.0**	62.193	0.99622	996.22
62.1	**16.7**	62.355	0.99882	998.82	**68.9**	**20.5**	62.309	0.99809	998.09	**75.7**	**24.3**	62.254	0.99721	997.21	**82.6**	**28.1**	62.191	0.99620	996.20
62.2	**16.8**	62.354	0.99881	998.81	**69.1**	**20.6**	62.308	0.99807	998.07	**75.9**	**24.4**	62.252	0.99718	997.18	**82.8**	**28.2**	62.189	0.99617	996.17
62.4	**16.9**	62.353	0.99879	998.79	**69.3**	**20.7**	62.306	0.99805	998.05	**76.1**	**24.5**	62.251	0.99716	997.16	**82.9**	**28.3**	62.188	0.99614	996.14
62.6	**17.0**	62.352	0.99877	998.77	**69.4**	**20.8**	62.305	0.99803	998.03	**76.3**	**24.6**	62.249	0.99713	997.13	**83.1**	**28.4**	62.186	0.99612	996.12
62.8	**17.1**	62.350	0.99874	998.74	**69.6**	**20.9**	62.303	0.99800	998.00	**76.5**	**24.7**	62.247	0.99710	997.10	**83.3**	**28.5**	62.184	0.99609	996.09
63.0	**17.2**	62.349	0.99873	998.73	**69.8**	**21.0**	62.302	0.99798	997.98	**76.6**	**24.8**	62.246	0.99708	997.08	**83.5**	**28.6**	62.183	0.99606	996.06
63.1	**17.3**	62.348	0.99871	998.71	**70.0**	**21.1**	62.301	0.99796	997.96	**76.8**	**24.9**	62.244	0.99705	997.05	**83.7**	**28.7**	62.181	0.99603	996.03
63.3	**17.4**	62.347	0.99869	998.69	**70.2**	**21.2**	62.300	0.99794	997.94	**77.0**	**25.0**	62.243	0.99703	997.03	**83.8**	**28.8**	62.180	0.99601	996.01
63.5	**17.5**	62.346	0.99868	998.68	**70.3**	**21.3**	62.298	0.99792	997.92	**77.2**	**25.1**	62.241	0.99700	997.00	**84.0**	**28.9**	62.178	0.99598	995.98
63.7	**17.6**	62.345	0.99866	998.66	**70.5**	**21.4**	62.297	0.99789	997.89	**77.4**	**25.2**	62.240	0.99698	996.98	**84.2**	**29.0**	62.176	0.99596	995.96
63.9	**17.7**	62.344	0.99864	998.64	**70.7**	**21.5**	62.295	0.99787	997.87	**77.5**	**25.3**	62.238	0.99695	996.95	**84.4**	**29.1**	62.175	0.99594	995.94
64.0	**17.8**	62.343	0.99863	998.63	**70.9**	**21.6**	62.294	0.99785	997.85	**77.7**	**25.4**	62.236	0.99692	996.92	**84.6**	**29.2**	62.174	0.99592	995.92
64.2	**17.9**	62.342	0.99861	998.61	**71.1**	**21.7**	62.293	0.99783	997.83	**77.9**	**25.5**	62.235	0.99690	996.90	**84.7**	**29.3**	62.172	0.99589	995.89
64.4	**18.0**	62.341	0.99860	998.60	**71.2**	**21.8**	62.291	0.99780	997.80	**78.1**	**25.6**	62.233	0.99687	996.87	**84.9**	**29.4**	62.171	0.99587	995.87
64.6	**18.1**	62.339	0.99857	998.57	**71.4**	**21.9**	62.290	0.99778	997.78	**78.3**	**25.7**	62.231	0.99684	996.84	**85.1**	**29.5**	62.169	0.99584	995.84
64.8	**18.2**	62.338	0.99855	998.55	**71.6**	**22.0**	62.288	0.99776	997.76	**78.4**	**25.8**	62.230	0.99682	996.82	**85.3**	**29.6**	62.167	0.99581	995.81
64.9	**18.3**	62.337	0.99854	998.54	**71.8**	**22.1**	62.262	0.99733	997.33	**78.6**	**25.9**	62.228	0.99679	996.79	**85.5**	**29.7**	62.165	0.99578	995.78
65.1	**18.4**	62.335	0.99850	998.50	**72.0**	**22.2**	62.285	0.99771	997.71	**78.8**	**26.0**	62.226	0.99676	996.76	**85.6**	**29.8**	62.164	0.99576	995.76
65.3	**18.5**	62.334	0.99848	998.48	**72.1**	**22.3**	62.284	0.99769	997.69	**79.0**	**26.1**	62.225	0.99674	996.74	**85.8**	**29.9**	62.162	0.99573	995.73
65.5	**18.6**	62.333	0.99847	998.47	**72.3**	**22.4**	62.283	0.99767	997.67	**79.2**	**26.2**	62.223	0.99671	996.71	**86.0**	**30.0**	62.160	0.99570	995.70
65.7	**18.7**	62.332	0.99845	998.45	**72.5**	**22.5**	62.281	0.99764	997.64	**79.3**	**26.3**	62.221	0.99668	996.68					

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Worksheets with Examples SP 10

1. Scope

- This standard practice includes copies of all the standard forms developed for use on DOT&PF projects. Examples have been included to help clarify their use.

STATE OF ALASKA
DOT & PF

FOP for T 180 Modified Proctor
FIELD WORKSHEET

☐ Acceptance ☐ Verification ☐ Info. ☐ IA ☐ QC

Sample No:

Project Name:

Federal No: AKSAS No:

Material: Source:

Item No: Location:

Sampled by / Qualification No: Date: Qty. Represented:

Standard Density — Modified Proctor — WAQTC FOP for T 180		METHOD:				
COMPACTION TEST	1	2	3	4	5	6
A Mass of Mold						
B Mass of Mold + Wet Soil						
M Mass of Wet Sample B - A						
MOISTURE CONTENT — WAQTC FOP for T 255 / T 265				*W = [(Mw - MD) / MD] x 100		
C Container						
D Container + Moist Sample						
Mw Moist sample D - C						
E Container + Dry Sample						
MD Dry Sample E - C						
*W Moisture Content, %						
Pw Wet Density						
Pd Dry Density						

Gradation, % Pass	
50mm / 2"	
37.5mm / 1 1/2"	
25mm / 1"	
19mm / 3/4"	
12.5mm / 1/2"	
9.5mm / 3/8"	
4.75mm / #4	
2.36mm / #8	
1.18mm / #16	
.600mm / #30	
.300mm / #50	
.150mm / #100	
.075mm / #200	

ZAV Curve Calculations: $Ws = \frac{(62.4)(Gsa) - (Yd)}{(Yd)(Gsa)} \times 100$

Dry Density (Yd) Input for ZAV Curve: 1 2

Ws % Water Content for complete saturation 1 2

F Factor:[1/(1/Mold Volume)] =
Mold Volume =

Pw Wet Density = (M x F)

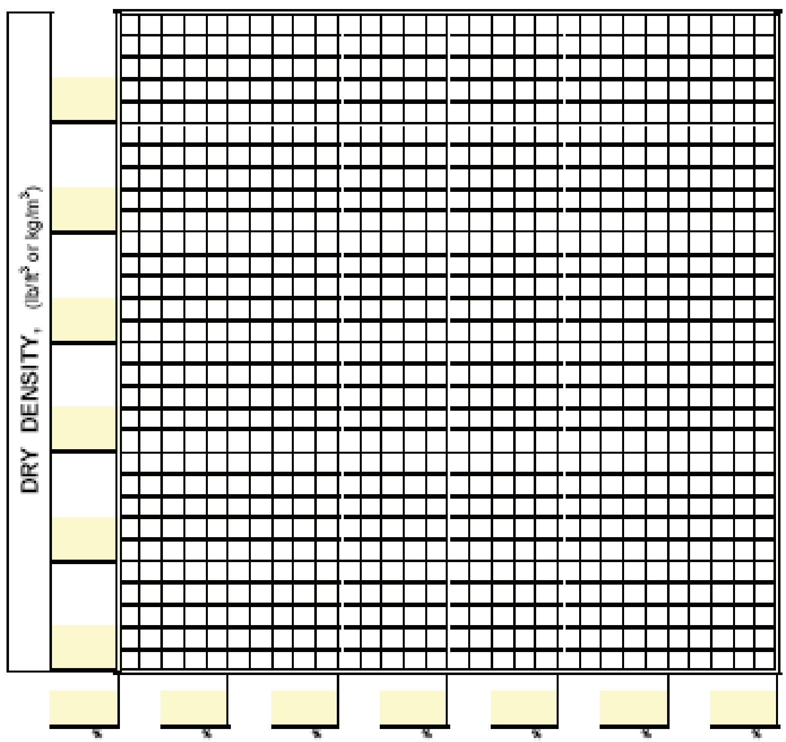
Pd Dry Density = Pw / [1 + (W / 100)]

SPECIFIC GRAVITY — WAQTC FOP for T 85	
b SSD Aggregate Mass	
c Aggregate Weight in Water	
a Dry Aggregate Mass	
Gsb BULK Specific Gravity = a / (b - c)	
SSD Specific Gravity = b / (b - c)	
Gsa Apparent Specific Gravity = a / (a - c)	
Absorption = [(b - a) / a] x 100	

MAXIMUM DENSITY (0.1 lb/ft³ or 1 kg/m³)	
OPTIMUM MOISTURE (0.1%)	

Remarks:

DRY DENSITY vs. MOISTURE CONTENT



MOISTURE CONTENT, (%)

Tested by / Date:
Checked by / Date:

Rev. 12/31/05

STATE OF ALASKA
DOT & PF

FOP for T 180 Modified Proctor
FIELD WORKSHEET

☐ Acceptance ☐ Verification ☐ Info. ☑ IA ☐ QC **Sample No:** 05C-119

Project Name: JNU EGAN DR / 10TH STREET INTERSECTION
Federal No: NH-093-2(29) AKSAS No: 70168
Material: BEDDING MATERIAL Source: MONTANA CREEK
Item No: 603 Location: JUNEAU, ALASKA
Sampled by / Qualification No: V. BEAN #079 Date: 4/5/2005 Qty. Represented: SOURCE

Standard Density — Modified Proctor — WAQTC FOP for T 180							METHOD: D
COMPACTION TEST							
A	Mass of Mold	12.61	12.61	12.61	12.61	12.61	
B	Mass of Mold + Wet Soil	23.08	23.35	23.52	23.71	23.88	
M	Mass of Wet Sample B - A	10.47	10.74	10.91	11.10	11.27	
MOISTURE CONTENT — WAQTC FOP for T 255 / T 265					*W = [(Mw - MD) / MD] x 100		
C	Container	522.1	544.6	546.1	567.8	538.8	
D	Container + Moist Sample	848.8	955.0	852.2	913.1	894.6	
Mw	Moist sample D - C	326.7	410.4	306.1	345.3	355.8	
E	Container + Dry Sample	840.0	942.0	838.5	896.9	876.5	
MD	Dry Sample E - C	317.9	397.4	292.4	329.1	337.7	
*W	Moisture Content, %	2.8	3.3	4.7	4.9	5.4	
Pw	Wet Density	139.6	143.2	145.4	148.0	150.2	
Pd	Dry Density	135.8	138.6	138.9	141.0	142.6	

Bleed

Gradation, % Pass	
50mm / 2"	
37.5mm / 1 1/2"	
25mm / 1"	100
19mm / 3/4"	99
12.5mm / 1/2"	80
9.5mm / 3/8"	69
4.75mm / #4	51
2.36mm / #8	42
1.18mm / #16	33
.600mm / #30	24
.300mm / #50	15
.150mm / #100	9
.075mm / #200	5.2

ZAV Curve Calculations:

$$Ws = \frac{(62.4)(Gsa) - (Pd)}{(Pd)(Gsa)} \times 100$$

Dry Density (Pd) Input for ZAV Curve: 7.0 | 9.0

Ws % Water Content for complete saturation

F Factor = **1 / Mold Volume** = 13.33
Mold Volume Assumed = .0750

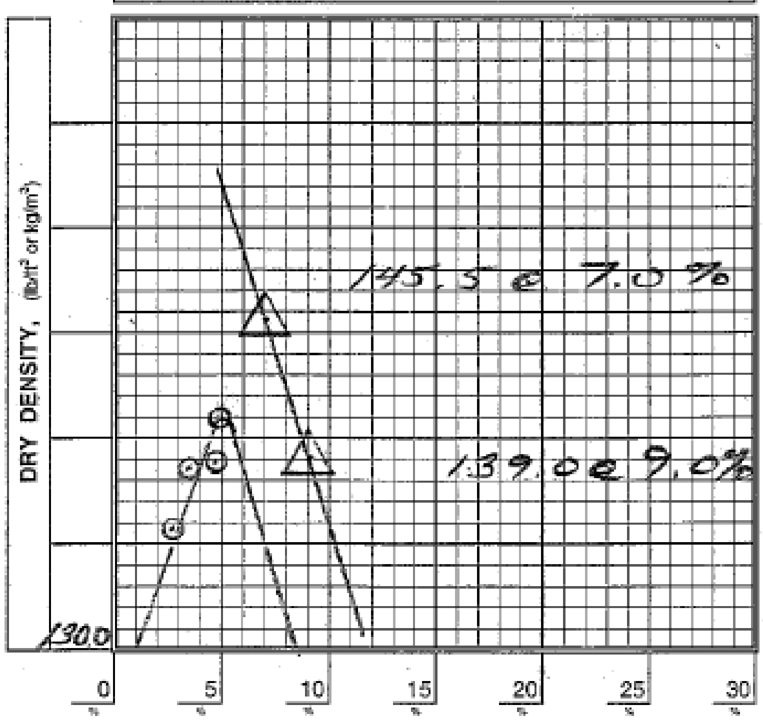
Pw Wet Density = **(M x F)**

Pd Dry Density = **Pw / [1 + (W / 100)]**

SPECIFIC GRAVITY — WAQTC FOP for T 85		
b	SSD Aggregate Mass	3052.6
c	Aggregate Weight in Water	1941.5
a	Dry Aggregate Mass	3027.7
Gsb	BULK Specific Gravity = a / (b - c)	2.725
	SSD Specific Gravity = b / (b - c)	2.747
Gsa	Apparent Specific Gravity = a / (a - c)	2.787
	Absorption = [(b - a) / a] x 100	0.8

MAXIMUM DENSITY (0.1 lb/ft³ or 1 kg/m³)	**141.0**
OPTIMUM MOISTURE (0.1%)	**5.0**

DRY DENSITY vs. MOISTURE CONTENT



Remarks: ALL IS WELL

Tested by / Date: Jeffrey A. Hart / #009
Checked by / Date: Trinie Kelley / #041

Rev. 12/31/05

STATE OF ALASKA
DOT & PF

WAQTC FOP for T 310 (METHOD A)
FIELD DENSITY WORKSHEET

☐ Acceptance ☐ Verification ☐ Info. ☐ IA ☐ QC

Project Name:
Federal No: AKSAS No:
Material: Date:
Item No: Spec. Gauge S/N:

	FIELD DENSITY TEST NUMBER				
	STATION				
	C/L REFERENCE				
	GRADE REFERENCE				
	QUANTITY REPRESENTED				
	SOURCE				
STANDARD DENSITY	WAQTC FOP for T 180:	☐ A	☐ B	☐ C ☐ D /	☐ ATM 212
	Standard Density Lab Number				
Df	Standard Density T 99/ T180 (Maximum Lab)				
	Standard Density ATM 212 (from Chart)				
	Optimum Moisture				
B	Specific Gravity ☑ Bulk ☐ Apparent				

DENSITY DETERMINATION

	Probe Depth								
		Reading #1	Reading #2	Reading #1	Reading #2	Reading #1	Reading #2	Reading #1	Reading #2
	Wet Density, (lb/ft³ or kg/m³) Gauge								
C	**Average Wet Density**								
Pd	Dry Density (gauge) C / [1 + (E / 100)]								
Pd	Dry Density (actual) C / [1 + (W / 100)]								

MOISTURE CONTENT ☐ Use WAQTC FOP for T 255/T 265 ☐ Use gauge moisture ☐ Use gauge moisture ONLY if within 1%

	% Moisture Gauge								
E	**Average % Moisture** Gauge								
F	Wet Mass + Container								
G	Dry Mass + Container								
J	Container								
W	**% Moisture** (actual) [(F - G) / (G - J)] x 100								

GRADATION / OVERSIZE CORRECTION *Note: If % Oversize (Pc) is less than or equal to 5%, no correction is required.

	ATM 212 or *WAQTC FOP for T 224	☐ 3/4" ☐ #4	☐ 3/4" ☐ #4	☐ 3/4" ☐ #4	☐ 3/4" ☐ #4
P	Wet Mass + Container				
Q	Container				
Mm	Wet Mass P - Q				
Md	Dry Mass (actual) or Mm / [1 + (E / 100)]				
T	Oversize Mass + Container				
V	Container				
M_{oc}	Oversize Mass T - V				
Pc	% Oversize (M_{DC} / Md) x 100				
Pf	% Fines 100 - Pc				
	Corrected Std. Density (Dd formual)				
% Compaction	(Pd / Corr. Std. Den.) x 100				

Dd = (100 * Df * k) / [(Df * Pc) + (k * Pf)] ⇒ k = (62.4 lb/ft³ * B) or (1000 kg/m³ * B) TCTT = Too Coarse To Test

Signature / Qualification No. / Date: Checked by / Date:

REMARKS:

Rev. 12/31/05

STATE OF ALASKA
DOT & PF

WAQTC FOP for T 310 (METHOD A)
FIELD DENSITY WORKSHEET

☑ Acceptance ☐ Verification ☐ Info. ☐ IA ☐ QC

Project Name:	Parks Hwy. Seward Meridian to Crusey		
Federal No:	NH-OA4-1(12)	AKSAS No:	52474
Material:	Unclassified	Date:	7/12/2005
Item No:		Spec.	95%
		Gauge S/N:	444888

	FIELD DENSITY TEST NUMBER	SB-D-12			
	STATION	122+00			
	C/L REFERENCE	Lt 5'			
	GRADE REFERENCE	Tob SB			
	QUANTITY REPRESENTED	1/5000 cyd			
	SOURCE	Existing			

STANDARD DENSITY WAQTC FOP for T 180: ☐ A ☐ B ☐ C ☑ D / ☐ ATM 212

	Standard Density Lab Number	SB-SC-1			
Df	Standard Density (Maximum Lab)	127.9			
	Optimum Moisture	5.8			
B	Bulk Specific Gravity	2.690			

DENSITY DETERMINATION

	Probe Depth		8"							
			Reading #1	Reading #2	Reading #1	Reading #2	Reading #1	Reading #2	Reading #1	Reading #2
	Wet Density, (lb/ft³ or kg/m³)	Gauge	137.9	139.1						
C	**Average Wet Density**		138.5							
Pd	Dry Density (gauge)	C / [1 + (E / 100)]	126.1							
Pd	Dry Density (actual)	C / [1 + (W / 100)]								

MOISTURE CONTENT WAQTC FOP for T 255/T 265 or use gauge moisture if it is within 1% of actual moisture.

	% Moisture	Gauge	9.8	9.8						
E	**Average % Moisture**	Gauge	9.8							
F	Wet Mass + Container									
G	Dry Mass + Container									
J	Container									
W	**% Moisture** (actual)	[(F - G) / (G - J)] x 100								

GRADATION / OVERSIZE CORRECTION *Note: If % Oversize (Pc) is less than or equal to 5%, no correction is required.

	ATM 212 or *WAQTC FOP for T 224		☑ 3/4" ☐ #4	☐ 3/4" ☐ #4	☐ 3/4" ☐ #4	☐ 3/4" ☐ #4
P	Wet Mass + Container		26.45			
Q	Container		1.23			
Mm	Wet Mass	P - Q	25.22			
Md	Dry Mass	(actual) or Mm / [1 + (E / 100)]	22.97			
T	Oversize Mass + Container		4.24			
V	Container					
M_{oc}	Oversize Mass	T - V	4.24			
Pc	% Oversize	(M_{oc} / Md) x 100	18			
Pf	% Fines	100 - Pc	82			
	Corrected Std. Density (Dd formual)		133.1			
	Std. Density ATM 212 (from Chart)					
	% Compaction	(Pd / Corr. Std. Den.) x 100	95			

Dd = (100 * Df* *k*) / [(Df * Pc) + (*k* * Pf)] ⇒ *k* = (62.4 lb/ft³ * B) or (1000 kg/m³ * B)

Signature / Qualification No. / Date: J Dirks / 057 / 7-12-05 Checked by / Date:

REMARKS:

Rev. 12/31/05

STATE OF ALASKA
DOT & PF

SOILS & AGGREGATE, METHOD A FIELD WORKSHEET

☐ Acceptance ☐ Verification ☐ Info. ☐ QC

Sample No:

Project Name:			
Federal No:		AKSAS No:	
Material:		Source:	
Item No:		Location:	
Sta. / Sampled from:		Sampled by / Qual. No:	
C/L & Grade Reference:		Quantity Represented:	Date:

FRACTURE — WAQTC FOP for TP 61

☑ Single Face ☐ Double Face ☐ All Face

Fractured Mass F		% Q = [Q / (F + Q + N)] x 100
Questionable Mass Q		* % Questionable ⇒
Unfractured Mass N		*Recount if > 15%
% Fracture		⇐ [(F+(Q/2)) / (F+Q+N)] x 100
Test by/date:		⇐ Spec.

MOISTURE CONTENT — WAQTC FOP for T 255 / T 265

			Constant Mass	
C	Container		Time	Gross Mass / Net Mass
A	Moist Mass + Container			
Mw	Wet Mass A - C			
B	Dry Mass + Container			
Md	Dry Mass B - C			
W	Moisture, %			
W = [(Mw - Md) / Md] x 100			% Change ⇒	

Test by/date: % Change = [(Mp - Mn) / Mp] x 100

Mp = Previous Mass Measured / Mn = New Mass Measured

LIQUID AND PLASTIC LIMIT — WAQTC FOP for T 89 and T 90

		LL	PL	
N	Number of Blows		X	
C	Container			
A	Moist Mass + Container			
Mw	Moist Mass A - C			
B	Dry Mass + Container			
Md	Dry Mass B - C			PL
W	Moisture Content, % [(Mw - Md) / Md] x 100			
LL	$W \times (N / 25)^{0.121}$			LL Spec.
Test by/date:	Plastic Index LL - PL			PI Spec.

GRADATION — WAQTC FOP for T 27 / T 11 — Method A

mm / USC	Increment 1	Increment 2	Cumulative Mass Retained C	Cumulative % Retained (C / M) x 100	% Passing = 100 − % Retained	Specs.
*75 / 3"						
50 / 2"						
*37.5 / 1½"						
25 / 1"						
*19.0 / 3/4"						
12.5 / 1/2"						
*9.5 / 3/8"						
6.3 / 1/4"						
*4.75 / #4						
*2.36 / #8						
2.00 / #10						
*1.18 / #16						
.850 / #20						
*.600 / #30						
.425 / #40						
*.300 / #50						
*.150 / #100						
.075 / #200						
Cum. Pan				⇐ G	Check Sum (≤ 0.3%) [(A - G) / A] x 100 =	
Cumulative Mass AFTER Sieving						
Dry Mass AFTER Wash BEFORE Sieving				⇐ A	Test by/date:	
Original Dry Mass				⇐ M		

FM ⇒			⇐ Fineness Modulus Target (From MD)
	to		⇐ FM Limits (± 0.2 of Mix Design FM)
(FM = Fineness Modulus = Total of % Retained of *Sieves / 100)			

Remarks:

Signature / Date:

Checked by / Date:

Rev. 3/15/06

STATE OF ALASKA
DOT & PF

SOILS & AGGREGATE, METHOD A FIELD WORKSHEET

☑ Acceptance ☐ Verification ☐ Info. ☐ QC

Sample No:	Ex-G-1		
Project Name:	Parks Hwy. Seward meridian to Crusey		
Federal No:	NH-OA4-1(12)	AKSAS No:	52474
Material:	Unclassified	Source:	Existing
Item No:	203(3)	Location:	Project Limits
Sta. / Sampled from:	304+10	Sampled by / Qual. No:	J Dirks 057
$^C/_L$ & Grade Reference:	-9	Quantity Represented:	as required
		Date:	1/1/2006

FRACTURE — WAQTC FOP for TP 61

☑ Single Face ☐ Double Face ☐ All Face

Fractured Mass F	632.6	% Q = [Q / (F + Q + N)] x 100	
Questionable Mass Q	97.6	* % Questionable ⇒	9
Unfractured Mass N	352.3	*Recount if > 15%	
% Fracture	63	⇐ [(F+(Q/2)) / (F+Q+N)] x 100	
Test by/date:	60	⇐ Spec.	

MOISTURE CONTENT — WAQTC FOP for T 255 / T 265

			Constant Mass	
C	Container	1232.1	Time	Gross Mass / Net Mass
A	Moist Mass + Container	2764.7	1:10	2637.2 / 1405.1
Mw	Wet Mass A - C	1532.6	1:45	2634.1 / 1402.0
B	Dry Mass + Container	2633.1	2:20	2633.1 / 1401.0
Md	Dry Mass B - C	1401.0		
W	Moisture, %	9		
W = [(Mw - Md) / Md] x 100 ⇑			% Change ⇒	0.07
Test by/date:			% Change = [(Mp - Mn) / Mp] x 100	

Mp = Previous Mass Measured / Mn = New Mass Measured

LIQUID AND PLASTIC LIMIT — WAQTC FOP for T 89 and T 90

		LL	PL	
N	Number of Blows	23	X	
C	Container	14.20	14.18	
A	Moist Mass + Container	24.22	23.69	
Mw	Moist Mass A - C	10.02	9.51	
B	Dry Mass + Container	22.83	22.81	
Md	Dry Mass B - C	8.63	8.63	PL
W	Moisture Content, % [(Mw - Md) / Md] x 100	16.1	10.2	10
LL	$W \times (N / 25)^{0.121}$	16	35	LL Spec.
Test by/date:	Plastic Index LL - PL	6	6	PI Spec.

GRADATION — WAQTC FOP for T 27 / T 11 — Method A

mm / USC	Increment 1	Increment 2	Cumulative Mass Retained C	Cumulative % Retained (C / M) x 100	% Passing = 100 − % Retained	Specs.
*75 / 3"						
50 / 2"						
*37.5 / 1½"						
25 / 1"						
*19.0 / 3/4"					100	
12.5 / 1/2"	724.7		724.7	14.0	86	
*9.5 / 3/8"	619.2		1343.9	26.0	74	
6.3 / 1/4"						
*4.75 / #4	1189.8		2533.7	49.0	51	
*2.36 / #8	877.6		3411.3	66.0	34	
2.00 / #10						
*1.18 / #16	574.8		3986.1	77.1	23	
.850 / #20						
*.600 / #30	329.8		4315.9	83.5	16	
.425 / #40						
*.300 / #50	228.5		4544.4	87.9	12	
*.150 / #100	205.7		4750.1	91.9	8	
.075 / #200	135.4		4885.5	94.5	5.5	
Cum. Pan	20.4					

Cumulative Mass AFTER Sieving	4905.9	⇐ G	Check Sum (≤ 0.3%) [(A - G) / A] x 100 = 0.11%
Dry Mass AFTER Wash BEFORE Sieving	4911.3	⇐ A	
Original Dry Mass	5168.7	⇐ M	Test by/date:

FM ⇒	4.81	4.70	⇐ Fineness Modulus Target (From MD)
4.5	to	4.9	⇐ FM Limits (± 0.2 of Mix Design FM)

(FM = Fineness Modulus = Total of % Retained of *Sieves / 100)

Remarks:

Signature / Date:

Checked by / Date:

Rev. 3/15/06

STATE OF ALASKA
DOT & PF

SOILS & AGGREGATE, METHOD B FIELD WORKSHEET

☐ Acceptance ☐ Verification ☐ Info. ☐ QC

Sample No:

Project Name:

Federal No: AKSAS No:

Material: Source:

Item No: Location:

Sta. / Sampled from: Sampled by / Qual. No:

C/L & Grade Reference: Quantity Represented: Date:

FRACTURE — WAQTC FOP for TP 61

☑ Single Face ☐ Double Face ☐ All Face

Fractured Mass F		% Q = [Q / (F + Q + N)] x 100
Questionable Mass Q		* % Questionable ⇒
Unfractured Mass N		*Recount if > 15%
% Fracture		⇐ [(F+(Q/2)) / (F+Q+N)] x 100
Test by/date:		⇐ Spec.

MOISTURE CONTENT — WAQTC FOP for T 255 / T 265

			Constant Mass	
C	Container		Time	Gross Mass / Net Mass
A	Moist Mass + Container			
Mw	Wet Mass A - C			
B	Dry Mass + Container			
Md	Dry Mass B - C			
W	Moisture, %			
W = [(Mw - Md) / Md] x 100			% Change ⇒	
Test by/date:		% Change = [(Mp - Mn) / Mp] x 100		

Mp = Previous Mass Measured / Mn = New Mass Measured

LIQUID AND PLASTIC LIMIT — WAQTC FOP for T 89 and T 90

		LL	PL	
N	Number of Blows		X	
C	Container			
A	Moist Mass + Container			
Mw	Moist Mass A - C			
B	Dry Mass + Container			
Md	Dry Mass B - C			PL
W	Moisture Content, % [(Mw - Md) / Md] x 100			
LL	$W \times (N / 25)^{0.121}$			LL Spec.
Test by/date:	Plastic Index LL - PL			PI Spec.

Remarks:

GRADATION — WAQTC FOP for T 27 / T 11 — Method B

mm / USC	Increment 1	Increment 2	Cumulative Mass Retained C	Cumulative % Retained (C / M) x 100	% Passing = 100 − % Retained	Specs.
*75 / 3"						
50 / 2"						
*37.5 / 1½"						
25 / 1"						
*19.0 / 3/4"						
12.5 / 1/2"						
*9.5 / 3/8"						
6.3 / 1/4"						
*4.75 / #4			D			
Pan				⇐ M1	CA Check Sum (≤ 0.3%)	
Cumulative Mass AFTER Sieving = (D + M1)				⇐ G	[(A - G) / A] x 100 =	
Dry Mass AFTER Wash BEFORE Sieving				⇐ A		
Original Dry Mass				⇐ M	Test by/date:	
			⇐ F = (M1 / M2) (0.001)			

mm / USC	Cumulative Mass B	Total Sample Cumulative Mass C = (F x B) + D	Cumulative % Retained (C / M) x 100	% Passing = 100 − % Retained	Specs.
*2.36 / #8					
2.00 / #10					
*1.18 / #16					
.850 / #20					
*.600 / #30					
.425 / #40					
*.300 / #50					
*.150 / #100					
.075 / #200					
Cum. Pan P					
M2 ⇒		⇐ − #4 Mass Actually Sieved		FA Check Sum (≤ 0.3%)	
		Test by/date:		[(M2 - P) / M2] x 100 =	

FM ⇒			⇐ Fineness Modulus Target (From MD)
	to		⇐ FM Limits (± 0.2 of Mix Design FM)

(FM = Fineness Modulus = Total of % Retained of *Sieves / 100)

Signature / Date:

Checked by / Date:

Rev. 12/31/05

STATE OF ALASKA
DOT & PF

SOILS & AGGREGATE, METHOD B FIELD WORKSHEET

☑ Acceptance ☐ Verification ☐ Info. ☐ QC

Sample No: Ex-G-1

Project Name:	Parks Hwy. Seward meridian to Crusey		
Federal No:	NH-OA4-1(12)	AKSAS No:	52474
Material:	Unclassified	Source:	Existing
Item No:	203(3)	Location:	Project Limits
Sta. / Sampled from:	304+10	Sampled by / Qual. No:	J Dirks 057
C/L & Grade Reference:	-9	Quantity Represented:	as required
		Date:	1/12/2006

FRACTURE — WAQTC FOP for TP 61

☑ Single Face ☐ Double Face ☐ All Face

Fractured Mass F	632.6	% Q = [Q / (F + Q + N)] x 100
Questionable Mass Q	97.6	* % Questionable ⇒ 9
Unfractured Mass N	352.3	*Recount if > 15%
% Fracture	63	⇐ [(F+(Q/2)) / (F+Q+N)] x 100
Test by/date	60%	⇐ Spec.

MOISTURE CONTENT — WAQTC FOP for T 255 / T 265

			Constant Mass	Gross Mass / Net Mass
C	Container	1232.1	Time	
A	Moist Mass + Container	2764.7	1:10	2637.2
Mw	Wet Mass A - C	1532.6		1405.1
B	Dry Mass + Container	2633.1	1:45	2634.1
				1402.0
Md	Dry Mass B - C	1401.0	2:20	2633.1
				1401.0
W	Moisture, %	9		
W = [(Mw - Md) / Md] x 100			% Change ⇒	0.07
Test by/date:			% Change = [(Mp - Mn) / Mp] x 100	

Mp = Previous Mass Measured / Mn = New Mass Measured

LIQUID AND PLASTIC LIMIT — WAQTC FOP for T 89 and T 90

		LL	PL	
N	Number of Blows	23		
C	Container	14.20	14.18	
A	Moist Mass + Container	24.22	23.69	
Mw	Moist Mass A - C	10.02	9.51	
B	Dry Mass + Container	22.83	22.81	
Md	Dry Mass B - C	8.63	8.63	PL
W	Moisture Content, % [(Mw - Md) / Md] x 100	16.1	10.2	10
LL	$W \times (N / 25)^{0.121}$	16	35	LL Spec.
Test by/date:	Plastic Index LL - PL	6	12	PI Spec.

Remarks:

GRADATION — WAQTC FOP for T 27 / T 11 — Method B

mm / USC	Increment 1	Increment 2	Cumulative Mass Retained C	Cumulative % Retained (C / M) x 100	% Passing = 100 − % Retained	Specs.
*75 / 3"						
50 / 2"						
*37.5 / 1½"						
25 / 1"						
*19.0 / 3/4"					100	
12.5 / 1/2"	161.1		161.1	5.0	95	
*9.5 / 3/8"	481.4		642.5	20.0	80	
6.3 / 1/4"						
*4.75 / #4	475.8		1118.3 D	34.8	65	
Pan	1966.7		1966.7	⇐ M1	CA Check Sum (≤ 0.3%)	
Cumulative Mass AFTER Sieving = (D + M1)			3085.0	⇐ G	[(A - G) / A] x 100 =	
Dry Mass AFTER Wash BEFORE Sieving			3085.1	⇐ A	0.00%	
Original Dry Mass			3214.0	⇐ M	Test by/date:	
	3.835		⇐ F = (M1 / M2) (0.001)			

mm / USC	Cumulative Mass B	Total Sample Cumulative Mass C = (F x B) + D	Cumulative % Retained (C / M) x 100	% Passing = 100 − % Retained	Specs.
*2.36 / #8					
2.00 / #10	207.1	1912.6	59.5	41	
*1.18 / #16					
.850 / #20					
*.600 / #30					
.425 / #40	395.0	2633.2	81.9	18	
*.300 / #50					
*.150 / #100	454.9	2862.9	89.1	11	
.075 / #200	504.0	3051.3	94.9	5.1	
Cum. Pan P	511.8				
M2 ⇒	512.8	⇐ − #4 Mass Actually Sieved		FA Check Sum (≤ 0.3%)	
		Test by/date:		[(M2 - P) / M2] x 100 =	
				0.20%	

FM ⇒			⇐ Fineness Modulus Target (From MD)
	to		⇐ FM Limits (± 0.2 of Mix Design FM)

(FM = Fineness Modulus = Total of % Retained of *Sieves / 100)

Signature / Date:

Checked by / Date:

Rev. 12/31/05

STATE OF ALASKA
DOT & PF

SOILS & AGGREGATE, METHOD C FIELD WORKSHEET

☐ Acceptance ☐ Verification ☐ Info. ☐ QC

Sample No:

Project Name:

Federal No: AKSAS No:

Material: Source:

Item No: Location:

Sta. / Sampled from: Sampled by / Qual. No:

C/L & Grade Reference: Quantity Represented: Date:

FRACTURE — WAQTC FOP for TP 61

☐ Single Face ☐ Double Face ☐ All Face

Fractured Mass F		% Q = [Q / (F + Q + N)] x 100
Questionable Mass Q		* % Questionable ⇒
Unfractured Mass N		*Recount if > 15%
% Fracture		⇐ [(F+(Q/2)) / (F+Q+N)] x 100
Test by/date:		⇐ Spec.

MOISTURE CONTENT — WAQTC FOP for T 255 / T 265

			Constant Mass	
C	Container		Time	Gross Mass / Net Mass
A	Moist Mass + Container			
Mw	Wet Mass A - C			
B	Dry Mass + Container			
Md	Dry Mass B - C			
W	Moisture, %			
	W = [(Mw - Md) / Md] x 100		% Change ⇒	
Test by/date:		% Change = [(Mp - Mn) / Mp] x 100		

Mp = Previous Mass Measured / Mn = New Mass Measured

LIQUID AND PLASTIC LIMIT — WAQTC FOP for T 89 and T 90

		LL	PL	
N	Number of Blows		X	
C	Container			
A	Moist Mass + Container			
Mw	Moist Mass A - C			
B	Dry Mass + Container			
Md	Dry Mass B - C			PL
W	Moisture Content, % [(Mw - Md) / Md] x 100			
LL	$W \times (N / 25)^{0.121}$			LL Spec.
Test by/date:	Plastic Index LL - PL			PI Spec.

GRADATION — WAQTC FOP for T 27 / T 11 — Method C

mm / USC	Increment 1	Increment 2	Cumulative Mass Retained C	Cumulative % Retained (C / M) x 100	% Passing = 100 − % Retained	Specs.
100 / 4"						
*75 / 3"					t	
50 / 2"						
*37.5 / 1½"						
25 / 1"						
*19.0 / 3/4"						
12.5 / 1/2"						
*9.5 / 3/8"						
6.3 / 1/4"						
*4.75 / #4			D			
Pan				⇐ M1	CA Check Sum (≤ 0.3%)	
Dry Mass AFTER Sieving = (D + M1)				⇐ G	[(M - G) / M] x 100 =	
Original Dry Mass BEFORE Sieving				⇐ M		
			⇐ F = (M1 / M3) (0.001)		Test by/date:	

mm / USC	Cumulative Mass B	Total Sample Cumulative Mass C = (F x B) + D	Cumulative % Retained (C / M) x 100	% Passing = 100 − % Retained	Specs.
*2.36 / #8					
2.00 / #10					
*1.18 / #16					
.850 / #20					
*.600 / #30					
.425 / #40					
*.300 / #50					
*.150 / #100					
.075 / #200				s	
Cum. Pan P		#200 on − 3" = [(s / t) x 100] ⇒			
H ⇒		⇐ Total Mass AFTER Wash		FA Check Sum (≤ 0.3%)	
M3 ⇒		⇐ − #4 Mass BEFORE Wash		[(H - P) / H] x 100 =	
		Test by/date:			

FM ⇒			⇐ Fineness Modulus Target (From MD)
	to		⇐ FM Limits (± 0.2 of Mix Design FM)
(FM = Fineness Modulus = Total of % Retained of *Sieves / 100)			

Remarks:

Signature / Date:

Checked by / Date:

Rev. 3/15/06

STATE OF ALASKA
DOT & PF

SOILS & AGGREGATE, METHOD C FIELD WORKSHEET

☑ Acceptance ☐ Verification ☐ Info. ☐ QC

Sample No:	Ex-G-1		
Project Name:	Parks Hwy. Seward meridian to Crusey		
Federal No:	NH-OA4-1(12)	AKSAS No:	58474
Material:	Unclassified	Source:	Existing
Item No:	203(3)	Location:	Project Limits
Sta. / Sampled from:	304+10	Sampled by / Qual. No:	J Dirks 057
C/L & Grade Reference:	-9	Quantity Represented:	as required
		Date:	1/12/2006

FRACTURE — WAQTC FOP for TP 61

☑ Single Face ☐ Double Face ☐ All Face

Fractured Mass F	632.6	% Q = [Q / (F + Q + N)] x 100
Questionable Mass Q	97.6	* % Questionable ⇒ 9
Unfractured Mass N	352.3	*Recount if > 15%
% Fracture	63	⇐ [(F+(Q/2)) / (F+Q+N)] x 100
Test by/date:	60%	⇐ Spec.

MOISTURE CONTENT — WAQTC FOP for T 255 / T 265

			Constant Mass	
C	Container	1232.1	Time	Gross Mass / Net Mass
A	Moist Mass + Container	2764.7	1:10	2637.2
Mw	Wet Mass A - C	1532.6		1405.1
			1:45	2634.1
B	Dry Mass + Container	2633.1		1402.0
			2:20	2633.1
Md	Dry Mass B - C	1401.0		1401.0
W	Moisture, %	9		
W = [(Mw - Md) / Md] x 100			% Change ⇒	0.07
Test by/date:			% Change = [(Mp - Mn) / Mp] x 100	

Mp = Previous Mass Measured / Mn = New Mass Measured

LIQUID AND PLASTIC LIMIT — WAQTC FOP for T 89 and T 90

		LL	PL	
N	Number of Blows	23	X	
C	Container	14.20	14.18	
A	Moist Mass + Container	24.22	23.69	
Mw	Moist Mass A - C	10.02	9.51	
B	Dry Mass + Container	22.83	22.81	
Md	Dry Mass B - C	8.63	8.63	PL
W	Moisture Content, % [(Mw - Md) / Md] x 100	16.1	10.2	10
LL	$W \times (N / 25)^{0.121}$	16		LL Spec.
Test by/date:	Plastic Index LL - PL	6		PI Spec.

Remarks:

GRADATION — WAQTC FOP for T 27 / T 11 — Method C

mm / USC	Increment 1	Increment 2	Cumulative Mass Retained C	Cumulative % Retained (C / M) x 100	% Passing = 100 − % Retained	Specs.
100 / 4"						
*75 / 3"					t	
50 / 2"						
*37.5 / 1½"						
25 / 1"						
*19.0 / 3/4"					100	
12.5 / 1/2"	125.9		125.9	3.8	96	
*9.5 / 3/8"	478.2		604.1	18.3	82	
6.3 / 1/4"						
*4.75 / #4	691.5		1295.6 D	39.1	61	
Pan	2008.9		2008.9	⇐ M1	CA Check Sum (≤ 0.3%)	
Dry Mass AFTER Sieving = (D + M1)			3304.5	⇐ G	[(M - G) / M] x 100 =	
Original Dry Mass BEFORE Sieving			3310.0	⇐ M	0.2%	
	3.808		⇐ F = (M1 / M3) (0.001)		Test by/date	

mm / USC	Cumulative Mass B	Total Sample Cumulative Mass C = (F x B) + D	Cumulative % Retained (C / M) x 100	% Passing = 100 − % Retained	Specs.
*2.36 / #8					
2.00 / #10	194.3	2035.4	61.5	39	
*1.18 / #16					
.850 / #20					
*.600 / #30					
.425 / #40	365.6	2687.7	81.2	19	
*.300 / #50					
*.150 / #100	430.8	2935.9	88.7	11	
.075 / #200	484.4	3140.0	94.9	s 5.0	
Cum. Pan P	495.1	#200 on − 3" = [(s / t) x 100] ⇒			
H ⇒	495.3	⇐ Total Mass AFTER Wash		FA Check Sum (≤ 0.3%)	
M3 ⇒	527.6	⇐ − #4 Mass BEFORE Wash		[(H - P) / H] x 100 =	
		Test by/date:			

FM ⇒			⇐ Fineness Modulus Target (From MD)
	to		⇐ FM Limits (± 0.2 of Mix Design FM)

(FM = Fineness Modulus = Total of % Retained of *Sieves / 100)

Signature / Date:

Checked by / Date:

Rev. 3/15/06

STATE OF ALASKA
DOT & PF

AGGREGATE, Sand Equivalent
FIELD WORKSHEET

☐ Acceptance ☐ Verification ☐ Info. ☐ IA ☐ QC

Sample No:

Project Name:

Federal No: AKSAS No:

Material: Source:

Item No: Location:

Sta. / Sampled from: Sampled by:

$^{C}/_{L}$ & Grade Reference: Qualification No: Date Sampled:

Sand Equivalent WAQTC FOP T 176

Sedimentation Time	20 min.

Trial No.	1	2	3
Sand Reading SR			
Clay Reading CR			
Sand Equivalent SE			
Sedimentation Time			

SE = (SR / CR) * 100

Test by/date:		Average	

Flat and Elongated ATM 306

Ratio: ☐ 1:5 ☐ 1:3 ☐ 1:2

Size Fraction mm	in	Group % Retained (A)	Dry Mass	F & E Mass	% F & E (B)	Weighted % F&E (C)
37.5 to 19.0	1½ to ¾					
19.0 to 9.5	¾ to ⅜					
9.5 to 4.75	⅜ to No. 4					
(A) Group Retained is based on plus No. 4 only				Total Weighted %		
(B) % F & E = [(F & E Mass) / (Dry Mass)] * 100				Test by/date:		
(C) Weighted % F & E = Group % Retained / % F & E						

Remarks:

Signature / Date:

Checked by / Date:

Rev.3/31/06

STATE OF ALASKA
DOT & PF

AGGREGATE, Sand Equivalent
FIELD WORKSHEET

☐ Acceptance ☐ Verification ☑ Info. ☐ IA ☐ QC

Sample No: SE LAB #O5C-383

Project Name:	Ketchikan Tongass Avenue Resurfacing		
Federal No:	IM-0902(28)	AKSAS No:	68140
Material:	Asphalt Conc.,SP,TypeA	Source:	Glacier Northwest
Item No:	401(1)	Location:	Dupont, WA
Sta. / Sampled from:		Sampled by:	WA
C/L & Grade Reference:		Qualification No:	1202
		Date Sampled:	6/4/2005

Sand Equivalent WAQTC FOP T 176

Sedimentation Time: 20 min.

Trial No.	1	2	3
Sand Reading **SR**	4.1	4.3	4.1
Clay Reading **CR**	6.3	6.7	6.5
Sand Equivalent **SE**	66	65	64
Sedimentation Time	20 min.	20 min	20 min

SE = (SR / CR) * 100

Test by/date: | Average: 65

Flat and Elongated ATM 306

Ratio: ☑ 1:5 ☐ 1:3 ☐ 1:2

Size Fraction mm	in	Group % Retained (A)	Dry Mass	F & E Mass	% F & E (B)	Weighted % F&E (C)
37.5 to 19.0	1½ to ¾					
19.0 to 9.5	¾ to ⅜	12.5	695.4	10.5	2	2
9.5 to 4.75	⅜ to No. 4	10.2	158.9	6.3	4	2

(A) Group Retained is based on plus No. 4 only — Total Weighted %: 4

(B) % F & E = [(F & E Mass) / (Dry Mass)] * 100 — Test by/date:

(C) Weighted % F & E = Group % Retained / % F & E

Remarks:

Signature / Date:
Checked by / Date:

Rev. 12/31/05

STATE OF ALASKA
DOT & PF

HOT MIX ASPHALT (HMA)
FIELD WORKSHEET

☐ Acceptance ☐ Verification ☐ Info. ☐ IA ☐ QC **Sample No:**

Project Name:
Federal No: AKSAS No:
Type Mix: Agg. Source:
Item No: Asph. Cement Source / Type:
Sta. / Location: Sampled by / Qualification No:
C/L Offset: Sample Method: Date / Time Sampled:
Lift: Quantity Rep'd: Lot: Sublot: Mix Design No: Date Tested:

AC Content of HMA by Nuclear Method — ATM 405

Gauge Make & Model:
Gauge Serial No:
Calib. No: Calib. Date:

*Sample Temperature		⇐	*N/A if using 3241-C
Sample Pan Mass			
Calib. / Target Mass		± 5g	
	16 Min. Count		Background Count
Gauge Count			
A Uncorrected AC		Gauge, 0.01 %	
W Moisture Content		T 329, 0.01 %	
Corrected AC A - W		0.1 %	
Test by/date:		⇐ Specs.	

AC Content of HMA by Ignition — WAQTC FOP for T 308 (External Balance)

☑ Method A	Furnace No. / ID:		
☐ Method B	Furnace Temp:		☐ °F ☐ °C
B	Basket Assembly Mass		0.1 g
C	Sample Mass + Basket Assembly		Before Ignition
Mi	Initial Sample Mass C - B		0.1 g
	Furnace Mass: Basket + Sample		± 5g of Mass C
D	Basket Assembly + Sample Mass		0.1 g, After Ignition
Mf	Final Sample Mass D - B		Aggregate Mass
BC	Loss, % [((Mi - Mf) / Mi) x 100]		Binder Content, 0.01%
Cf	AC Correction Factor		Oven Specific
A	UnCorrected AC BC - Cf		0.01 %
W	Moisture Content		T 329, 0.01 %
Pb	Corrected AC A - W		0.1 %
Test by/date:			⇐ Specs.

Moisture of HMA — WAQTC FOP for T 329

Oven, °F:	Sample, °F:	Time In:	Time Out:	Constant Mass
				% Change @ <0.05% = [(Mp - Mn) / Mp] x 100

			Gross Mass	% Change
C	Container, 0.1 g			
A	Wet + Container		90 min.	
B	Dry + Container		+30 min.	
Mi	Moist Mass A - C		+30 min.	
Mf	Dry Mass B - C		+30 min.	
W	Moisture Content, % [(Mi - Mf) / Mi] x 100		Mp = Previous Net Mass; Mn = New Net Mass	
Test by/date:		% Wet Mass 0.5% max	⇐ Specs.	

MSG of HMA Mix — WAQTC FOP for T 209 — Flask Method

D	Mass of Flask + Lid + Water @ 77°F, 0.1 g	
B	Mass of Flask + Lid, 0.1 g	
C	Mass of Flask + Lid + Sample, 0.1 g	
A	Mass of Dry Sample in Air C - B	
E	Flask + Lid + De-aired Water + Sample, 0.1 g	
R	Temperature Correction Factor * (Table 2 in FOP)	
	*Use only if a test temperature other than 77°F is used. R = 1 for water @ 77°F	
	Temp. of Water, °F = MSG = [A / (A + D - E)] x R	
Test by/date:	Mix Design MSG:	

⇓ *Remarks — Gauge / Ignition Printout* ⇓

Bulk Specific Gravity — WAQTC FOP for T 166 / T 275

Oven Temp:

	Method C / A	Panel	Joint
C	Weight in Water, 0.1 g		
B	Mass at SSD, 0.1 g		
X	Dry Mass + Pan, 0.1 g		
Y	Pan		
A	Dry Mass in Air, 0.1 g (X - Y)		
BSG	Bulk SpG, 0.001 A / (B - C)		
	Absorption, 0.1 [(B - A) / (B - C)] x 100		
	Lot MSG		
	Compaction, % (BSG / MSG) x 100		
Test by/date:	Specs. ⇒	-	-

Constant Mass

% Change @ <0.05% = [(Mp - Mn) / Mp] x 100

Mp = Previous Net Mass; Mn = New Net Mass		Pan		% Change
Initial Gross		Initial Net		
Mass @ <2 hrs.		Net		
Mass @ <2 hrs.		Net		

Core Thickness (Inches)

Panel		Joint	
		Avg.	
⇒		⇒	

Signature / Date: Checked by / Date:

Rev. 1/31/06

STATE OF ALASKA
DOT & PF

HOT MIX ASPHALT (HMA)
FIELD WORKSHEET

☑ Acceptance ☐ Verification ☐ Info. ☐ IA ☐ QC **Sample No:** HMA-OC-11

Project Name:	KTN-N.Tong.Wh.Crk.to MP 15 & S. Tong.Mt.Pt.-Herring Cove		
Federal No:	STP-OOOS(491) & IM-0902(30)	AKSAS No:	68062 & 68326
Type Mix:	Type II, Class B	Agg. Source:	CoAlaska Quarry
Item No:	401(1)	Asph. Cement Source / Type:	U.S. Oil/PG 58-22
Sta. / Location:	82 + 76	Sampled by / Qualification No:	Heidi Fredrickson No. 193
C/L Offset:	6' Lt	Sample Method:	Plate - ATM 403
Date / Time Sampled:	8/14/05, 7:30 AM		
Lift:	2" Top	Quantity Rep'd: Lot:	2
Sublot:	11	Mix Design No:	05C-285
Date Tested:	8/14/2005		

AC Content of HMA by Nuclear Method — ATM 405

Gauge Make & Model:	Troxler 3241-C		
Gauge Serial No:	2528		
Calib. No:	05C-148	Calib. Date:	5/30/2005

	*Sample Temperature		⇐	*N/A if using 3241-C
	Sample Pan Mass	562		
	Calib. / Target Mass	7900	± 5g	
		16 Min. Count		Background Count
	Gauge Count	4054		2209
A	Uncorrected AC	5.3	Gauge, 0.01 %	
W	Moisture Content	0.06	T 329, 0.01 %	
	Corrected AC A - W	5.2	0.1 %	
Test by/date:	HF 8/14/05	5.1 - 5.9	⇐ Specs.	

AC Content of HMA by Ignition — WAQTC FOP for T 308 (External Balance)

☑ Method A	Furnace No. / ID:	KTN#1-33	
☐ Method B	Furnace Temp:	538	☐ °F ☑ °C
B	Basket Assembly Mass	3002.3	0.1 g
C	Sample Mass + Basket Assembly	5064.6	Before Ignition
Mi	Initial Sample Mass C - B	2062.3	0.1 g
	Furnace Mass: Basket + Sample	5067.7	± 5g of Mass C
D	Basket Assembly + Sample Mass	4935.4	0.1 g, After Ignition
Mf	Final Sample Mass D - B	1933.1	Aggregate Mass
BC	Loss, % [((Mi - Mf) / Mi) x 100]	6.26	Binder Content, 0.01%
Cf	AC Correction Factor	0.69	Oven Specific
A	UnCorrected AC BC - Cf	5.57	0.01 %
W	Moisture Content	0.06	T 329, 0.01 %
Pb	Corrected AC A - W	5.5	0.1 %
Test by/date:	HF No. 193 8/14/05	5.1 - 5.9	⇐ Specs.

Moisture of HMA — WAQTC FOP for T 329

Oven, °F:	Sample, °F:	Time In:	Time Out:	Constant Mass		
280	200	9:30 AM	11:30 AM	% Change @ <0.05% = [(Mp - Mn) / Mp] x 100		
C	Container, 0.1 g	346.3			Gross Mass	% Change
A	Wet + Container	1741.1		90 min.	1740.50	
B	Dry + Container	1740.2		+30 min.	1740.40	0.01
Mi	Moist Mass A - C	1394.8		+30 min.		
Mf	Dry Mass B - C	1393.9		+30 min.		
W	Moisture Content, % [(Mi - Mf) / Mi] x 100	0.06		Mp = Previous Net Mass; Mn = New Net Mass		
		% Wet Mass 0.5% max				
Test by/date:	HF 8/14/05		⇐ Specs.			

MSG of HMA Mix — WAQTC FOP for T 209 — Flask Method

D	Mass of Flask + Lid + Water @ 77°F, 0.1 g	7363.8
B	Mass of Flask + Lid, 0.1 g	2984.8
C	Mass of Flask + Lid + Sample, 0.1 g	5027.5
A	Mass of Dry Sample in Air C - B	2042.7
E	Flask + Lid + De-aired Water + Sample, 0.1 g	8597.6
R	Temperature Correction Factor * (Table 2 in FOP)	0.99981
	*Use only if a test temperature other than 77°F is used. R = 1 for water @ 77°F	
Temp. of Water, °F = 77.0	MSG = [A / (A + D - E)] x R	2.525
Test by/date: HF No. 193 8/14/05	Mix Design MSG:	2.534

⇓ *Remarks — Gauge / Ignition Printout* ⇓

Bulk Specific Gravity — WAQTC FOP for T 166 / T 275 Oven Temp: 230

	Method C / A	Panel	Joint
C	Weight in Water, 0.1 g	966.5	
B	Mass at SSD, 0.1 g	1651.2	
X	Dry Mass + Pan, 0.1 g	2264.2	
Y	Pan	616.6	
A	Dry Mass in Air, 0.1 g (X - Y)	1647.6	
BSG	Bulk SpG, 0.001 A / (B - C)	2.406	
	Absorption, 0.1 [(B - A) / (B - C)] x 100	0.5	
	Lot MSG	2.525	
	Compaction, % (BSG / MSG) x 100	95	
Test by/date: HF 8/14/05	Specs. ⇒	92 - 98	91 - 98

Constant Mass

% Change @ <0.05% = [(Mp - Mn) / Mp] x 100

Mp = Previous Net Mass; Mn = New Net Mass		Tare	616.6	% Change
Initial Gross	2267.8	Initial Net	1651.2	
Mass @ +2 hrs.	2263.1	Net	1646.5	0.28
Mass @ +2 hrs.	2263.0	Net	1646.4	0.01

Core Thickness (inches)

Panel	Joint
1.90	
2.00	
2.00	
Avg. 1.97	Avg.
⇒ 2.0"	⇒

Signature / Date:	Heidi Fredrickson No. 193 8/14/05	Checked by / Date:	Amanda Smith 8/15/05

Rev.1/31/06

STATE OF ALASKA
DOT & PF

HMA Extracted Aggregate Gradation
FOP for T 30 - FIELD WORKSHEET

☐ Acceptance ☐ Verification ☐ Info. ☐ IA ☐ QC **Sample No:** ____ — ____

Project Name:
Federal No: AKSAS No:
Material: Source:
Item No: Location:
Sta. / Sampled from: Sampled by / Qual. No:
C/L & Grade Reference: Quantity Rep'd: Lot Sublot # Date/Time:

FRACTURE — WAQTC FOP for TP 61

☐ Single Face ☐ Double Face ☐ All Face

Fractured Mass F		% Q = [Q / (F + Q + N)] x 100	
Questionable Mass Q		* % Questionable ⇒	
Unfractured Mass N		*Recount if > 15%	
% Fracture		⇐ [(F+(Q/2)) / (F+Q+N) x 100	
Test by/date:			⇐ Spec.

MOISTURE CONTENT — WAQTC FOP for T 255 / T 265

			Constant Mass	
C	Container		Time	Gross Mass / Net Mass
A	Moist Mass + Container			
Mw	Wet Mass A - C			
B	Dry Mass + Container			
Md	Dry Mass B - C			
W	Moisture, %			
	W = [(Mw - Md) / Md] x 100 ⇑		% Change ⇒	
Test by/date:			% Change = [(Mp - Mn) / Mp] x 100	

Mp = Previous Mass Measured / Mn = New Mass Measured

LIQUID AND PLASTIC LIMIT — WAQTC FOP for T 89 and T 90

		LL	PL	
N	Number of Blows			
C	Container			
A	Moist Mass + Container			
Mw	Moist Mass A - C			
B	Dry Mass + Container			
Md	Dry Mass B - C			PL
W	Moisture Content, % [(Mw - Md) / Md] x 100			
LL	W x (N / 25)$^{0.121}$		35	LL Spec.
Test by/date:	Plastic Index LL - PL		6	PI Spec.

HMA AGGREGATE GRADATION — WAQTC FOP for T 30

mm / USC	Cumulative Mass Retained C	Cumulative % Retained (C / M) x 100	% Passing = 100 – % Retained	***Aggregate Correction Add	***Aggregate Correction Subtract	Reported % Passing	Specs.
50 / 2"							—
*37.5 / 1½"							—
25 / 1"							—
*19.0 / 3/4"							—
12.5 / 1/2"							—
*9.5 / 3/8"							—
6.3 / 1/4"							—
*4.75 / #4							—
*2.36 / #8							—
2.00 / #10							—
*1.18 / #16							—
.850 / #20							—
*.600 / #30							—
.425 / #40							—
*.300 / #50							—
*.150 / #100							—
.075 / #200			*				—
Pan (only)		⇐ P	* #200 = {[(M - A) + P] / M} x 100				

Cumulative Mass AFTER Sieving		⇐ G	Test by/date:	
Dry Mass AFTER Wash BEFORE Sieving		⇐ A		
Dry Sample Mass before Wash		⇐ **M** **(within 0.1% of Mf FOP for T 308)		

☐ Wetting Agent Used

Check Sum (≤ 0.2%)
[(A - G) / A] x 100 =

**(M) must be within 0.1% of (Mf)
Dry Sample Mass before Wash (M) = ____ % of
mass of aggregate remaining after ignition FOP for T 308
Mf 1933.1

****For aggregate correction to adjust sieves correctly, you must input numbers from the HMA Correction Factors Worksheet. Use minus sign in subtract column. Enter "0" in column if no adjustment.*

FM ⇒			⇐ Fineness Modulus Target (From MD)
	to		⇐ FM Limits (± 0.2 of Mix Design FM)

(FM = Fineness Modulus = Total of % Retained of *Sieves / 100)

Remarks:

Copy to Contractor/Date:
Tested By / Qual#:
Signature / Date:
Checked by / Date:

Rev.12/31/06

STATE OF ALASKA
DOT & PF

HMA Extracted Aggregate Gradation
FOP for T 30 - FIELD WORKSHEET

☐ Acceptance ☑ Verification ☐ Info. ☐ IA ☐ QC **Sample No:** —

Project Name:
Federal No: AKSAS No:
Material: Source:
Item No: Location:
Sta. / Sampled from: Sampled by / Qual. No:
C/L & Grade Reference: Quantity Rep'd: Lot Sublot # Date/Time:

FRACTURE — WAQTC FOP for TP 61

☐ Single Face ☐ Double Face ☐ All Face

Fractured Mass	F	1088.0	% Q = [Q / (F + Q + N)] x 100	
Questionable Mass	Q	67.0	* % Questionable ⇒	5
Unfractured Mass	N	277.0	*Recount if > 15%	
% Fracture		78	⇐ [(F+(Q/2)) / (F+Q+N)] x 100	
Test by/date:			⇐ Spec.	

MOISTURE CONTENT — WAQTC FOP for T 255 / T 265

			Constant Mass	
C	Container	1232.1	Time	Gross Mass / Net Mass
A	Moist Mass + Container	2764.7	1:10	2637.2 / 1405.1
Mw	Wet Mass A - C	1532.6	1:45	2634.1 / 1402.0
B	Dry Mass + Container	2633.1	2:20	2633.1 / 1401.0
Md	Dry Mass B - C	1401.0		
W	Moisture, %	9		
W = [(Mw - Md) / Md] x 100 ⇑			% Change ⇒	0.07
Test by/date:			% Change = [(Mp - Mn) / Mp] x 100	

Mp = Previous Mass Measured / Mn = New Mass Measured

LIQUID AND PLASTIC LIMIT — WAQTC FOP for T 89 and T 90

		LL	PL	
N	Number of Blows	23		
C	Container	14.20	14.18	
A	Moist Mass + Container	24.22	23.69	
Mw	Moist Mass A - C	10.02	9.51	
B	Dry Mass + Container	22.83	22.81	
Md	Dry Mass B - C	8.63	8.63	PL
W	Moisture Content, % [(Mw - Md) / Md] x 100	16.1	10.2	10
LL	$W \times (N / 25)^{0.121}$	16	35	LL Spec.
Test by/date:	Plastic Index LL - PL	6	6	PI Spec.

HMA AGGREGATE GRADATION — WAQTC FOP for T 30

mm / USC	Cumulative Mass Retained C	Cumulative % Retained (C / M) x 100	% Passing = 100 – % Retained	***Aggregate Correction Add	***Aggregate Correction Subtract	Reported % Passing	Specs.
50 / 2"							—
*37.5 / 1½"							—
25 / 1"							—
*19.0 / 3/4"			100.0			100	—
12.5 / 1/2"	172.4	8.9	91.0			91	—
*9.5 / 3/8"	421.2	21.8	78.0			78	—
6.3 / 1/4"							—
*4.75 / #4	950.8	49.3	51.0			51	—
*2.36 / #8	1290.1	66.8	33.0			33	—
2.00 / #10							—
*1.18 / #16	1495.7	77.5	23.0			23	—
.850 / #20							—
*.600 / #30	1608.3	83.3	17.0			17	—
.425 / #40							—
*.300 / #50	1679.1	87.0	13.0			13	—
*.150 / #100	1731.0	89.7	10.0			10	—
.075 / #200	1779.9	92.2	* 7.8			7.8	—
Pan (only)	19.2	⇐ P	* #200 = {[(M - A) + P] / M} x 100				

Cumulative Mass AFTER Sieving	1799.1	⇐ G	Test by/date:
Dry Mass AFTER Wash BEFORE Sieving	1799.4	⇐ A	
**Dry Sample Mass before Wash	1930.4	⇐ M **(within 0.1% of Mf FOP for T 308)	

☐ Wetting Agent Used

Check Sum (≤ 0.2%)
[(A - G) / A] x 100 = 0.0

**(M) must be within 0.1% of (Mf)
Dry Sample Mass before Wash (M) = 0.1 % of
mass of aggregate remaining after ignition FOP for T 308
Mf 1933.1

****For aggregate correction to adjust sieves correctly, you must input numbers from the HMA Correction Factors Worksheet. Use minus sign in subtract column. Enter '0' in column if no adjustment.*

FM ⇒			⇐ Fineness Modulus Target (From MD)
	to		⇐ FM Limits (± 0.2 of Mix Design FM)

(FM = Fineness Modulus = Total of % Retained of *Sieves / 100)

Remarks:

Copy to Contractor/Date:
Tested By / Qual#:
Signature / Date:
Checked by / Date:

Rev.12/31/05

STATE OF ALASKA DOT & PF	☐ Acceptance ☐ Verification ☐ Info. ☐ IA ☐ QC — **Sample No:**
HMA Correction Factors	Project Name:
FIELD WORKSHEET	Federal No: / AKSAS No:
	Material: / Agg.Source:
	Item No: / Location:

WAQTC FOP for T 308, Method: Mix Design No.: Furnace No. / ID:

ASPHALT CEMENT CORRECTION WAQTC FOP for T 308					
Mix Design %AC #1		After Burn %AC #1		%AC Diff. #1	
Mix Design %AC #2		After Burn %AC #2		%AC Diff. #2	
Cf	AC CORRECTION FACTOR (average of differences)				

CORRECTION FACTORS

	AGGREGATE CORRECTION	Sample #1	Sample #2
D	Sample & Basket Assembly		
B	Basket Assembly		
Mf	Mass after Ignition (D-B)		

HMA AGGREGATE GRADATION WAQTC FOP for T 30 — **AGGREGATE CORRECTION** WAQTC FOP for T 308

mm / USC	Correction Factor Blank Sample			Correction Factor Sample #1			Correction Factor Sample #2		
	Cumulative Mass Retained C	Cumulative % Retained (C / M) x 100	% Passing = 100 – % Retained	Cumulative Mass Retained C	Cumulative % Retained (C / M) x 100	% Passing = 100 – % Retained	Cumulative Mass Retained C	Cumulative % Retained (C / M) x 100	% Passing = 100 – % Retained
25 / 1"									
19.0 / 3/4"									
12.5 / 1/2"									
9.5 / 3/8"									
4.75 / #4									
2.36 / #8									
1.18 / #16									
.600 / #30									
.300 / #50									
.150 / #100									
.075 / #200									
Cum. Pan Mass			⇐Check Sum ≤0.2			⇐Check Sum ≤0.2			⇐Check Sum ≤0.2
Dry Mass After Wash			Dry Mass After Wash			Dry Mass After Wash			Calculate & Report % Passing to 0.1%
M Mass Before Wash			M Mass Before Wash			M Mass Before Wash			

mm / USC	Allowable Difference	Blank Sample % Passing	Sample #1 % Passing	Sample #2 % Passing	Difference from Blank Sample #1	Difference from Blank Sample #2	Average Difference	*Sieves to Adjust Add	*Sieves to Adjust Subtract
25 / 1"	± 5.0 %								
19.0 / 3/4"	± 5.0 %								
12.5 / 1/2"	± 5.0 %								
9.5 / 3/8"	± 5.0 %								
4.75 / #4	± 5.0 %								
2.36 / #8	± 5.0 %								
1.18 / #16	± 3.0 %								
.600 / #30	± 3.0 %								
.300 / #50	± 3.0 %								
.150 / #100	± 3.0 %								
.075 / #200	± 0.5 %								

Adjust Sieves for FOP for T 30 Gradation: Use "Y" if adjustment N/A; use minus sign for negative numbers in subtract column.

Remarks:

Signature / Date:

**Checked by / Date:

Rev.12/31/05

STATE OF ALASKA
DOT & PF

HMA Correction Factors
FIELD WORKSHEET

☐ Acceptance ☑ Verification ☐ Info. ☐ IA ☐ QC

Sample No: **SE LAB #O5C-383**

Project Name: Ketchikan Tongass Avenue Resurfacing
Federal No: IM-0902(28) AKSAS No: 68140
Material: Asphalt Conc.,SP,Type A Agg.Source: Glacier Northwest
Item No: 401(1) Location: Dupont WA
WAQTC FOP for T 308, Method: A Mix Design No.: O5C-383 Furnace No. / ID: JNU - SE Lab #1

ASPHALT CEMENT CORRECTION	WAQTC FOP for T 308				
Mix Design %AC #1	5.3	After Burn %AC #1	5.8	%AC Diff. #1	0.5
Mix Design %AC #2	5.3	After Burn %AC #2	5.9	%AC Diff. #2	0.6
Cf	AC CORRECTION FACTOR (average of differences)				0.5

CORRECTION FACTORS

	AGGREGATE CORRECTION	Sample #1	Sample #2
D	Sample & Basket Assembly	5389.6	5418.8
B	Basket Assembly	3315.6	3343.7
Mf	Mass after Ignition (D-B)	2074.0	2075.1

HMA AGGREGATE GRADATION WAQTC FOP for T 30 — **AGGREGATE CORRECTION** WAQTC FOP for T 308

mm / USC	Correction Factor Blank Sample: Cumulative Mass Retained C	Cumulative % Retained (C / M) x 100	% Passing = 100 – % Retained	Correction Factor Sample #1: Cumulative Mass Retained C	Cumulative % Retained (C / M) x 100	% Passing = 100 – % Retained	Correction Factor Sample #2: Cumulative Mass Retained C	Cumulative % Retained (C / M) x 100	% Passing = 100 – % Retained
25 / 1"	0.0	0.0	100.0	0.0	0.0	100.0	0.0	0.0	100.0
19.0 / 3/4"	169.9	8.1	91.9	153.3	7.4	92.6	168.1	8.1	91.9
12.5 / 1/2"	663.9	31.6	68.4	587.1	28.3	71.7	575.9	27.7	72.3
9.5 / 3/8"	1026.1	48.9	51.1	970.8	46.8	53.2	981.1	47.3	52.7
4.75 / #4	1305.2	62.2	37.8	1280.6	61.7	38.3	1279.6	61.6	38.4
2.36 / #8	1579.1	75.2	24.8	1552.5	74.8	25.2	1559.0	75.1	24.9
1.18 / #16	1740.3	82.9	17.1	1718.6	82.8	17.2	1724.0	83.0	17.0
.600 / #30	1844.3	87.8	12.2	1825.0	88.0	12.0	1831.0	88.2	11.8
.300 / #50	1908.7	90.9	9.1	1887.6	91.0	9.0	1894.7	91.3	8.7
.150 / #100	1947.7	92.7	7.3	1926.7	92.9	7.1	1933.9	93.2	6.8
.075 / #200	1988.6	94.70	5.30	1966.9	94.82	5.18	1975.5	95.16	4.84
Cum. Pan Mass	2002.5	0.0	⇐Check Sum ≤0.2	1991.0		⇐Check Sum ≤0.2	1991.8		⇐Check Sum ≤0.2
Dry Mass After Wash	2002.6			1995.0			1992.1		
M Mass Before Wash	2100.0			2074.4			2076.0		

Calculate & Report % Passing to 0.1%

mm / USC	Allowable Difference	Blank Sample % Passing	Sample #1 % Passing	Sample #2 % Passing	Difference from Blank Sample #1	Difference from Blank Sample #2	Average Difference	*Sieves to Adjust: Add	*Sieves to Adjust: Subtract
25 / 1"	± 5.0 %	100.0	100.0	100.0	0.0	0.0	0.0	0.0	0.0
19.0 / 3/4"	± 5.0 %	91.9	92.6	91.9	-0.7	0.0	-0.3	0.0	0.0
12.5 / 1/2"	± 5.0 %	68.4	71.7	72.3	-3.3	-3.9	-3.6	0.0	0.0
9.5 / 3/8"	± 5.0 %	51.1	53.2	52.7	-2.1	-1.6	-1.9	0.0	0.0
4.75 / #4	± 5.0 %	37.8	38.3	38.4	-0.5	-0.6	-0.6	0.0	0.0
2.36 / #8	± 5.0 %	24.8	25.2	24.9	-0.4	-0.1	-0.2	0.0	0.0
1.18 / #16	± 3.0 %	17.1	17.2	17.0	-0.1	0.1	0.0	0.0	0.0
.600 / #30	± 3.0 %	12.2	12.0	11.8	0.2	0.4	0.3	0.0	0.0
.300 / #50	± 3.0 %	9.1	9.0	8.7	0.1	0.4	0.3	0.0	0.0
.150 / #100	± 3.0 %	7.3	7.1	6.8	0.2	0.5	0.4	0.0	0.0
.075 / #200	± 0.5 %	5.30	5.18	4.84	0.12	0.46	0.29	0.00	0.00

Adjust Sieves for FOP for T 30 Gradation: Use "0" if adjustment N/A; use minus sign for negative numbers in subtract column.

Remarks:

Signature / Date: Jeff Hart #009 8/1/05
**Checked by / Date: TK 8/2/05

Rev.12/31/05

STATE OF ALASKA DOT & PF	☐ Acceptance ☐ Verification ☐ Info. ☐ IA ☐ QC	Sample No:
STANDARD DENSITY by CONTROL STRIP	Project Name:	
ATM 412 - FIELD WORKSHEET	Federal No:	AKSAS No:
	Material:	Source:
	Item No: Gauge Model:	Gauge S/N:
Standard Count:	Station to Station: Lane:	Width:
		Date:

*All initial readings are to be **Wet Density** 15 Second readings and taken in **backscatter** position.

Equipment	Pass #:	*Site 1	*Site 2	*Site 3	Average	Change	Remarks / Temp.
Drum Roller	1					X	
Roller Brand:	2						
Model No:	3						
Frequency (VPM):	4						
Amplitude:	5						
Pneumatic Roller	1					X	
	2						
	3						
	4						
	5						

Locations ⇒	1	2	3	4	5	6	7	8	9	10	
Reading 1 (1 minute)											Standard Density
Reading 2 (1 minute)											
Average Wet Density											

Moisture control is not required for HMA or ATB

Reading 1 % Moisture											Average Moisture
Reading 2 % Moisture											
Average % Moisture											

Remarks:

Tested By / Qualification No:

Signature / Date:

Checked by / Date:

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STATE OF ALASKA
DOT & PF

STANDARD DENSITY by CONTROL STRIP

ATM 412 - FIELD WORKSHEET

☑ Acceptance ☐ Verification ☐ Info. ☐ IA ☐ QC **Sample No:**

Project Name:

Federal No: AKSAS No:

Material: Source:

Item No: Gauge Model: Gauge S/N:

Standard Count: Station to Station: Lane: Width:

Date:

All initial readings are to be **Wet Density 15 Second readings and taken in **backscatter** position.*

Equipment	Pass #:	*Site 1	*Site 2	*Site 3	Average	Change	Remarks / Temp.
Drum Roller	1	127.3	130.3	126.2	127.9	X	
Roller Brand:	2	131.2	134.1	132.7	132.7	4.8	
Model No:	3	133.3	133.2	135.1	133.9	1.2	
Frequency (VPM):	4	132.7	132.4	135.6	133.6	-0.3	
Amplitude:	5						
Pneumatic Roller	1	135.5	137.1	131.1	134.6	X	
	2	138.9	136.4	134.8	136.7	2.1	
	3						
	4						
	5						

Locations ⇒	1	2	3	4	5	6	7	8	9	10	
Reading 1 (1 minute)	135.1	133.4	134.1	137.2	130.1	135.3	137.5	134.9	133.6	139.7	Standard Density
Reading 2 (1 minute)	137.2	134.3	133.8	138.9	129.2	136.5	139.8	132.1	131.7	141.3	
Average Wet Density	136.2	133.9	134.0	138.1	129.7	135.9	138.7	133.5	132.7	140.5	135.3

Moisture control is not required for HMA or ATB

Reading 1 % Moisture											Average Moisture
Reading 2 % Moisture											
Average % Moisture											

Remarks:

Tested By / Qualification No:

Signature / Date:

Checked by / Date:

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STATE OF ALASKA
DOT & PF
Density and Depth
FIELD WORKSHEET - WAQTC TM 8

☐ Info. ☐ QC

Sample No: ______

Federal No: ______ AKSAS No: ______ Gauge & Model No: ______

Material: ______ Source: ______ Serial No: ______

Item No: ______ Density Standard: 154 *Correlation Factor: ______ Spec: ______

LOCATION and Area Represented: ______ Qty Represented: ______ Core Set No: ______ Date: ______

FIELD DENSITY TEST NUMBER	1	2	3	4	5	6	7	8	9	10
STATION										
C/L REFERENCE (offset)										
GRADE REFERENCE										
QUANTITY REPRESENTED										
DENSITY DETERMINATION ☐ Backscatter Mode										
(Reading #2 is rotated 90° from reading #1)	Reading #1 / Reading#2	Reading #1 / Reading#2	Reading #1 / Reading#2	Reading #1 / Reading#2	Reading #1 / Reading#2	Reading #1 / Reading#2	Reading #1 / Reading#2	Reading #1 / Reading#2	Reading #1 / Reading#2	Reading #1 / Reading#2
D Wet Density, lb/ft^3 (Difference <=2.5 lb/ft3)										
E Average Wet Density										
F Adj Density (use *Correlation Factor)										
G % Compaction (F / Density Std) x 100										
CORRELATION with CORES										
WAQTC FOP for AASHTO T 166	Core 1	Core 2	Core 3	Core 4	Core 5	Core 6	Core 7	Core 8	Core 9	Core 10
H Core Thickness (inches)										
A Mass of Dry Specimen in Air										
B Mass of SSD Specimen in Air										
C Weight of Specimen in Water										
J Bulk Specific Gravity (.001) A / (B - C)										
K Unit Wt = Bulk SpG x 62.4 (pcf)										
E Avg Wet Density (from E above)										
L Difference = Unit Wt - Avg Wet Density K - E										

☐ Filler Material (Native Fines) Used

Tested by / Qual#: ______ Avg Difference: ______

REMARKS : ______ Signature / Date: ______ Standard Deviation (<= 2.5): ______

Checked by / Date: ______

Rev.12/31/05

STATE OF ALASKA
DOT & PF
Density and Depth
FIELD WORKSHEET - WAQTC TM 8

☐ Acceptance ☐ Verification ☑ Info. ☐ IA ☐ QC

Sample No: XX-XX-352

Federal No: STPOL9-998 AKSAS No: 92541 Gauge & Model No: XXXXX/3430

Material: Asphalt Conc., SP,Type A Source: Glacier Northwest Serial No: XXXXXXXX

Item No: 401(1) Density Standard: 157.3 *Correlation Factor: Spec: 92-98%

LOCATION and Area Represented: Test Strip Qty Represented: Core Set No: Date: 7/4/2005

FIELD DENSITY TEST NUMBER	1	2	3	4	5	6	7	8	9	10
STATION	12+60	16+44	18+12	20+95	22+45	24+20	26+86	28+38	30+99	32+48
C/L REFERENCE (offset)	6' Lt	7' Rt	4' Rt	12' Lt	5' Lt	2' Lt	8' Rt	11' Rt	7' Rt	3' Lt
GRADE REFERENCE										
QUANTITY REPRESENTED										
DENSITY DETERMINATION ☑ Backscatter Mode										
(Reading #2 is rotated 90° from reading #1)	Reading #1 / Reading#2	Reading #1 / Reading#2	Reading #1 / Reading#2	Reading #1 / Reading#2	Reading #1 / Reading#2	Reading #1 / Reading#2	Reading #1 / Reading#2	Reading #1 / Reading#2	Reading #1 / Reading#2	Reading #1 / Reading#2
D Wet Density, lb/ft³ (Difference <=2.5 lb/ft3)	151.2	152.0	150.3	150.6	151	153	151.6	152.9	152.6	151.6
	150.9	151.3	151	150.1	150.9	152.4	152	152.6	152.3	151.1
E Average Wet Density	151.1	151.7	150.7	150.4	151	152.7	151.8	152.8	152.5	151.4
F Adj Density (use *Correlation Factor)										
G % Compaction (F / Density Std) x 100	96.1	96.4	95.8	95.6	96	97.1	96.5	97.1	96.9	96.2
CORRELATION with CORES										
WAQTC FOP for AASHTO T 166	Core 1	Core 2	Core 3	Core 4	Core 5	Core 6	Core 7	Core 8	Core 9	Core 10
H Core Thickness (inches)	2	2	2	2	2	2	2	2	2	2
A Mass of Dry Specimen in Air	1647.6	1795.4	1695.4	1659.2	1644.3	1649.7	1651.9	1655.8	1659.7	1670.1
B Mass of SSD Specimen in Air	1651.2	1799.4	1698.1	1663.8	1646.6	1652.7	1655.3	1658.3	1664.4	1672.9
C Weight of Specimen in Water	966.5	1064.9	990.6	977.6	964.1	978.2	974.3	978.6	980.5	983
J Bulk Specific Gravity (.001) A / (B - C)	2.406	2.444	2.396	2.418	2.409	2.446	2.426	2.436	2.427	2.421
K Unit Wt = Bulk SpG x 62.4 (pcf)	150.1	152.5	149.5	150.9	150.3	152.6	151.4	152.0	151.4	151.1
E Avg Wet Density (from E above)	151.1	151.7	150.7	150.4	151	152.7	151.8	152.8	152.5	151.4
L Difference = Unit Wt - Avg Wet Density K - E	-1.0	0.8	-1.2	0.5	-0.7	-0.1	-0.4	-0.8	-1.1	-0.3

☐ Filler Material (Native Fines) Used

Tested by / Qual#: xyz No. 00022221 Avg Difference: -0.4

REMARKS : Signature / Date: Standard Deviation (<= 2.5): 0.67

Checked by / Date:

Rev.12/31/05

STATE OF ALASKA
DOT & PF

CONCRETE PLACEMENT REPORT

FIELD WORKSHEET

☐ Acceptance ☐ Verification ☐ Info. ☐ IA ☐ QC

Pour No:

Project Name:

Federal No: AKSAS No: Date:

Structure / Bridge: Item No:

Stations / Area Rep'd: Truck No:

Supplier: Class: Ticket No:

Aggregate Source: Cement/Type: Mix Design No:

BATCH MASS (from Scale)

			Lbs.
Nt	Cementitious Material (Nc + Nf + Nm)		
	Port. Cem. (Nc) ___ Fly Ash (Nf) ___ M-silica (Nm) ___		
A	Fine Aggregate or Sand (FA)		
B	Intermediate Aggregate (IA)		
C	Coarse Aggregate (CA)		
D	Water Added at Plant	gal. x 8.34 lbs. ⇨	
D1	Water Added on Site	gal. x 8.34 lbs. ⇨	
W1	Total Mass of Batch (Nt + A + B + C + D + D1)		

AGGREGATE SSD WEIGHTS

				-		
FA	a	Free Moisture, %		-		%
	b	SSD Weight [A / (1 + (a / 100))]	(% Moisture)*		(absorption)**	
IA	c	Free Moisture, %		-		%
	d	SSD Weight [B / (1 + (c / 100))]	(% Moisture)*		(absorption)**	
CA	e	Free Moisture, %		-		%
	f	SSD Weight [C / (1 + (e / 100))]	(% Moisture)*		(absorption)**	

* Moisture From Batch Ticket

** Absorption From Mix Design, use 0.0% if Batch Ticket reports free moisture

MASS OF WATER IN BATCH

		Lbs.
E	Free Water in FA (A - b)	
F	Free Water in IA (B - d)	
G	Free Water in CA (C - f)	
H	Total Water Mass (D + D1 + E + F + G)	

Pour Time: Start		Finish	
Mix Time:	Mix Revs:	Time of Discharge:	

Spec.= 1½ hrs. with +1 minute per degree < 70°F, not to exceed 2 hrs.

Time Between Batches: ___ < 30 Minutes

TEMPERATURE — WAQTC FOP for T 309

		Weather Conditions
Concrete Temperature		
Air Temperature		
Water Temperature		

WAQTC FOP for:			Specs:	
	T 119	Slump, in.		
	T 152	Air, %		
a	Mass of Bucket + Conc.			lb.
b	Mass of Bucket			lb.
Mm	Mass of Conc. (a - b)			lb.
Vm	Bucket Volume			ft³
W	T 121	Density (Mm/Vm)		lb / ft³
Test by/date:				

CYLINDER DATA — WAQTC FOP for T 23

Time Made	Cylinder ID	
Spec:		
Test by/date:		

Yd³ Batch Design		BATCH DATA		Actual yd³ Batch Data	Specifications		Allowable Range*	
	VB	Design Batch Volume, nearest 0.01yd³						
		Actual yd³ / Batch = *W1 / (27 x W)*, nearest 0.01 yd³	YB		* excludes 606, 609, 615, & Aviation items			
		Yield per yd³ Batch = *YB / VB*, nearest 0.01 yd³	Y					
	W / C	Water Cement Ratio (lb / lb) = *H / Nt*, nearest 0.01	W / C					
	Mix Design Proportions	Cementitious Content (lb / yd³) = *Nt / YB*, nearest lb.	N		± 1%	Batch Design		–
		Sacks / yd³ = *N / 94*, nearest 0.1 sack						
		Portland Cement Content (lb / yd³) = *Nc / YB*, nearest lb.			± 1%	Batch Design		–
		Fly Ash Content (lb / yd³) = *Nf / YB*, nearest lb.			± 5%	Batch Design		–
		Microsilica Content (lb / yd³) = *Nm / YB*, nearest lb.			± 10%	Batch Design		–
		Fine Aggregate = *b / YB*, nearest lb.			± 2%*	Batch Design		–
		Intermediate Aggregate = *d / YB*, nearest lb.			± 2%*	Batch Design		–
		Coarse Aggregate = *f / YB*, nearest lb.			± 2%*	Batch Design		–

Remarks:

Signature / Date:

Checked by / Date:

Rev.1/31/06

STATE OF ALASKA
DOT & PF

CONCRETE PLACEMENT REPORT
FIELD WORKSHEET

☑ Acceptance ☐ Verification ☐ Info. ☐ IA ☐ QC

Pour No: A 1 - Load #1

Project Name:	Egan Drive/10th St. Intersection Improvements, Phase 1				
Federal No:	NH-F-093-2(29)	AKSAS No:	70168	Date:	6/8/2005
Structure / Bridge:	Curb and Gutter Standard			Item No:	609(2a)
Stations / Area Rep'd:	"G" 2+00, Lt. To "D" 7+00, Lt.			Truck No:	9
Supplier:	AggPro	Class:	A	Ticket No:	4576
Aggregate Source: Glacier Northwest	Cement/Type:	Ash Grove Type I-II		Mix Design No:	05C-130

BATCH MASS (from Scale)

				Lbs.
Nt	Cementitious Material (Nc + Nf + Nm)			2491
Port. Cem. (Nc) 2094	Fly Ash (Nf) 397	M-silica (Nm)		
A	Fine Aggregate or Sand (FA)			5489
B	Intermediate Aggregate (IA)			
C	Coarse Aggregate (CA)			7804
D	Water Added at Plant	79	gal. x 8.34 lbs. ⇨	659
D1	Water Added on Site	11	gal. x 8.34 lbs. ⇨	92
W1	Total Mass of Batch (Nt + A + B + C + D + D1)			16535

Pour Time: Start	10:54 AM	Finish	12:05 PM
Mix Time:	Mix Revs:	Time of Discharge:	
10 Min	70	11:45 AM	

Spec.= 1½ hrs. with +1 minute per degree < 70°F, not to exceed 2 hrs.

Time Between Batches: 1st load < 30 Minutes

AGGREGATE SSD WEIGHTS

			(% Moisture)*		(absorption)**	
FA	a	Free Moisture, %	4.2	-		4.20 %
	b	SSD Weight [A / (1 + (a / 100))]				5268
IA	c	Free Moisture, %		-		%
	d	SSD Weight [B / (1 + (c / 100))]				0
CA	e	Free Moisture, %	1.70	-		1.70 %
	f	SSD Weight [C / (1 + (e / 100))]				7674

* Moisture From Batch Ticket

** Absorption From Mix Design, use 0.0% if Batch Ticket reports free moisture

TEMPERATURE — WAQTC FOP for T 309

		Weather Conditions
Concrete Temperature	66	
Air Temperature	65	Partly Cloudy
Water Temperature	59	No Rain or Wind

WAQTC FOP for:

				Specs:
	T 119	Slump, in.	4	2"-4"
	T 152	Air, %	5.0%	4-7%
a	Mass of Bucket + Conc.		43.75	lb.
b	Mass of Bucket		7.69	lb.
Mm	Mass of Conc. (a - b)		36.06	lb.
Vm	Bucket Volume		0.2494	ft^3
W	T 121	Density (Mm/Vm)	144.6	lb / ft^3

Test by/date: V. Bean #079 / 6-8-05

MASS OF WATER IN BATCH

		Lbs.
E	Free Water in FA (A - b)	221
F	Free Water in IA (B - d)	0
G	Free Water in CA (C - f)	130
H	Total Water Mass (D + D1 + E + F + G)	1102

CYLINDER DATA — WAQTC FOP for T 23

Time Made	Cylinder ID	
11:30 AM	1	5210
	2	5120
Spec: 4000 psi		

Test by/date: VB 6-8-05

Yd^3 Batch Design		BATCH DATA		Actual yd^3 Batch Data	Specifications		Allowable Range*		
4.25	VB	Design Batch Volume, nearest $0.01yd^3$							
		Actual yd^3 / Batch = $W1 / (27 \times W)$, nearest 0.01 yd^3	YB	4.24	* excludes 608, 609, 615, & Aviation items				
		Yield per yd^3 Batch = YB / VB, nearest 0.01 yd^3	Y	1.00					
0.45	W/C	Water Cement Ratio (lb / lb) = H / Nt, nearest 0.01	W/C	0.44					
	Mix Design Proportions	Cementitious Content (lb / yd^3) = Nt / YB, nearest lb.	N	588	± 1%	Batch Design		–	
		Sacks / yd^3 = $N / 94$, nearest 0.1 sack		6.3					
494		Portland Cement Content (lb / yd^3) = Nc / YB, nearest lb.		494	± 1%	Batch Design	489	–	499
94		Fly Ash Content (lb / yd^3) = Nf / YB, nearest lb.		94	± 5%	Batch Design	89	–	99
		Microsilica Content (lb / yd^3) = Nm / YB, nearest lb.			± 10%	Batch Design		–	
1250		Fine Aggregate = b / YB, nearest lb.		1242	± 2%*	Batch Design	1225	–	1275
		Intermediate Aggregate = d / YB, nearest lb.			± 2%*	Batch Design		–	
1800		Coarse Aggregate = f / YB, nearest lb.		1810	± 2%*	Batch Design	1764	–	1836

Remarks: Air entrainment added at 6 oz/cy Mix Design = 6 oz/cy, No WRA

Signature / Date:

Checked by / Date:

Rev.1/31/06